

TECHNICAL NARRATIVE & STORMWATER MANAGEMENT REPORT THE WILLOWS AT BOXFORD LOCATED OFF WILLOW ROAD

BOXFORD, MASSACHUSETTS

November 19, 2020

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TECHNICAL NARRATIVE & STORMWATER MANAGEMENT REPORT THE WILLOWS AT BOXFORD

LOCATED OFF WILLOW ROAD **BOXFORD, MASSACHUSETTS**

November 19, 2020

APPLICANT:

TOLL BROS., INC. 116 FLANDERS ROAD WESTBOROUGH, MA 01581

PREPARED BY: THE MORIN-CAMERON GROUP, INC. 66 ELM STREET DANVERS, MA 01923



Table of Contents

TECHNICAL NARRATIVE	2
I. EXECUTIVE SUMMARY	2
II. EXISTING SITE DESCRIPTION	2
III. PROPOSED PROJECT DESCRIPTION	4
A. Dwelling Units & Amenities	4
B. Private Drive, Sidewalks & Emergency Ac	cess 4
C. Earthwork and Land Disturbance	5
D. Stormwater Management Overview	5
E. Open Space and Preservation of Natural	Features 5
F. Utilities	6
G. Schedule	6
IV. STORMWATER MANAGEMENT	6
A. Existing Watershed Description	7
B. Proposed Watershed Description	8
C. Hydrologic Analysis	9
D. Stormwater Management Standards	11
V. CONCLUSION	13
FIGURES	
Figure 1: 2013 Ortho Map	
Figure 2: FEMA Flood Map	
Figure 3: USGS Locus Map	
Figure 4: SCS Soils Map	
Figure 5: Existing Watershed Plan	
Figure 6: Proposed Watershed Plan	
Figure 7: Rational Method Plan	

APPENDICIES

APPENDIX A: MassDEP Stormwater Management Report Checklist

APPENDIX B: Existing Conditions Hydrologic Analysis

APPENDIX C: Proposed Conditions Hydrologic Analysis

APPENDIX D: Stormwater Management Calculations

APPENDIX E: Vernal Pool Water Budget Summary

APPENDIX F: Construction Phase Best Management Practices

APPENDIX G: Long Term Best Management Practices O&M Plan

APPENDIX H: Illicit Discharge Statement

TECHNICAL NARRATIVE

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The Willows at Boxford

I. EXECUTIVE SUMMARY

Toll Brothers, Inc., the project proponent, proposes to develop a 66-unit age-restricted, active adult community on a 117.62-acre parcel located on Willow Road in Boxford, Massachusetts. The project consists of thirty-three (33) duplex style buildings, an accessory community building and outdoor amenity space. The new neighborhood will be supported by a private drive, stormwater management systems, electric and communications utilities, private water supply and an onsite wastewater disposal system. A large portion of the parcel will be preserved as permanent open space. The dwellings, associated improvements and open space on the property described herein will be known as The Willows at Boxford.

The Willows at Boxford was designed in accordance with the Town of Boxford Zoning Bylaw, the Massachusetts Stormwater Handbook and Boxford Stormwater Bylaw, the Wetlands Protection Act and its Regulations promulgated through 310 CMR 10.00, the Boxford Wetlands Protection Bylaw and the Boxford Health Regulations. The project will require a Special Permit and Site Plan Approval from the Boxford Zoning Board, an Order of Conditions from the Boxford Conservation Commission, an onsite wastewater disposal system approval from the Boxford Board of Health, a Conservation and Management permit from the Natural Heritage and Endangered Species Program, a community public water system permit from Mass Department of Environmental Protection (MassDEP) and an Environmental Notification Form under the Massachusetts Environmental Policy Act.

II. EXISTING SITE DESCRIPTION

The property consists of a single tract with a total land area of 117.62-acres. It is identified by the Boxford Assessor's Department on Tax Map 6 as Block 2, Lot 2.2. The property has $2,195\pm$ feet of frontage along Willow Road split between a small access frontage of 50-feet and the remaining frontage. The property is entirely within the Elderly Housing Zoning District. It has historically been used for agriculture and forestry. Refer to Figure 1 for an aerial depiction of the property.

Agricultural uses extend north from Willow Road over an approximate 25.62-acre portion of the tract (the "agricultural area"). Farming activities such as haying, corn, blueberry and Christmas tree horticulture are evidenced on the property today. There is a small farm stand structure near Willow Road which was used in the past for retail sales of the farmed products. The property has also been used for loam screening and distribution and recreational dirt biking. In support of the agricultural activities, manmade farm ponds were constructed. The remainder of the property, approximately 92 acres, has been left in a natural state and is interspersed by woods roads and pedestrian trails. The parcel also contains an extensive wetlands system which includes several vernal pools and is bordered to the north by the Parker River.

The Parker River is a regulatory floodway in this location, according the FEMA Federal Insurance Rate Map (FIRM) #25009C0233F with an effective date of July 3, 2012 (See Figure 2: FEMA Map). The 100-year Base Flood Elevation at the subject property is between elevation 88.0 and 89.0 (NAVD88), which generally follows the edge of the bordering vegetated wetlands that abut the river and serve as floodplain area. The remaining portion of the subject property is located within a FEMA flood hazard zone X (above the 100-year flood elevation).

An Order of Resource Area Delineation (ORAD) and ORAD Extension were issued for the subject property by the Boxford Conservation Commission, under DEP File No. 114-1235. Refer to the Notice of Intent prepared by LEC, dated November 19, 2020 for more information about the wetland resource areas (LEC report).

The contouring of the property varies from undulating hilly terrain to rolling farm fields. Slopes range from 2-3% to as steep as 25-33% in the hilly areas and approximately 10-15% throughout the farm fields. Wetlands, ponds and vernal pools can be found consistently at low points on the property. The lowest elevation on the property can be found near the northern property line along the Parker River at elevation 90. The highest elevation on the property can be found near the center of the property to the northwest of the well area at elevation 158. The agricultural area ranges from elevation 124 near Willow Road to 130 near the northern end of the field. Contours throughout the agricultural area have been manipulated over time through excavation activities as evidenced by soil tests conducted throughout this area. See Figure 3 for the United States Geological Survey map of the property.

Extensive soil testing was conducted by MCG and the project proponent throughout the agricultural area. In total, 111 test holes were excavated, the results of which are included in the site development plan set. In general, most of the agricultural area has been stripped down to within 2-4 feet of bedrock and filled with loam for agricultural purposes. Towards the rear of this area, native soil remains consisting of Glaciofluvial outwash deposits. Other pockets of native soil were identified throughout this area. The Natural Resource Conservation Service (NRCS) soil maps were also evaluated throughout the entire property. The Western and Southern portions of the locus parcel consist of well-drained Charlton Fine Sandy Loam (406D, 406C), excessively drained Hinckley loamy Sand (253B/C/D, 257E), and poorly drained Freetown muck (52A). The Northern portion of the locus parcel consists of poorly drained Swansea muck (51A) and excessively drained Hinckley Loamy Sand (253C/D, 257E). The Eastern portion of the locus parcel consists of poorly drained Swansea muck Hinckley loamy sand (253B/C/D, 257E). The Eastern portion of the locus parcel consists of poorly drained Swansea muck (51A) and excessively drained Charlton Fine Sandy Loam (406D), excessively drained Hinckley Loamy Sand (253C/D, 257E). The Eastern portion of the locus parcel consists of well-drained Charlton Fine Sandy Loam (406D), excessively drained Hinckley Loamy Sand (253C/D, 257E). The Eastern portion of the locus parcel consists of well-drained Charlton Fine Sandy Loam (406D), excessively drained Hinckley Loamy Sand (253C/D, 257E). The Eastern portion of the locus parcel consists of well-drained Charlton Fine Sandy Loam (406D), excessively drained Hinckley Loamy Sand (253C/D, 257E). The Eastern portion of the locus parcel consists of well-drained Charlton Fine Sandy Loam (406D), excessively drained Hinckley Loamy Sand (253B/C/D, 257E).

III. PROPOSED PROJECT DESCRIPTION

A. Dwelling Units & Amenities

The Willows at Boxford will consist of thirty-three (33) new duplex buildings for a total of sixtysix (66) new age-restricted homes. The age restriction is consistent with the Elderly Housing Zoning District for persons 55 years or older and the dwellings and amenities are configured specifically for that age demographic. There will be multiple unit styles available for buyers to select each with a relatively consistent exterior appearance. Various options will be available for each unit style along with the flexibility of customizing interior finishes. The unit floor plans will all include a first-floor master bedroom. Livable floor area will vary between 1,627-2,900 square feet per home, including the second-floor guest bed/study area. Each home will have a dedicated driveway, a two-car garage facing the street, and a patio or deck in the rear. Landscaping around each unit is illustrated on the landscape plans included with this report. There will be a community clubhouse with a pool, and outdoor recreational area for use by residents of The Willows at Boxford. The project will also feature an extensive passive recreational pedestrian trail network throughout preserved woodland and open space for use by the residents of the neighborhood and public at large.

B. Private Drive, Sidewalks & Emergency Access

A twenty-four-foot-wide private drive will be constructed to provide access to the dwelling units and amenity spaces. Private Drive "A" is the primary access and is 2,490 feet long from Willow Road to a cul-de-sac designed in accordance with the Boxford Subdivision Regulations. Private Drive "B" is a short spur road off of Private Drive "A", which services three duplex buildings and connects to the emergency access Drive. The emergency access drive will be gated at Willow Road, and signage will be placed at the other end, prohibiting use by unauthorized vehicles. All vehicular surfaces will be paved with bituminous asphalt. The total length of new private drive is approximately 2,837 feet, and the emergency access drive is approximately 537 feet long. The length of Private Drive A between the emergency access drive and the end of the cul-de-sac is 1,342 feet.

Sidewalks will be constructed along one side of the private drive. The sidewalks will provide a pedestrian route through the neighborhood and connect to the amenities including the clubhouse, trails and open space. The slope of the sidewalk will match the slope of the adjacent private drive.

The private drives were primarily designed to have gentle slopes ranging between 1.2% to 4%. A short section between stations 21+23.5 to 22+68.5 will be constructed to a 5% slope. Vertical curves along the road were designed to accommodate a 25 MPH design speed. The private drives will have a crown along the centerline and a curb at the gutter line to convey roadway runoff to closed drainage infrastructure (i.e. catch basins), before being directed to stormwater best management practices for treatment prior to infiltration or discharge. All dwelling driveways were sloped back to the private drive so that stormwater runoff from all paved areas

will be directed to the closed drainage system. The private drive design standards follow the Boxford Subdivision Rules and Regulations.

Private Drive A will feature a significant upgrade to the existing access to the rear portion of the parcel as it passes through a wetland near flags W105 to W108. The existing farm road passing through the wetland in this area was constructed with a 12" culvert, solely intended to allow the conveyance of surface runoff under the farm road. With the construction of Private Drive A, a new 10' wide x 9' tall concrete box culvert will replace the existing 12" culvert as part of a full reconstruction of this wetland crossing. The new box culvert will maintain existing grades at each end to preserve the hydrologic gradient that exists today. This is important in maintaining the hydrology of the wetland system. Concurrently, the culvert will improve wildlife passage by complying with the openness ratio (height and width vs. area) and other requirements of the MassDEP River and Stream Crossing Guidance. While there will be a marginal increase to the footprint of the road as it crosses through the use of modular retaining walls. Wetland impacts will be mitigated through the construction of new wetland areas as outlined in the LEC report.

C. Earthwork and Land Disturbance

The Project Site is generally located within the previously altered agricultural area on the property. The land area of the Project Site is approximately 25.62 acres. As described above, this area has been historically manipulated through excavation of overburden soil and import of loam associated with the agricultural use. It is for the most part relatively flat with earth work being driven by the need to ensure proper stormwater management slopes are achieved for the road and areas around the dwellings. Earth work occurring between stations #+## to #+## will be necessary to soften the steep slope of the hill in that area. Overall, the project has been designed to balance cut and fill volumes to minimize the export and import of soil material from the property. Not only is this strategy cost effective, but it also benefits the public by minimizing temporary construction truck trips and the duration of construction.

D. Stormwater Management Overview

The stormwater management system was designed in full compliance with the Massachusetts Stormwater Handbook and Boxford Stormwater Bylaw. The treatment train consists of deepsump hooded catch basins, sediment forebays, infiltration basins, infiltration trenches and a detention basin. A closed-drainage system will be installed in the roadway, which will convey runoff to best management practice systems to provide storage and infiltration. Further explanation of the stormwater management system and design methodology can be found later in this report.

E. Open Space and Preservation of Natural Features

The project was designed such that a significant percentage of the site will remain undisturbed. Of the 117.6-acre total parcel area, only 25.7 acres will be disturbed, and two acres will be set aside for a future development parcel along Willow Road. This results in a total of 89.9 acres of land that will be protected, which is 76% of the subject property. The proposed site design incorporates the principals of clustered development practices in minimizing the separation between dwellings, minimizing pavement footprints and consolidation the limit of work. This approach maximizes land use efficiency by filling the need for senior housing while maximizing the preservation of open space. The design allows for the protection of all wetland resource areas and other unique natural features on the subject property, such as the farm ponds and multiple open meadow areas.

The Natural Heritage and Endangered Species Program has jurisdiction over the subject property, and the applicant, through LEC, has had extensive conversations with Massachusetts Division of Fisheries and Wildlife about the proposed project. In conjunction with these efforts, the project has been designed to avoid, minimize, and mitigate potential impacts to state-listed rare species habitat. A Habitat Management Area Plan was prepared by LEC, which is included in the Notice of Intent application. LEC will also be filing a Conservation and Management Permit Application with NHESP and an Environmental Notification Form with MEPA for the project.

F. Utilities

The project will include a community public water supply system, with the proposed well locations identified on the Site Plans. The well design, permitting, construction and long-term maintenance will follow MassDEP regulations. The project will also include an onsite wastewater disposal system which will be designed in accordance with 310 CMR 15.00: Title 5 and the Boxford Board of Health Regulations. Provisions for natural gas (if no natural gas, propane or oil fuel will be utilized), electric service, cable, fiber optic and other communications services will be coordinated with the individual utility providers. Two new fire cisterns will be installed within the development, which will be coordinated with the Boxford Fire Department.

G. Schedule

Construction of the proposed development is anticipated to start in spring of 2021 and will take approximately 2 years to complete.

IV. STORMWATER MANAGEMENT

The proposed stormwater management system for the project will consist of various Best Management Practice (BMP) techniques used in both mitigating and renovating stormwater runoff. The entire stormwater system was designed in accordance with the Massachusetts Stormwater Management Handbook, in addition to the requirements contained within the Boxford Stormwater Management Bylaw. The existing watershed characteristics, flow paths and drainage patterns were matched to the extent practicable in the proposed condition to ensure that there are no adverse impacts to adjacent properties or wetland resource areas.

A detailed analysis was conducted for each of the three vernal pools on the subject property, to ensure that there will not be a decrease in the amount of water they receive from their tributary watersheds. This "water budget" comparison was made based on the existing versus proposed conditions and includes an analysis of both surface runoff and groundwater recharge volumes.

The vernal pool subcatchments are identified in the next section, and the results of this analysis are summarized in Appendix H: Vernal Pool Water Budget Summary.

A. Existing Watershed Description

The existing watershed of the Project Site was divided into eight separate subcatchment areas, as shown on Figure 5: Existing Watershed Plan. The edge of the bordering vegetated wetland surrounding the Project Site was chosen as the limit of the study area, and the Design Points were selected according to the natural drainage divides of the study area. In order to perform the water budget analysis of the vernal pools, individual subcatchments were delineated and a Design Point was assigned to each vernal pool (2A, 3A and 5A). As these Design Points were only used to compare existing and proposed volumes discharging to the vernal pools, the peak flow rates are not reported at these locations. Instead, Design Points 2A, 3A and 5A were routed to Design Points 2, 3 and 5, respectively. The table below summarizes the characteristics and tributary Design Point of each subcatchment.

Based on the results of extensive on-site soil testing, Hydrologic Soil Group B (HSG-B) was selected as the most appropriate and realistic category for the purposes of the drainage analysis. The published SCS Soil Map lists the upland soils in the study area as HSG-A, based on the well-draining parent material derived from glacial outwash deposits. However, the landscape within the study area has been substantially altered by past earth disturbance and agricultural activities, so the soils will not function as native undisturbed soils would. Additionally, the use of HSG-A in the HydroCAD model gives unrealistically low runoff rates for these large watershed areas, based on the associated runoff curve numbers. Therefore, the selection of HSG-B as a composite Hydrologic Soil Group was determined to yield the most accurate representation of the surface runoff and infiltration values within the study area.

Summary of Exist	ang Subcatchi	nemus		
<u>Existing</u>	<u>Total Area</u>	<u>% Impervious</u>	<u>Curve Number</u>	<u>Tributary Design</u>
Subcatchment	<u>(SF)</u>			<u>Point</u>
ES1	338,407	0	59	DP-1
ES2	201,899	0	58	DP-2
ES2A	84,051	0	60	DP2A (VP1) \rightarrow DP2
ES3	160,395	0	59	DP-3
ES3A	115,072	0	57	DP3A (VP3) \rightarrow DP3
ES4	420,097	0	61	DP-4
ES5	301,140	0	60	DP-5
ES5A	168,926	0	59	DP5A (VP2) \rightarrow DP5
Totals	1,789,987	0	59	
	.,	5	20	

Summary of Existing Subcatchments

B. Proposed Watershed Description

The proposed (post development) drainage analysis was performed by dividing the study area into sixteen (16) subcatchment areas (See Figure 6: Proposed Watershed Plan). In order to provide treatment and mitigation of stormwater runoff from the development, several BMPs were included in the design. They are listed below, along with their corresponding HydroCAD "pond" number.

- Pond 1P: Grassed Detention Basin
- Pond 2P: Grassed Infiltration Basin
- Pond 3P: Grassed Infiltration Basin
- Pond 4P: Grassed Infiltration Basin
- Pond 5P: Grassed Infiltration Basin
- Pond 6P: Crushed Stone Infiltration Trench

The table below summarizes the characteristics and tributary Design Point (and BMP) of each subcatchment.

Juliniary of Trop	oscu Subcute			
<u>Proposed</u>	<u>Total Area</u>	<u>% Impervious</u>	<u>Curve Number</u>	<u>Tributary Design</u>
<u>Subcatchment</u>	<u>(SF)</u>			<u>Point / Pond</u>
PS1	343,774	1.74	58	DP1
PS2	119,197	5.18	59	DP2
PS2A	52,258	2.20	57	$DP2A \rightarrow DP2$
PS3	97,067	3.56	58	DP3
PS3A	67,954	3.39	57	$DP3A \rightarrow DP3$
PS4	171,976	9.20	61	DP4
PS5	73,892	3.12	58	PS5
PS5A	95,000	1.21	56	$DP5A \rightarrow DP5$
PS6	168,938	15.67	63	DP5
PS7	95,556	32.02	73	$5P \rightarrow DP5A \rightarrow DP5$
PS8	39,073	71.28	87	$3P \rightarrow DP4$
PS9	149,876	53.46	81	$3P \rightarrow DP4$
PS10	78,810	59.90	83	$1P \rightarrow DP2$
PS11	72,767	37.18	79	$3P \rightarrow DP4$
PS12	45,344	3.81	62	$1P \rightarrow DP2$
PS13	25,606	30.26	72	$2P \rightarrow DP2A \rightarrow DP2$
PS14	22,124	10.42	63	$4P \rightarrow DP3A \rightarrow DP3$
PS15	21,777	100	98	$2P \rightarrow DP2A \rightarrow DP2$
PS16	21,777	100	98	$3P \rightarrow DP4$
PS17	27,221	100	98	$6P \rightarrow DP3A \rightarrow DP3$
Totals	1,789,987	20.12	66	

Summary of Proposed Subcatchments

C. Hydrologic Analysis

The purpose of the stormwater analysis is to demonstrate that the proposed development will not adversely impact either the Project Site or surrounding land and resource areas. The industry standard for stormwater management design in Massachusetts is governed by the Massachusetts Stormwater Management Handbook ("Handbook") published by the Mass Department of Environmental Protection, January 2008. The Regulations require applicants to comply with the Handbook standards for development projects. The Handbook lists 10 standards covering both mitigation and renovation of stormwater runoff. A full discussion on the project compliance with the standards can be found at the end of this report. However, the following section will summarize the project's compliance with the mitigation standards 1 and 2 of the Handbook relating to reducing peak rates of runoff and creating no adverse down gradient impacts.

To demonstrate that there will be no downstream impacts because of developing the site, a stormwater analysis was performed using the U.S. Soil Conservation Service (S.C.S) method of analysis contained in Technical Release #20 (TR-20) published by the U.S. Conservation Service, along with the precipitation values listed in Boxford's Stormwater Management Bylaw. The software application HydroCAD was utilized to analyze the pre and post-development watershed conditions.

The following is a listing of the total pre-and post-development rates of stormwater runoff for the primary Design Points for the 2, 10, 25, 50 and 100-year rainfall events. The dedicated vernal pool Design Points (2A, 3A & 5A) were not individually analyzed because they are tributary to other Design Points (2, 3 & 5) as described previously.

Design	Storm	Existing	Proposed	Change in
Point	Event	Conditions	Conditions	Peak
	(Years)	(Peak CFS)	(Peak CFS)	(CFS)
<u>DP-1</u>	2	1.4	1.2	-0.2
	10	6.6	6.4	-0.2
	25	11.0	10.7	-0.3
	50	14.5	14.3	-0.2
	100	18.5	18.4	-0.1
DP-2	2	1.2	1.1	-0.1
	10	6.7	4.8	-1.9
	25	11.2	9.5	-1.7
	50	14.8	14.5	-0.3
	100	19.1	19.1	-0.0

Comparison of Existing and Proposed Rates of Runoff

2	1.0	0.7	-0.3
10	5.4	5.1	-0.3
25	9.1	8.0	-1.1
50	12.1	10.3	-1.8
100	15.6	12.9	-2.7
2	2.3	1.3	-1.0
10	10.0	5.8	-4.2
25	16.1	9.4	-6.7
50	21.0	12.2	-8.8
100	26.6	16.0	-10.6
2	2.2	1.7	-0.5
10	10.4	8.0	-2.4
25	17.0	13.0	-4.0
50	22.4	18.8	-3.6
100	28.6	26.9	-1.7
	10 25 50 100 2 10 25 50 100 2 10 25 50	10 5.4 25 9.1 50 12.1 100 15.6 2 2.3 10 10.0 25 16.1 50 21.0 100 26.6 2 2.2 10 10.4 25 17.0 50 22.4	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$

As shown in the table above, the proposed development will maintain or reduce peak flow rates to all Design Points for the 2, 10, and 100-year design storms as required by the Massachusetts Stormwater Management Handbook. The 25-year and 50-year events were also analyzed as required by Boxford's Stormwater Management Bylaw.

The Boxford Stormwater Management Bylaw also requires that total runoff volume is not increased from the pre-development to post-development condition. The table below summarizes the total runoff volume generated by the study area watershed, which is reported at Design Point 1, the most downstream location of the Parker River.

Comparison of Existing and Proposed Volumes of Runoff	
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Design	Storm	Existing	Proposed	Change in
Point	Event	Conditions	Conditions	Volume
	(Years)	(CF)	(CF)	(CF)
<u>DP-1</u>	2	60,455	51,634	-8,821
	10	198,997	178,492	-20,505
	25	308,122	291,336	-16,786

50	396,067	383,075	-12,992
100	499,157	489,806	-9,351

D. Stormwater Management Standards

The proposed site development will comply with all Stormwater Management Standards. The following is an assessment of each Standard:

1. STANDARD: No stormwater conveyance system discharges untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth.

SUMMARY OF MITIGATING MEASURES: The project meets this standard as there are no new untreated discharges from the project site. The existing drainage patterns will be maintained to the extent practicable and the stormwater discharge locations will generally be maintained. Treatment of stormwater is proposed with best management practices (BMPs) including deep sump hooded catch basins, hydrodynamic separators, grassed infiltration basins, infiltration trenches, and a detention basin. The outfalls of all the systems will be reinforced with rip rap outlet protection to prevent erosion.

CONCLUSION: The proposed development meets this standard.

2. STANDARD: The stormwater management system shall be designed such that postdevelopment peak rates of stormwater runoff do not exceed pre-development rates for the 2- and 10-year storm events.

SUMMARY OF MITIGATING MEASURES: The project will utilize several BMPs that include outlet structures to control the rate of release of stormwater. As a result, the peak rate of stormwater runoff in the post-development condition will match or reduce the rate under existing conditions. The 100-year storm event was also evaluated and the BMPs were designed to reduce the existing conditions peak 100-year storm rate of runoff to prevent storm damage and prevent off-site flooding. The 25-year and 50-year events were included in the analysis as required by the Boxford Stormwater Management Bylaw.

CONCLUSION: The proposed development meets this standard.

3. STANDARD: Loss of annual recharge to groundwater shall be eliminated or minimized with infiltration measures including environmentally sensitive site design, low impact development techniques, stormwater best management practices, and good operation and maintenance. At a minimum, the annual recharge from the post-development site shall approximate the annual recharge from pre-development conditions based on soil type. This Standard is met when the stormwater management system is designed to infiltrate the required recharge volume as determined in accordance with the Massachusetts Stormwater handbook.

SUMMARY OF MITIGATING MEASURES: To promote groundwater recharge, the site has been designed to include numerous infiltration systems. The systems were strategically placed within the site in order to maximize the infiltration capacity and to spread out the groundwater recharge locations. The system will accept either pre-treated stormwater or direct roof runoff prior to infiltration. The BMPs will provide recharge to groundwater in excess of what is estimated in the existing condition.

CONCLUSION: The proposed development meets this standard.

4. STANDARD: Stormwater management systems shall be designed to remove 80% of the average annual post-construction load of Total Suspended Solids (TSS).

SUMMARY OF MITIGATING MEASURES: The stormwater management system will use treatment trains of deep sump hooded catch basins, proprietary treatment structures and infiltration/detention systems to treat stormwater prior to discharge. Pre-treatment of stormwater is provided for all systems. All stormwater will be treated to a minimum of 80% TSS removal prior to discharging to the design points.

CONCLUSION: The proposed development meets this standard.

5. STANDARD: For land uses with higher potential pollutant loads, source control and pollution prevention shall be implemented in accordance with the Massachusetts Stormwater handbook to eliminate or reduce the discharge of stormwater runoff from such land uses to the maximum extent practicable.

SUMMARY OF MITIGATING MEASURES: None.

CONCLUSION: The proposed development meets this standard as it does not apply to this project.

6. **STANDARD:** Stormwater discharges within the Interim Wellhead Protection Area of a public water supply, and stormwater discharges near or to any other critical area including vernal pools, require the use of the specific source control and pollution prevention measures and the specific structural stormwater best management practices determined by the Department to be suitable for managing discharges to such areas, as provided in the Massachusetts Stormwater Management handbook.

SUMMARY OF MITIGATING MEASURES: The project has been designed to provide the higher level of treatment including 44% pretreatment primary to the retention/detention BMP and treating for 1" of runoff.

CONCLUSION: The proposed development meets this standard.

7. STANDARD: A redevelopment project is required to meet the following Stormwater Management Standards only to the maximum extent practicable: Standard 2, Standard 3, and the pretreatment and structural best management practice requirements of Standards 4, 5 and 6. Existing stormwater discharges shall comply with Standard 1 only to the maximum extent practicable. A redevelopment project shall also comply with all other requirements of the Stormwater Management Standards and improve existing conditions.

SUMMARY OF MITIGATING MEASURES: None.

CONCLUSION: The proposed development meets this standard as it does not apply to this project.

8. **STANDARD:** A plan to control construction-related impacts including erosion, sedimentation and other pollutant sources during construction and land disturbance activities (construction period erosion, sedimentation, and pollution prevention plan) shall be developed and implemented).

SUMMARY OF MITIGATING MEASURES: Refer to the Construction Phase Best Management Practices prepared by MCG, dated November 19, 2020. Since the project will disturb greater than one acre of land a SWPPP will be prepared and a NPDES Construction General Permit will be obtained prior to commencement of land disturbing activities on site.

CONCLUSION: The proposed development meets this standard.

9. STANDARD: A long-term operation and maintenance plan shall be developed and implemented to ensure that stormwater management systems function as designed.

SUMMARY OF MITIGATING MEASURES: Refer to the Long-Term Best Management Practices Operation and Maintenance Plan prepared by MCG, dated November 19, 2020.

CONCLUSION: The proposed development meets this standard.

10. STANDARD: There shall be no new illicit discharges created as a result of the project.

SUMMARY OF MITIGATING MEASURES: To the best of our knowledge and belief there are no illicit discharges being created as a result of the proposed project. An illicit discharge statement is included herein.

CONCLUSION: The proposed development meets this standard.

V. CONCLUSION

The proposed site development project for Willows at Boxford, as proposed, is in full compliance with the MassDEP Stormwater Management Handbook and utilizes generally accepted engineering practices for site development. Peak rates of stormwater runoff and volume leaving the site under proposed conditions are no greater than under existing conditions. Recharge to groundwater will be increased by proposed stormwater management systems. All stormwater leaving the proposed development will be fully treated and there are no illicit discharges to the waters of the Commonwealth.

The clustered development footprint allows for the provision of local, age-restricted housing units while maximizing the protection of open space and natural resource areas. As such, the proposed project will be a benefit to the Town of Boxford by incorporating innovative land use techniques, providing local housing units in an active adult community and protecting the wetland and water resources of the Commonwealth.

For questions regarding this report, please contact The Morin-Cameron Group, Inc. between the hours of 7:30am to 4:30pm at (978) 373-0310.

The Willows at Boxford Technical Narrative

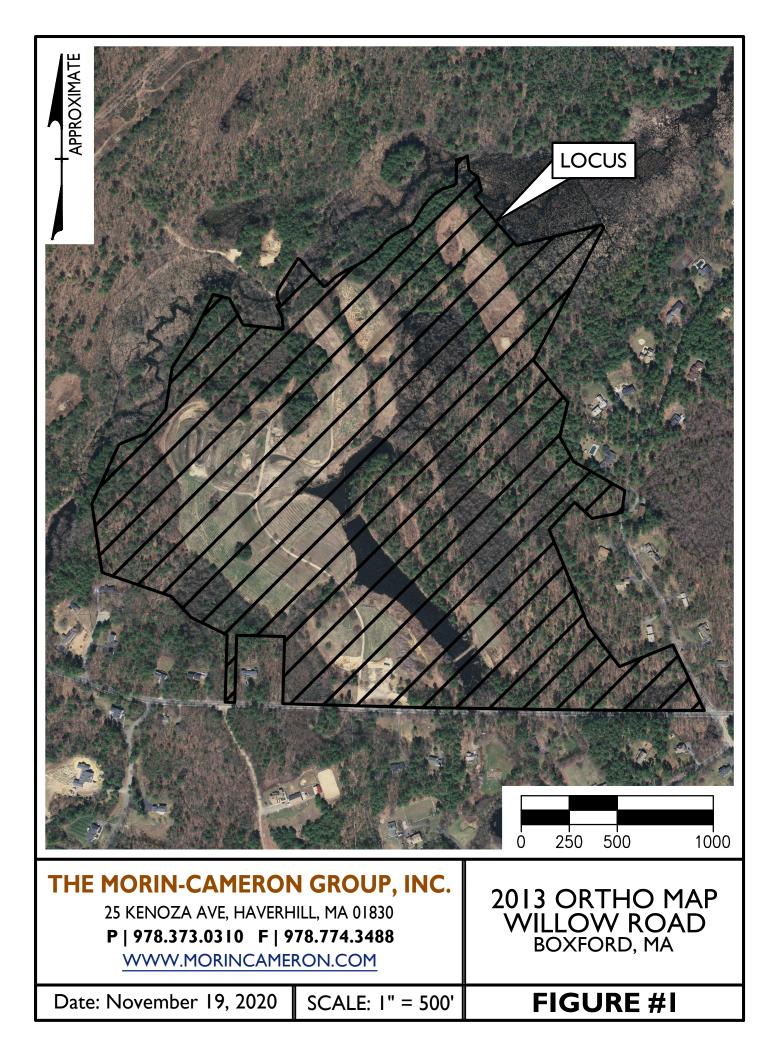
FIGURES

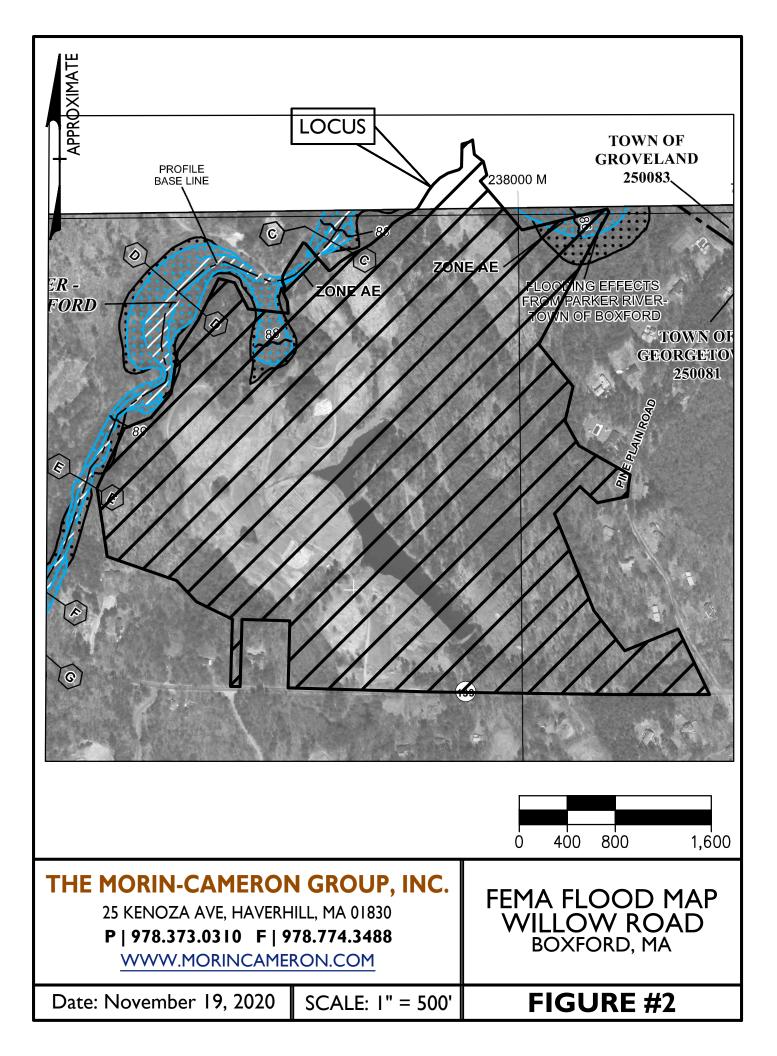
Figure 1: 2013 Ortho Map Figure 2: FEMA Flood Map Figure 3: USGS Locus Map Figure 4: SCS Soils Map Figure 5: Existing Watershed Plan Figure 6: Proposed Watershed Plan Figure 7: Rational Method Plan

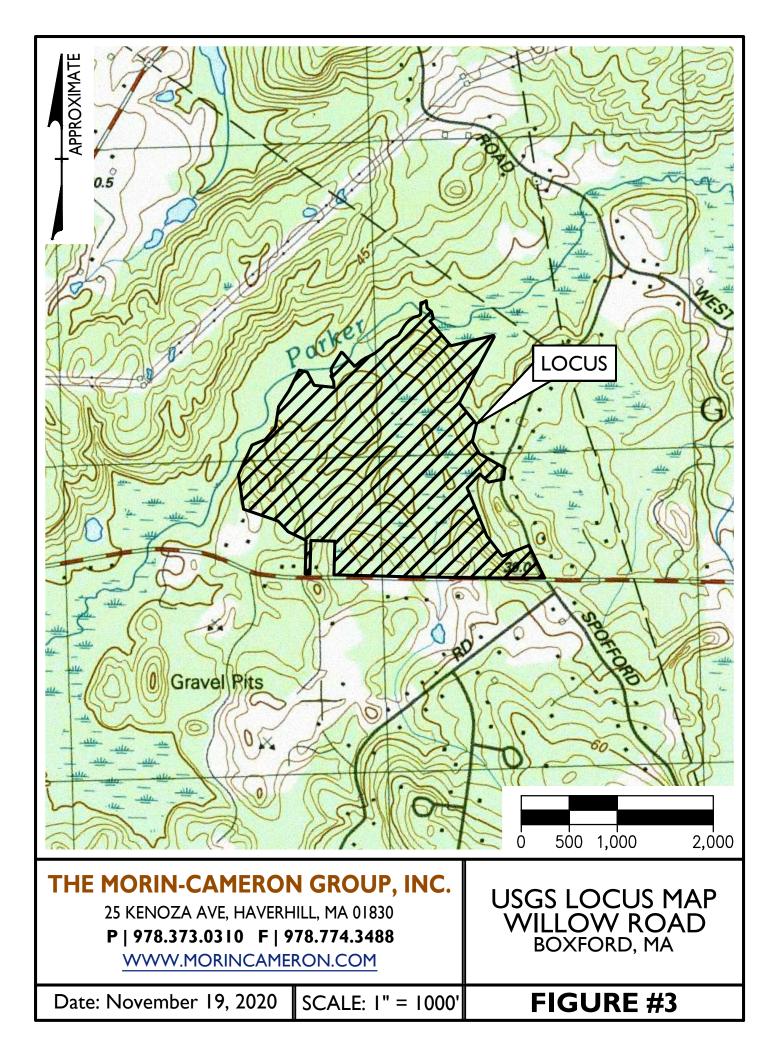
APPENDICIES

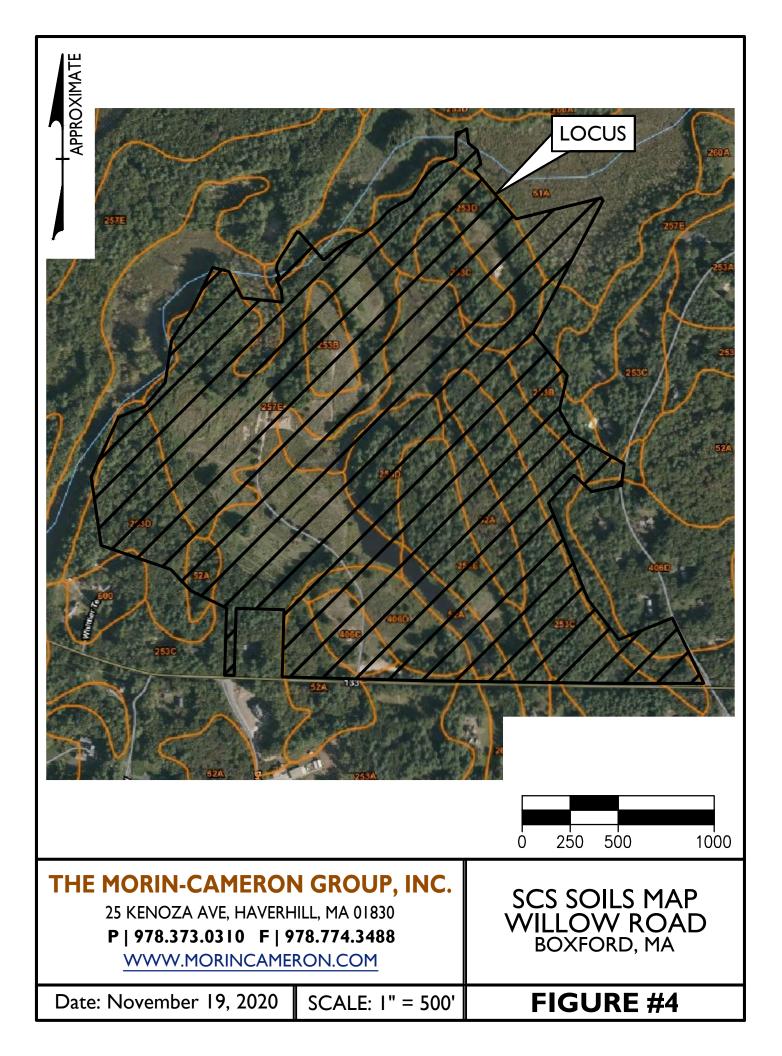
APPENDIX A: MassDEP Stormwater Management Report Checklist APPENDIX B: Existing Conditions Hydrologic Analysis APPENDIX C: Proposed Conditions Hydrologic Analysis APPENDIX D: Stormwater Management Calculations APPENDIX E: Vernal Pool Water Budget Summary APPENDIX F: Construction Phase Best Management Practices APPENDIX G: Long Term Best Management Practices O&M Plan APPENDIX H: Illicit Discharge Statement

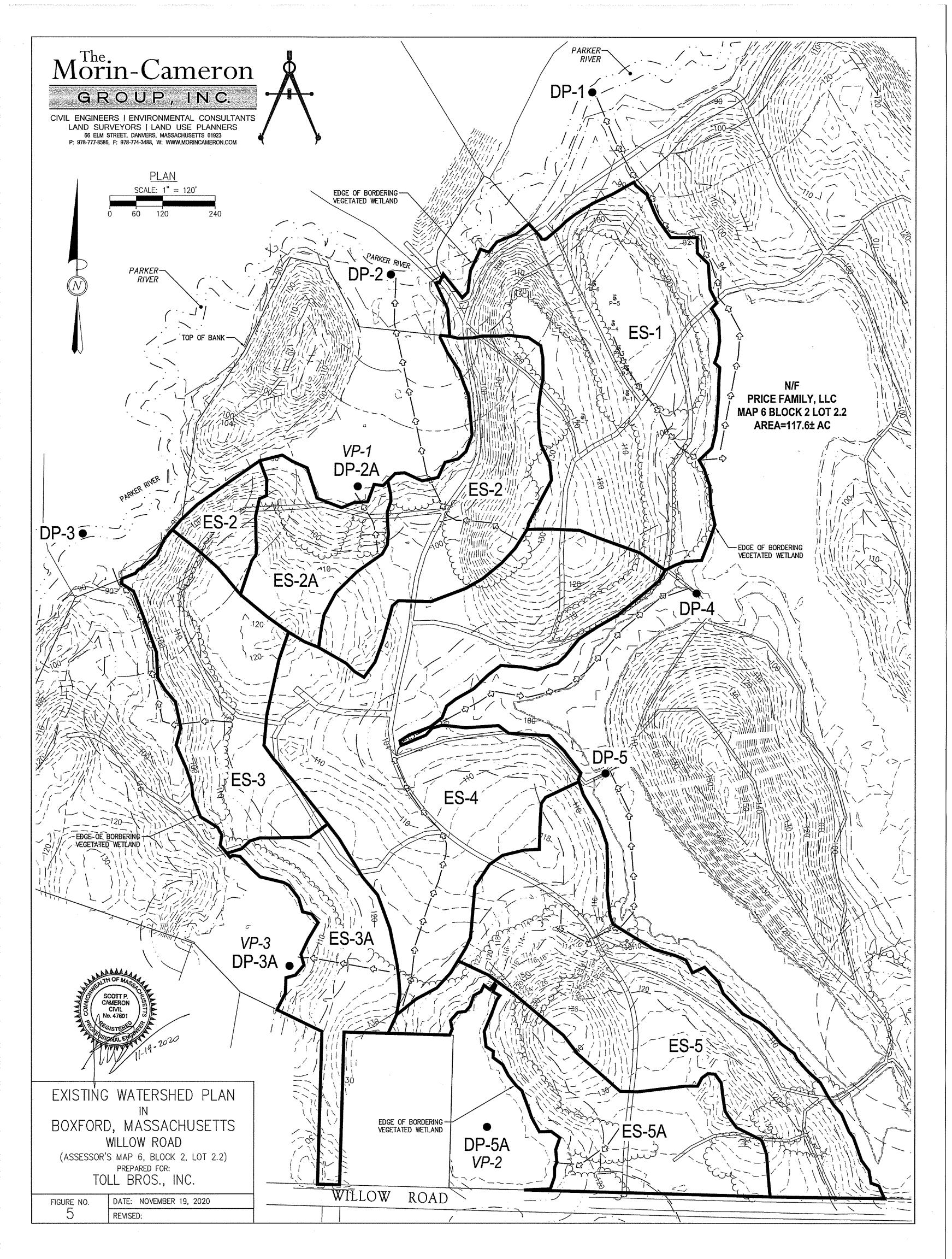
FIGURES

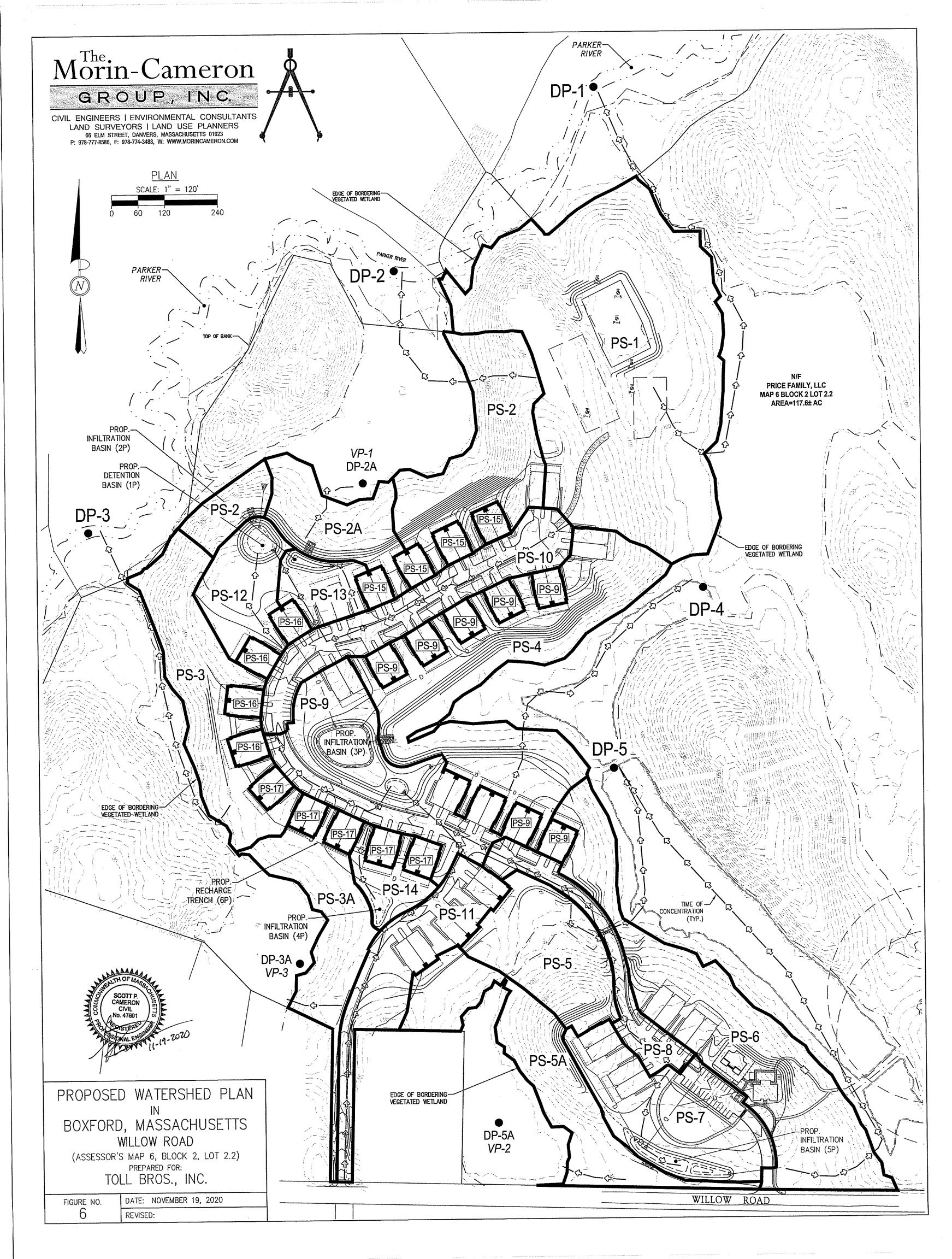


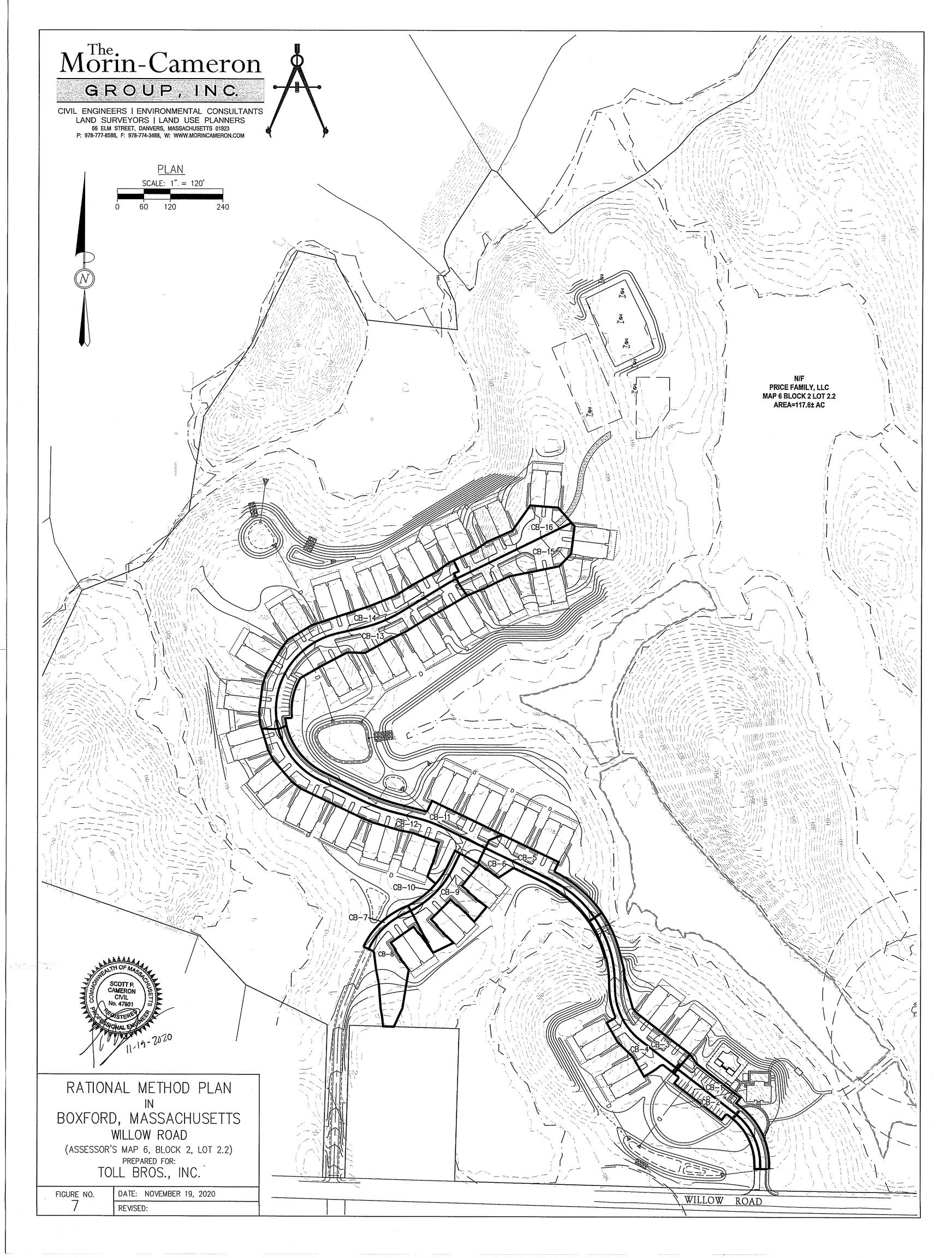












MANAGEMENT REPORT CHECKLIST

MASSDEP STORMWATER

APPENDIX A:



Checklist for Stormwater Report

A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.



A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.¹ This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8²
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

3717 DEP checklist.docx • 04/01/08

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

B. Stormwater Checklist and Certification

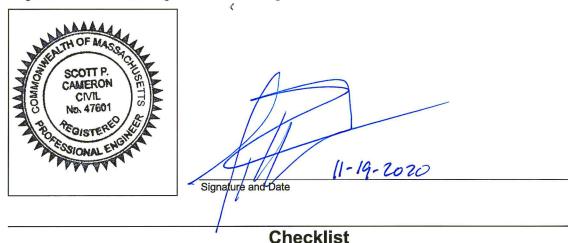
The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Long-term Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.



Registered Professional Engineer Block and Signature

Project Type: Is the application for new development, redevelopment, or a mix of new and

redevelopment?

New development

Redevelopment

Mix of New Development and Redevelopment



Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

Checklist (continued)

LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

- No disturbance to any Wetland Resource Areas
- Site Design Practices (e.g. clustered development, reduced frontage setbacks)
- Reduced Impervious Area (Redevelopment Only) (Reduced Pavement)
- Minimizing disturbance to existing trees and shrubs
- LID Site Design Credit Requested:
 - Credit 1
 - Credit 2
 - Credit 3
- Use of "country drainage" versus curb and gutter conveyance and pipe
- Bioretention Cells (includes Rain Gardens)
- Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
- Treebox Filter
- Water Quality Swale
- Grass Channel
- Green Roof
- Other (describe):

Standard 1: No New Untreated Discharges

- No new untreated discharges
- Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.

· V. . .



Checklist (continued)

Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.

Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm.

Standard 3: Recharge

Sc Sc	oil Ana	lysis	provided.
-------	---------	-------	-----------

- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.

Static Simple Dynamic

Dynamic Field¹

- Runoff from all impervious areas at the site discharging to the infiltration BMP.
- Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume *only* to the maximum extent practicable for the following reason:
 - Site is comprised solely of C and D soils and/or bedrock at the land surface
 - M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
 - Solid Waste Landfill pursuant to 310 CMR 19.000
 - Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- Calculations showing that the infiltration BMPs will drain in 72 hours are provided.
- Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

3717 DEP checklist.docx • 04/01/08

Stormwater Report Checklist • Page 4 of 8

¹ 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



Checklist for Stormwater Report

Checklist (continued)

Standard 3: Recharge (continued)

- The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
- Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

Standard 4: Water Quality

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- · Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
- Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
 - is within the Zone II or Interim Wellhead Protection Area
 - is near or to other critical areas
 - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
 - involves runoff from land uses with higher potential pollutant loads.
- The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



Checklist for Stormwater Report

Checklist (continued)

Standard 4: Water Quality (continued)

- The BMP is sized (and calculations provided) based on:
 - The ½" or 1" Water Quality Volume or
 - The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
- The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
- A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.

Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)

- The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.
- The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted **prior** to the discharge of stormwater to the post-construction stormwater BMPs.
- The NPDES Multi-Sector General Permit does *not* cover the land use.
- LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
- All exposure has been eliminated.
- All exposure has *not* been eliminated and all BMPs selected are on MassDEP LUHPPL list.
- ☐ The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.

Standard 6: Critical Areas

- The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
- Critical areas and BMPs are identified in the Stormwater Report.



Checklist for Stormwater Report

Checklist (continued)

Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

- The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:
 - Limited Project
 - Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.

Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area

- Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
- Bike Path and/or Foot Path
- Redevelopment Project
- Redevelopment portion of mix of new and redevelopment.
- Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.
- ☐ The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.
- A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



Checklist (continued)

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

- ☐ The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has *not* been included in the Stormwater Report but will be submitted *before* land disturbance begins.
- The project is *not* covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

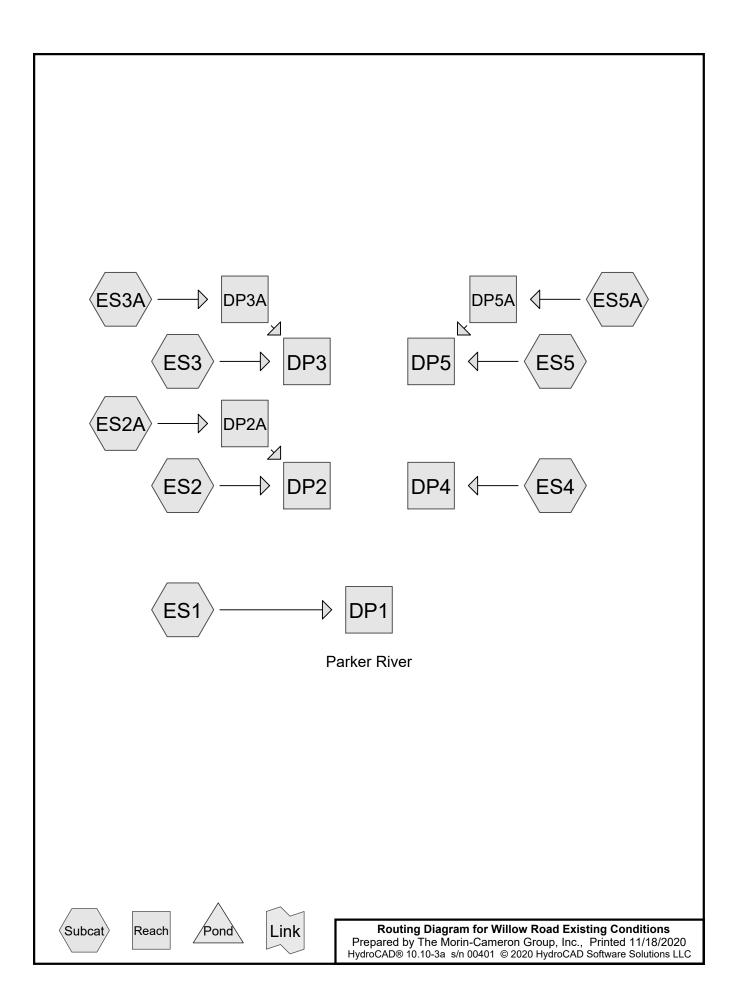
Standard 9: Operation and Maintenance Plan

- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
 - Name of the stormwater management system owners;
 - Party responsible for operation and maintenance;
 - Schedule for implementation of routine and non-routine maintenance tasks;
 - Plan showing the location of all stormwater BMPs maintenance access areas;
 - Description and delineation of public safety features;
 - Estimated operation and maintenance budget; and
 - Operation and Maintenance Log Form.
- The responsible party is **not** the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
 - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
 - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of any stormwater to post-construction BMPs.

APPENDIX B: EXISTING CONDITIONS HYDROLOGIC ANALYSIS



Willow Road Existing Conditions Prepared by The Morin-Cameron Group, Inc. HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLC

Area Listing (all nodes)

Area (sq-ft)	CN	Description (subcatchment-numbers)
1,252,784	61	>75% Grass cover, Good, HSG B (ES1, ES2, ES2A, ES3, ES3A, ES4, ES5, ES5A)
537,203 1,789,987	55 59	Woods, Good, HSG B (ES1, ES2, ES2A, ES3, ES3A, ES4, ES5, ES5A) TOTAL AREA

Willow Road Existing Conditions Prepared by The Morin-Cameron Group, Inc. HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLC

Soil Listing (all nodes)

Area	Soil	Subcatchment
(sq-ft)	Group	Numbers
0	HSG A	
1,789,987	HSG B	ES1, ES2, ES2A, ES3, ES3A, ES4, ES5, ES5A
0	HSG C	
0	HSG D	
0	Other	
1,789,987		TOTAL AREA

Willow Road Existing Conditions

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Printed 11/18/2020 Page 4

			,	· ·			
Sub Nun	Ground Cover	Total (sq-ft)	Other (sq-ft)	HSG-D (sq-ft)	HSG-C (sq-ft)	HSG-B (sq-ft)	HSG-A (sq-ft)
-	00701	(94 10)	(59 10)	(59 10)	(59 17)	(59 10)	(59 17)
	>75% Grass	1,252,784	0	0	0	1,252,784	0
	cover, Good						
	Woods, Good	537,203	0	0	0	537,203	0
	TOTAL AREA	1,789,987	0	0	0	1,789,987	0

Ground Covers (all nodes)

Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

SubcatchmentES1:	Runoff Area=338,407 sf 0.00% Impervious Runoff Depth=0.39" Flow Length=350' Tc=23.4 min CN=59 Runoff=1.4 cfs 10,971 cf
SubcatchmentES2:	Runoff Area=201,899 sf 0.00% Impervious Runoff Depth=0.36" Flow Length=615' Tc=13.8 min CN=58 Runoff=0.8 cfs 5,979 cf
SubcatchmentES2A:	Runoff Area=84,051 sf 0.00% Impervious Runoff Depth=0.42" Flow Length=150' Tc=13.5 min CN=60 Runoff=0.5 cfs 2,970 cf
SubcatchmentES3:	Runoff Area=160,395 sf 0.00% Impervious Runoff Depth=0.39" Flow Length=540' Tc=16.8 min CN=59 Runoff=0.7 cfs 5,200 cf
Subcatchment ES3A:	Runoff Area=115,072 sf 0.00% Impervious Runoff Depth=0.32" Flow Length=210' Tc=22.4 min CN=57 Runoff=0.3 cfs 3,099 cf
SubcatchmentES4:	Runoff Area=420,097 sf 0.00% Impervious Runoff Depth=0.46" Flow Length=650' Tc=19.7 min CN=61 Runoff=2.3 cfs 16,119 cf
Subcatchment ES5:	Runoff Area=301,140 sf 0.00% Impervious Runoff Depth=0.42" Flow Length=230' Tc=19.4 min CN=60 Runoff=1.5 cfs 10,641 cf
Subcatchment ES5A:	Runoff Area=168,926 sf 0.00% Impervious Runoff Depth=0.39" Flow Length=180' Tc=18.9 min CN=59 Runoff=0.7 cfs 5,476 cf
Reach DP1: Parker River	Inflow=1.4 cfs 10,971 cf Outflow=1.4 cfs 10,971 cf
Reach DP2:	Inflow=1.2 cfs 8,949 cf Outflow=1.2 cfs 8,949 cf
Reach DP2A:	Inflow=0.5 cfs 2,970 cf Outflow=0.5 cfs 2,970 cf
Reach DP3:	Inflow=1.0 cfs 8,298 cf Outflow=1.0 cfs 8,298 cf
Reach DP3A:	Inflow=0.3 cfs 3,099 cf Outflow=0.3 cfs 3,099 cf
Reach DP4:	Inflow=2.3 cfs 16,119 cf Outflow=2.3 cfs 16,119 cf
Reach DP5:	Inflow=2.2 cfs 16,117 cf Outflow=2.2 cfs 16,117 cf
Reach DP5A:	Inflow=0.7 cfs 5,476 cf Outflow=0.7 cfs 5,476 cf

Total Runoff Area = 1,789,987 sf Runoff Volume = 60,455 cf Average Runoff Depth = 0.41" 100.00% Pervious = 1,789,987 sf 0.00% Impervious = 0 sf

Summary for Subcatchment ES1:

1.4 cfs @ 12.50 hrs, Volume= Runoff 10,971 cf, Depth= 0.39" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"

	Α	rea (sf)	CN [Description					
	2	00,998	61 >	75% Gras	s cover, Go	ood, HSG B			
	1	37,409	55 \	Noods, Good, HSG B					
	3	38,407	59 \	Veighted A	verage				
	3	38,407		00.00% Pe	ervious Are	а			
	_				- ··				
,	Τc	Length	Slope	Velocity	Capacity	Description			
(r	min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
2	21.8	50	0.0200	0.04		Sheet Flow,			
						Woods: Dense underbrush n= 0.800 P2= 3.10"			
	1.6	300	0.0400	3.22		Shallow Concentrated Flow,			
						Unpaved Kv= 16.1 fps			
2	23.4	350	Total						

Summary for Subcatchment ES2:

Runoff	_	0.8 cfs @	12 37 hrs	Volume-	5,979 cf, Depth= 0	36"
RUNOII	-	0.0 CIS (W)	12.37 1115,	volume-	3,979 CI, Depin- 0	.30

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"

_	A	rea (sf)	CN E	Description						
	1	00,828	61 >	>75% Grass cover, Good, HSG B						
_	1	01,071	55 V	Voods, Go	od, HSG B					
	2	01,899	58 V	Veighted A	verage					
201,899 100.00% Pervious Area										
	Тс	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	11.5	50	0.1000	0.07		Sheet Flow,				
						Woods: Dense underbrush n= 0.800 P2= 3.10"				
	2.3	565	0.0670	4.17		Shallow Concentrated Flow,				
_						Unpaved Kv= 16.1 fps				
_	10.0	C1E	Tatal							

13.8 615 Total

Summary for Subcatchment ES2A:

Runoff = 0.5 cfs @ 12.28 hrs, Volume= 2,970 cf, Depth= 0.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"

Willow Road Existing Conditions

Type III 24-hr 2 Year Rainfall=3.24" Printed 11/18/2020 LLC Page 8

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_	A	rea (sf)	CN I	Description					
		63,556	61 🗧	>75% Gras	s cover, Go	ood, HSG B			
_		20,495	55	Noods, Go	od, HSG B				
		84,051	60	Weighted Average					
		84,051		100.00% Pe	ervious Are	a			
	Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description			
	13.2	50	0.0700	0.06		Sheet Flow,			
	0.3	100	0.1000	5.09		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
	13.5	150	Total						

Summary for Subcatchment ES3:

Runoff = 0.7 cfs @ 12.38 hrs, Volume= 5,200 cf, Depth= 0.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"

_	A	rea (sf)	CN [Description						
	1	06,813	61 >	75% Gras	s cover, Go	ood, HSG B				
_		53,582	55 V	Voods, Go	od, HSG B					
	1	60,395	59 V	Veighted A	verage					
	1	60,395	1	00.00% Pe	ervious Are	a				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
_	14.1	50	0.0600	0.06		Sheet Flow,				
	2.7	490	0.0350	3.01		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
_	16.8	540	Total							

Summary for Subcatchment ES3A:

Runoff = 0.3 cfs @ 12.52 hrs, Volume= 3,099 cf, Depth= 0.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"

A	Area (sf)	CN	Description			
	36,688	61	>75% Grass cover, Good, HSG B			
	78,384	55	Woods, Good, HSG B			
	115,072	57	Weighted Average			
	115,072		100.00% Pervious Area			

			Conditio	ons Group, Inc	Type III 24-hr 2 Year Rainfall=3.24" Printed 11/18/2020	
) Software Solutions LLC Page 9	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
21.8	50	0.0200	0.04		Sheet Flow,	
0.6	160	0.0750	4.41		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps	
22.4	210	Total				
			0			
			Sun	nmary toi	r Subcatchment ES4:	
Runoff	=	2.3 c	fs @ 12.3	89 hrs, Volu	ume= 16,119 cf, Depth= 0.46"	
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"						
A	rea (sf)	CN D)escription			
4	09,301	61 >	75% Gras		ood, HSG B	
	10,796			od, HSG B		
	20,097 20,097		Veighted A 00.00% Pe	verage ervious Are	а	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
16.5	50	0.0400	0.05		Sheet Flow,	
3.2	600	0.0380	3.14		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps	
19.7	650	Total				
			Sun	nmary foi	r Subcatchment ES5:	
Runoff	=	1.5 c	fs @ 12.4	0 hrs, Volu	ume= 10,641 cf, Depth= 0.42"	
			nod, UH=S fall=3.24"	CS, Weigh	ted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs	
A	rea (sf)	CN D	escription			
	30,675				ood, HSG B	
	70,465			od, HSG B		
	01,140 01,140		Veighted A 00.00% Pe	ervious Are	а	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
18.6	50	0.0300	0.04		Sheet Flow,	
0.8	100	0.0500	3 60		Woods: Dense underbrush n= 0.800 P2= 3.10"	

Shallow Concentrated Flow, Unpaved Kv= 16.1 fps

19.4 230 Total

180 0.0500

3.60

0.8

Summary for Subcatchment ES5A:

Runoff = 0.7 cfs @ 12.42 hrs, Volume= 5,476 cf, Depth= 0.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"

_	A	rea (sf)	CN E	Description					
	1	03,925	61 >	>75% Grass cover, Good, HSG B					
_		65,001	55 V	Voods, Go	od, HSG B				
168,926 59 Weighted Average									
168,926 100.00% Pervious Area					а				
	Tc	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	18.6	50	0.0300	0.04		Sheet Flow,			
						Woods: Dense underbrush n= 0.800 P2= 3.10"			
	0.3	130	0.1600	6.44		Shallow Concentrated Flow,			
_						Unpaved Kv= 16.1 fps			
	10 0	100	Total						

18.9 180 Total

Summary for Reach DP1: Parker River

Inflow Area =	338,407 sf,	0.00% Impervious,	Inflow Depth = 0.39"	for 2 Year event
Inflow =	1.4 cfs @	12.50 hrs, Volume=	10,971 cf	
Outflow =	1.4 cfs @	12.50 hrs, Volume=	10,971 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2:

Inflow Area =	285,950 sf,	0.00% Impervious,	Inflow Depth = 0.38"	for 2 Year event
Inflow =	1.2 cfs @	12.34 hrs, Volume=	8,949 cf	
Outflow =	1.2 cfs @	12.34 hrs, Volume=	8,949 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2A:

Inflow Area	a =	84,051 sf,	0.00% Impervious,	Inflow Depth = 0.4	42" for 2 Year event
Inflow	=	0.5 cfs @	12.28 hrs, Volume=	2,970 cf	
Outflow	=	0.5 cfs @	12.28 hrs, Volume=	2,970 cf,	Atten= 0%, Lag= 0.0 min

Summary for Reach DP3:

Inflow Area =	275,467 sf,	0.00% Impervious,	Inflow Depth = 0.36"	for 2 Year event
Inflow =	1.0 cfs @	12.45 hrs, Volume=	8,298 cf	
Outflow =	1.0 cfs @	12.45 hrs, Volume=	8,298 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3A:

Inflow Area =	115,072 sf,	0.00% Impervious,	Inflow Depth = 0.32"	for 2 Year event
Inflow =	0.3 cfs @	12.52 hrs, Volume=	3,099 cf	
Outflow =	0.3 cfs @	12.52 hrs, Volume=	3,099 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP4:

Inflow Area	=	420,097 sf,	0.00% Impervious,	Inflow Depth = 0.46	for 2 Year event
Inflow	=	2.3 cfs @	12.39 hrs, Volume=	16,119 cf	
Outflow	=	2.3 cfs @	12.39 hrs, Volume=	16,119 cf, At	ten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5:

Inflow Area =		470,066 sf,	0.00% Impervious,	Inflow Depth = 0.41 "	for 2 Year event
Inflow =	:	2.2 cfs @	12.41 hrs, Volume=	16,117 cf	
Outflow =	:	2.2 cfs @	12.41 hrs, Volume=	16,117 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5A:

Inflow Area =	168,926 sf,	0.00% Impervious,	Inflow Depth = 0.39"	for 2 Year event
Inflow =	0.7 cfs @	12.42 hrs, Volume=	5,476 cf	
Outflow =	0.7 cfs @	12.42 hrs, Volume=	5,476 cf, Atte	n= 0%, Lag= 0.0 min

Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment ES1:	Runoff Area=338,407 sf 0.00% Impervious Runoff Depth=1.30" Flow Length=350' Tc=23.4 min CN=59 Runoff=6.6 cfs 36,743 cf
Subcatchment ES2:	Runoff Area=201,899 sf 0.00% Impervious Runoff Depth=1.24" Flow Length=615' Tc=13.8 min CN=58 Runoff=4.5 cfs 20,785 cf
Subcatchment ES2A:	Runoff Area=84,051 sf 0.00% Impervious Runoff Depth=1.37" Flow Length=150' Tc=13.5 min CN=60 Runoff=2.2 cfs 9,608 cf
Subcatchment ES3:	Runoff Area=160,395 sf 0.00% Impervious Runoff Depth=1.30" Flow Length=540' Tc=16.8 min CN=59 Runoff=3.6 cfs 17,415 cf
Subcatchment ES3A:	Runoff Area=115,072 sf 0.00% Impervious Runoff Depth=1.17" Flow Length=210' Tc=22.4 min CN=57 Runoff=2.0 cfs 11,211 cf
Subcatchment ES4:	Runoff Area=420,097 sf 0.00% Impervious Runoff Depth=1.44" Flow Length=650' Tc=19.7 min CN=61 Runoff=10.0 cfs 50,472 cf
Subcatchment ES5:	Runoff Area=301,140 sf 0.00% Impervious Runoff Depth=1.37" Flow Length=230' Tc=19.4 min CN=60 Runoff=6.8 cfs 34,423 cf
Subcatchment ES5A:	Runoff Area=168,926 sf 0.00% Impervious Runoff Depth=1.30" Flow Length=180' Tc=18.9 min CN=59 Runoff=3.6 cfs 18,341 cf
Reach DP1: Parker River	Inflow=6.6 cfs 36,743 cf Outflow=6.6 cfs 36,743 cf
Reach DP2:	Inflow=6.7 cfs 30,392 cf Outflow=6.7 cfs 30,392 cf
Reach DP2A:	Inflow=2.2 cfs 9,608 cf Outflow=2.2 cfs 9,608 cf
Reach DP3:	Inflow=5.4 cfs 28,625 cf Outflow=5.4 cfs 28,625 cf
Reach DP3A:	Inflow=2.0 cfs 11,211 cf Outflow=2.0 cfs 11,211 cf
Reach DP4:	Inflow=10.0 cfs 50,472 cf Outflow=10.0 cfs 50,472 cf
Reach DP5:	Inflow=10.4 cfs 52,764 cf Outflow=10.4 cfs 52,764 cf
Reach DP5A:	Inflow=3.6 cfs 18,341 cf Outflow=3.6 cfs 18,341 cf

Total Runoff Area = 1,789,987 sf Runoff Volume = 198,997 cf Average Runoff Depth = 1.33" 100.00% Pervious = 1,789,987 sf 0.00% Impervious = 0 sf

Summary for Subcatchment ES1:

Runoff = 6.6 cfs @ 12.37 hrs, Volume= 36,743 cf, Depth= 1.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"

_	A	rea (sf)	CN [Description					
	200,998 61 >75% Grass cover, Good, HSG B								
_	1	37,409	55 N	Voods, Go	od, HSG B				
	3	38,407	59 V	Veighted A	verage				
338,407 100.00% Pervious Area					ervious Are	а			
	Тс	Length	Slope		Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	21.8	50	0.0200	0.04		Sheet Flow,			
						Woods: Dense underbrush n= 0.800 P2= 3.10"			
	1.6	300	0.0400	3.22		Shallow Concentrated Flow,			
_						Unpaved Kv= 16.1 fps			
	23.4	350	Total						

Summary for Subcatchment ES2:

Runoff	=	4.5 cfs @	12.22 hrs.	Volume=	20,785 cf, Depth= 1.24"
1 turion		-1.0 010 (W)	12.22110,	Volumo	

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"

_	A	rea (sf)	CN E	Description					
	1	00,828	00,828 61 >75% Grass cover, Good, HSG B						
_	1	01,071	55 V	Voods, Goo	od, HSG B				
	2	01,899	58 V	Veighted A	verage				
201,899 100.00% Pervious Area						а			
	Tc	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	11.5	50	0.1000	0.07		Sheet Flow,			
						Woods: Dense underbrush n= 0.800 P2= 3.10"			
	2.3	565	0.0670	4.17		Shallow Concentrated Flow,			
_						Unpaved Kv= 16.1 fps			
_	40.0	045	Tatal						

13.8 615 Total

Summary for Subcatchment ES2A:

Runoff = 2.2 cfs @ 12.20 hrs, Volume= 9,608 cf, Depth= 1.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"

Willow Road Existing Conditions Prepared by The Morin-Cameron Group, Inc.

Type III 24-hr 10 Year Rainfall=5.12" Printed 11/18/2020 HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLC Page 15

_	A	rea (sf)	CN I	Description						
		63,556			75% Grass cover, Good, HSG B					
_		20,495	55	Woods, Go	<u>od, HSG B</u>					
84,051 60 Weighted Average										
		84,051		100.00% Pe	ervious Are	a				
	Tc	Length	Slope		Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	13.2	50	0.0700	0.06		Sheet Flow,				
						Woods: Dense underbrush n= 0.800 P2= 3.10"				
	0.3	100	0.1000	5.09		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				
_										

150 Total 13.5

Summary for Subcatchment ES3:

3.6 cfs @ 12.26 hrs, Volume= 17,415 cf, Depth= 1.30" Runoff =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"

_	A	rea (sf)	CN [Description					
	1	06,813	61 >	>75% Grass cover, Good, HSG B					
_		53,582	55 \	Noods, Go	od, HSG B				
160,395 59 Weighted Average									
	1	60,395		100.00% Pe	ervious Are	a			
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
-	14.1	50	0.0600	0.06		Sheet Flow,			
	2.7	490	0.0350	3.01		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
_	16.8	540	Total						

Summary for Subcatchment ES3A:

2.0 cfs @ 12.37 hrs, Volume= 11,211 cf, Depth= 1.17" Runoff =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"

Are	ea (sf)	CN	Description
3	6,688	61	>75% Grass cover, Good, HSG B
7	8,384	55	Woods, Good, HSG B
11	5,072	57	Weighted Average
11	5,072		100.00% Pervious Area

Prepared by The Morin-Cameron Group, Inc.Printed 11/18/202HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLCPage 1TcLengthSlopeVelocityCapacityDescription(min)(feet)(ft/ft)(ft/sec)(cfs)Description21.8500.02000.04Sheet Flow, Woods: Dense underbrush n= 0.800 P2= 3.10"0.61600.07504.41Shallow Concentrated Flow, Unpaved Kv= 16.1 fps22.4210TotalSummary for Subcatchment ES4:				
TcLengthSlopeVelocityCapacityDescription(min)(feet)(ft/ft)(ft/sec)(cfs)Description21.8500.02000.04Sheet Flow, Woods: Dense underbrush n= 0.800 P2= 3.10"0.61600.07504.41Shallow Concentrated Flow, Unpaved Kv= 16.1 fps22.4210Total				
(min) (feet) (ft/ft) (ft/sec) (cfs) 21.8 50 0.0200 0.04 Sheet Flow, Woods: Dense underbrush n= 0.800 P2= 3.10" 0.6 160 0.0750 4.41 Shallow Concentrated Flow, Unpaved Kv= 16.1 fps 22.4 210 Total Total				
0.6 160 0.0750 4.41 Woods: Dense underbrush n= 0.800 P2= 3.10" 22.4 210 Total Unpaved Kv= 16.1 fps				
0.6 160 0.0750 4.41 Shallow Concentrated Flow, Unpaved Unpaved Kv= 16.1 fps 22.4 210 Total Total				
Summary for Subcatchment ES4:				
Summary for Subcatchment ES4:				
Runoff = 10.0 cfs @ 12.30 hrs, Volume= 50,472 cf, Depth= 1.44"				
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"				
Area (sf) CN Description				
409,301 61 >75% Grass cover, Good, HSG B				
10,796 55 Woods, Good, HSG B				
420,09761Weighted Average420,097100.00% Pervious Area				
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)				
16.5 50 0.0400 0.05 Sheet Flow,				
3.26000.03803.14Woods: Dense underbrushn= 0.800P2= 3.10"Shallow Concentrated Flow, UnpavedKv= 16.1 fps				
19.7 650 Total				
Summary for Subcatchment ES5:				
Runoff = 6.8 cfs @ 12.31 hrs, Volume= 34,423 cf, Depth= 1.37"				
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"				
Area (sf) CN Description				
230,675 61 >75% Grass cover, Good, HSG B 70,465 55 Woods, Good, HSG B				
301,140 60 Weighted Average 301,140 100.00% Pervious Area				
Tc Length Slope Velocity Capacity Description _(min) (feet) (ft/ft) (ft/sec) (cfs)				
18.6 50 0.0300 0.04 Sheet Flow,				
0.8 180 0.0500 3.60 Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
19.4 230 Total				

Summary for Subcatchment ES5A:

Runoff = 3.6 cfs @ 12.29 hrs, Volume= 18,341 cf, Depth= 1.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"

	A	rea (sf)	CN I	Description						
_	1	03,925	61 >	>75% Grass cover, Good, HSG B						
_		65,001	55 \	Noods, Go	od, HSG B					
	1	68,926	59 \	Neighted A	verage					
168,926 100.00% Pervious Area						a				
_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
	18.6	50	0.0300	0.04		Sheet Flow,				
	0.3	130	0.1600	6.44		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
_	10.0	100	Total							

18.9 180 Total

Summary for Reach DP1: Parker River

Inflow Area =	338,407 sf,	0.00% Impervious,	Inflow Depth = 1.30"	for 10 Year event
Inflow =	6.6 cfs @	12.37 hrs, Volume=	36,743 cf	
Outflow =	6.6 cfs @	12.37 hrs, Volume=	36,743 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2:

Inflow Area =	285,950 sf,	0.00% Impervious,	Inflow Depth = 1.28"	for 10 Year event
Inflow =	6.7 cfs @	12.21 hrs, Volume=	30,392 cf	
Outflow =	6.7 cfs @	12.21 hrs, Volume=	30,392 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2A:

Inflow Area	a =	84,051 sf,	0.00% Impervious,	Inflow Depth = 1.37"	for 10 Year event
Inflow	=	2.2 cfs @	12.20 hrs, Volume=	9,608 cf	
Outflow	=	2.2 cfs @	12.20 hrs, Volume=	9,608 cf, Atte	en= 0%, Lag= 0.0 min

Summary for Reach DP3:

Inflow Area =	275,467 sf,	0.00% Impervious,	Inflow Depth = 1.25 "	for 10 Year event
Inflow =	5.4 cfs @	12.30 hrs, Volume=	28,625 cf	
Outflow =	5.4 cfs @	12.30 hrs, Volume=	28,625 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3A:

Inflow Area =	115,072 sf,	0.00% Impervious,	Inflow Depth = 1.17"	for 10 Year event
Inflow =	2.0 cfs @	12.37 hrs, Volume=	11,211 cf	
Outflow =	2.0 cfs @	12.37 hrs, Volume=	11,211 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP4:

Inflow Area =	420,097 sf,	0.00% Impervious,	Inflow Depth = 1.44"	for 10 Year event
Inflow =	10.0 cfs @	12.30 hrs, Volume=	50,472 cf	
Outflow =	10.0 cfs @	12.30 hrs, Volume=	50,472 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5:

Inflow Area =	470,066 sf,	0.00% Impervious,	Inflow Depth = 1.35"	for 10 Year event
Inflow =	10.4 cfs @	12.30 hrs, Volume=	52,764 cf	
Outflow =	10.4 cfs @	12.30 hrs, Volume=	52,764 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5A:

Inflow Area	=	168,926 sf,	0.00% Impervious,	Inflow Depth = 1.30 "	for 10 Year event
Inflow =	=	3.6 cfs @	12.29 hrs, Volume=	18,341 cf	
Outflow =	=	3.6 cfs @	12.29 hrs, Volume=	18,341 cf, Atte	en= 0%, Lag= 0.0 min

Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

SubcatchmentES1:	Runoff Area=338,407 sf 0.00% Impervious Runoff Depth=2.03" Flow Length=350' Tc=23.4 min CN=59 Runoff=11.0 cfs 57,146 cf
Subcatchment ES2:	Runoff Area=201,899 sf 0.00% Impervious Runoff Depth=1.94" Flow Length=615' Tc=13.8 min CN=58 Runoff=7.6 cfs 32,642 cf
Subcatchment ES2A:	Runoff Area=84,051 sf 0.00% Impervious Runoff Depth=2.11" Flow Length=150' Tc=13.5 min CN=60 Runoff=3.6 cfs 14,805 cf
SubcatchmentES3:	Runoff Area=160,395 sf 0.00% Impervious Runoff Depth=2.03" Flow Length=540' Tc=16.8 min CN=59 Runoff=5.9 cfs 27,086 cf
SubcatchmentES3A:	Runoff Area=115,072 sf 0.00% Impervious Runoff Depth=1.85" Flow Length=210' Tc=22.4 min CN=57 Runoff=3.4 cfs 17,786 cf
SubcatchmentES4:	Runoff Area=420,097 sf 0.00% Impervious Runoff Depth=2.20" Flow Length=650' Tc=19.7 min CN=61 Runoff=16.1 cfs 77,088 cf
Subcatchment ES5:	Runoff Area=301,140 sf 0.00% Impervious Runoff Depth=2.11" Flow Length=230' Tc=19.4 min CN=60 Runoff=11.1 cfs 53,044 cf
Subcatchment ES5A:	Runoff Area=168,926 sf 0.00% Impervious Runoff Depth=2.03" Flow Length=180' Tc=18.9 min CN=59 Runoff=6.0 cfs 28,526 cf
Reach DP1: Parker River	Inflow=11.0 cfs 57,146 cf Outflow=11.0 cfs 57,146 cf
Reach DP2:	Inflow=11.2 cfs 47,447 cf Outflow=11.2 cfs 47,447 cf
Reach DP2A:	Inflow=3.6 cfs 14,805 cf Outflow=3.6 cfs 14,805 cf
Reach DP3:	Inflow=9.1 cfs 44,872 cf Outflow=9.1 cfs 44,872 cf
Reach DP3A:	Inflow=3.4 cfs 17,786 cf Outflow=3.4 cfs 17,786 cf
Reach DP4:	Inflow=16.1 cfs 77,088 cf Outflow=16.1 cfs 77,088 cf
Reach DP5:	Inflow=17.0 cfs 81,570 cf Outflow=17.0 cfs 81,570 cf
Reach DP5A:	Inflow=6.0 cfs 28,526 cf Outflow=6.0 cfs 28,526 cf

Total Runoff Area = 1,789,987 sf Runoff Volume = 308,122 cf Average Runoff Depth = 2.07" 100.00% Pervious = 1,789,987 sf 0.00% Impervious = 0 sf

Summary for Subcatchment ES1:

Runoff = 11.0 cfs @ 12.35 hrs, Volume= 57,146 cf, Depth= 2.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

_	A	rea (sf)	CN [Description		
	2	00,998	61 >	>75% Gras	s cover, Go	ood, HSG B
_	1	37,409	55 \	Noods, Go	od, HSG B	
338,407 59 Weighted Average						
	3	38,407		100.00% Pe	ervious Are	а
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	21.8	50	0.0200	0.04		Sheet Flow,
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	1.6	300	0.0400	3.22		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
_	23.4	350	Total			

Summary for Subcatchment ES2:

Runoff	=	7.6 cfs @	12.20 hrs.	Volume=	32,642 cf, Depth= 1.94"
T CULION		1.0 013 (W)	12.201113,	volume-	02,04201, 000011 - 1.04

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

	A	rea (sf)	CN E	Description		
	1	00,828	61 >	75% Gras	s cover, Go	ood, HSG B
_	1	01,071	55 V	Voods, Go	od, HSG B	
	2	01,899	58 V	Veighted A	verage	
201,899 100.00% Pervious Area						a
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	11.5	50	0.1000	0.07		Sheet Flow,
	2.3	565	0.0670	4.17		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
	12.0	615	Tatal			

13.8 615 Total

Summary for Subcatchment ES2A:

Runoff = 3.6 cfs @ 12.20 hrs, Volume= 14,805 cf, Depth= 2.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

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Type III 24-hr 25 Year Rainfall=6.29" Printed 11/18/2020 HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLC Page 22

_	А	rea (sf)	CN	Description		
		63,556	61	>75% Gras	s cover, Go	bod, HSG B
_		20,495	55	Woods, Go	od, HSG B	
84,051 60 Weighted Average						
84,051 100.00% Pervious Area						а
_	Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
	13.2	50	0.0700	0.06		Sheet Flow,
	0.3	100	0.1000) 5.09		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps

13.5 150 Total

Summary for Subcatchment ES3:

5.9 cfs @ 12.25 hrs, Volume= 27,086 cf, Depth= 2.03" Runoff =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

_	A	rea (sf)	CN [Description		
	1	06,813	61 >	75% Gras	s cover, Go	ood, HSG B
_		53,582	55 V	Voods, Go	od, HSG B	
	1	160,395 59 Weighted Average				
	160,395 100.00% Pervious Area					a
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	14.1	50	0.0600	0.06		Sheet Flow,
	2.7	490	0.0350	3.01		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
_	16.8	540	Total			

Summary for Subcatchment ES3A:

3.4 cfs @ 12.34 hrs, Volume= 17,786 cf, Depth= 1.85" Runoff =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

Area (sf) CN	Description
36,6	88 61	>75% Grass cover, Good, HSG B
78,3	84 55	Woods, Good, HSG B
115,0	72 57	Weighted Average
115,0	72	100.00% Pervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.8	50	0.0200	0.04	· · ·	Sheet Flow,
0.6	160	0.0750	4.41		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
22.4	210	Total			
			Sun	nmary for	r Subcatchment ES4:
Runoff	=	16.1 c	fs @ 12.2	28 hrs, Vol	ume= 77,088 cf, Depth= 2.20"
			hod, UH=S nfall=6.29"		ted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs
А	rea (sf)	CN E	Description		
	09,301			s cover. Go	ood, HSG B
	10,796			od, HSG B	
	20,097 20,097		Veighted A 00.00% Pe	verage ervious Are	a
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.5	50	0.0400	0.05	· · ·	Sheet Flow,
3.2	600	0.0380	3.14		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unproved Ky= 16.1 fps
19.7	650	Total			Unpaved Kv= 16.1 fps
	000	i otai			
			Sun	nmary for	r Subcatchment ES5:
Runoff	=	11.1 c	fs @ 12.2	9 hrs, Vol	ume= 53,044 cf, Depth= 2.11"
			hod, UH=S nfall=6.29"		ted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs
Δ	rea (sf)	CN E	Description		
	30,675			s cover Go	ood, HSG B
	70,465			od, HSG B	
3	01,140 01,140	60 V	Veighted A		a
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
18.6	50	0.0300	0.04	()	Sheet Flow,
0.8		0 0500	3 60		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow

Shallow Concentrated Flow, Unpaved Kv= 16.1 fps

19.4 230 Total

0.8

180 0.0500

3.60

Summary for Subcatchment ES5A:

Runoff = 6.0 cfs @ 12.28 hrs, Volume= 28,526 cf, Depth= 2.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

_	A	rea (sf)	CN E	Description					
	1	03,925	61 >	75% Gras	s cover, Go	ood, HSG B			
_		65,001	55 V	Voods, Go	od, HSG B				
	1	68,926	8,926 59 Weighted Average						
	1	68,926	1	00.00% Pe	ervious Are	а			
	_				- ··				
	Tc	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	18.6	50	0.0300	0.04		Sheet Flow,			
						Woods: Dense underbrush n= 0.800 P2= 3.10"			
	0.3	130	0.1600	6.44		Shallow Concentrated Flow,			
_						Unpaved Kv= 16.1 fps			
	10 0	100	Total						

18.9 180 Total

Summary for Reach DP1: Parker River

Inflow Area =	338,407 sf,	0.00% Impervious,	Inflow Depth = 2.03"	for 25 Year event
Inflow =	11.0 cfs @	12.35 hrs, Volume=	57,146 cf	
Outflow =	11.0 cfs @	12.35 hrs, Volume=	57,146 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2:

Inflow Area =	285,950 sf,	0.00% Impervious,	Inflow Depth = 1.99"	for 25 Year event
Inflow =	11.2 cfs @	12.20 hrs, Volume=	47,447 cf	
Outflow =	11.2 cfs @	12.20 hrs, Volume=	47,447 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2A:

Inflow Area	a =	84,051 sf,	0.00% Impervious,	Inflow Depth = 2.11"	for 25 Year event
Inflow	=	3.6 cfs @	12.20 hrs, Volume=	14,805 cf	
Outflow	=	3.6 cfs @	12.20 hrs, Volume=	14,805 cf, Att	en= 0%, Lag= 0.0 min

Summary for Reach DP3:

Inflow Area =	275,467 sf,	0.00% Impervious,	Inflow Depth = 1.95 "	for 25 Year event
Inflow =	9.1 cfs @	12.27 hrs, Volume=	44,872 cf	
Outflow =	9.1 cfs @	12.27 hrs, Volume=	44,872 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3A:

Inflow Area =	115,072 sf,	0.00% Impervious,	Inflow Depth = 1.85"	for 25 Year event
Inflow =	3.4 cfs @	12.34 hrs, Volume=	17,786 cf	
Outflow =	3.4 cfs @	12.34 hrs, Volume=	17,786 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP4:

Inflow Area =	420,097 sf,	0.00% Impervious,	Inflow Depth = 2.20"	for 25 Year event
Inflow =	16.1 cfs @	12.28 hrs, Volume=	77,088 cf	
Outflow =	16.1 cfs @	12.28 hrs, Volume=	77,088 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5:

Inflow Area	a =	470,066 sf,	0.00% Impervious,	Inflow Depth = 2.08	for 25 Year event
Inflow	=	17.0 cfs @	12.29 hrs, Volume=	81,570 cf	
Outflow	=	17.0 cfs @	12.29 hrs, Volume=	81,570 cf, At	tten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5A:

Inflow Area	a =	168,926 sf,	0.00% Impervious,	Inflow Depth = 2.03"	for 25 Year event
Inflow	=	6.0 cfs @	12.28 hrs, Volume=	28,526 cf	
Outflow	=	6.0 cfs @	12.28 hrs, Volume=	28,526 cf, Atte	en= 0%, Lag= 0.0 min

Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment ES1:	Runoff Area=338,407 sf 0.00% Impervious Runoff Depth=2.61" Flow Length=350' Tc=23.4 min CN=59 Runoff=14.5 cfs 73,622 cf
Subcatchment ES2:	Runoff Area=201,899 sf 0.00% Impervious Runoff Depth=2.51" Flow Length=615' Tc=13.8 min CN=58 Runoff=10.2 cfs 42,260 cf
Subcatchment ES2A:	Runoff Area=84,051 sf 0.00% Impervious Runoff Depth=2.71" Flow Length=150' Tc=13.5 min CN=60 Runoff=4.7 cfs 18,984 cf
Subcatchment ES3:	Runoff Area=160,395 sf 0.00% Impervious Runoff Depth=2.61" Flow Length=540' Tc=16.8 min CN=59 Runoff=7.8 cfs 34,895 cf
Subcatchment ES3A:	Runoff Area=115,072 sf 0.00% Impervious Runoff Depth=2.41" Flow Length=210' Tc=22.4 min CN=57 Runoff=4.6 cfs 23,145 cf
Subcatchment ES4:	Runoff Area=420,097 sf 0.00% Impervious Runoff Depth=2.81" Flow Length=650' Tc=19.7 min CN=61 Runoff=21.0 cfs 98,397 cf
Subcatchment ES5:	Runoff Area=301,140 sf 0.00% Impervious Runoff Depth=2.71" Flow Length=230' Tc=19.4 min CN=60 Runoff=14.5 cfs 68,015 cf
Subcatchment ES5A:	Runoff Area=168,926 sf 0.00% Impervious Runoff Depth=2.61" Flow Length=180' Tc=18.9 min CN=59 Runoff=7.9 cfs 36,751 cf
Reach DP1: Parker River	Inflow=14.5 cfs 73,622 cf Outflow=14.5 cfs 73,622 cf
Reach DP2:	Inflow=14.8 cfs 61,243 cf Outflow=14.8 cfs 61,243 cf
Reach DP2A:	Inflow=4.7 cfs 18,984 cf Outflow=4.7 cfs 18,984 cf
Reach DP3:	Inflow=12.1 cfs 58,039 cf Outflow=12.1 cfs 58,039 cf
Reach DP3A:	Inflow=4.6 cfs 23,145 cf Outflow=4.6 cfs 23,145 cf
Reach DP4:	Inflow=21.0 cfs 98,397 cf Outflow=21.0 cfs 98,397 cf
Reach DP5:	Inflow=22.4 cfs 104,766 cf Outflow=22.4 cfs 104,766 cf
Reach DP5A:	Inflow=7.9 cfs 36,751 cf Outflow=7.9 cfs 36,751 cf

Total Runoff Area = 1,789,987 sf Runoff Volume = 396,067 cf Average Runoff Depth = 2.66" 100.00% Pervious = 1,789,987 sf 0.00% Impervious = 0 sf

Summary for Subcatchment ES1:

Page 28

14.5 cfs @ 12.35 hrs, Volume= Runoff = 73,622 cf, Depth= 2.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

_	A	rea (sf)	CN [Description		
	2	00,998	61 >	75% Gras	s cover, Go	ood, HSG B
_	1	37,409	55 \	Voods, Go	od, HSG B	
	338,407 59 Weighted Average					
	3	38,407		00.00% Pe	ervious Are	а
		Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	21.8	50	0.0200	0.04		Sheet Flow,
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	1.6	300	0.0400	3.22		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
_	23.4	350	Total			

Summary for Subcatchment ES2:

D			10.00 1	V / - 1	
Runoff	=	10.2 cfs @	12.20 nrs,	volume=	42,260 cf, Depth= 2.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

_	A	rea (sf)	CN E	Description					
	1	00,828	61 >	75% Gras	s cover, Go	bod, HSG B			
_	1	01,071	55 V	Woods, Good, HSG B					
	201,899 58 Weighted Average								
201,899 100.00% Pervious Area				а					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	11.5	50	0.1000	0.07		Sheet Flow,			
	2.3	565	0.0670	4.17		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
_	10.0	C1E	Tatal						

13.8 615 Total

Summary for Subcatchment ES2A:

Runoff = 4.7 cfs @ 12.19 hrs, Volume= 18,984 cf, Depth= 2.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

Willow Road Existing Conditions

 Type III 24-hr
 50 Year Rainfall=7.15"

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 11/18/2020

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 Page 29

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_	A	rea (sf)	CN	Description				
		63,556 61 >75% Grass cover, Good, HSG B						
_		20,495	55	Woods, Go	od, HSG B			
		84,051	60	Weighted A	verage			
		84,051		100.00% Pe	ervious Are	а		
	Tc	Length	Slope		Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	13.2	50	0.0700	0.06		Sheet Flow,		
						Woods: Dense underbrush n= 0.800 P2= 3.10"		
	0.3	100	0.1000	5.09		Shallow Concentrated Flow,		
_						Unpaved Kv= 16.1 fps		
	13 5	150	Total					

13.5 150 Total

Summary for Subcatchment ES3:

Runoff = 7.8 cfs @ 12.24 hrs, Volume= 34,895 cf, Depth= 2.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

_	A	rea (sf)	CN [Description		
	1	06,813	61 >	75% Gras	s cover, Go	ood, HSG B
_		53,582	55 V	Voods, Go	od, HSG B	
	1	60,395	59 V	Veighted A	verage	
	1	60,395	1	00.00% Pe	ervious Are	a
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	14.1	50	0.0600	0.06		Sheet Flow,
	2.7	490	0.0350	3.01		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
_	16.8	540	Total			

Summary for Subcatchment ES3A:

Runoff = 4.6 cfs @ 12.33 hrs, Volume= 23,145 cf, Depth= 2.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

Area (sf)	CN	Description
36,688	61	>75% Grass cover, Good, HSG B
78,384	55	Woods, Good, HSG B
115,072 115,072	57	Weighted Average 100.00% Pervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
21.8	50	0.0200	0.04	· · · ·	Sheet Flow,		
0.6	160	0.0750	4.41		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps		
22.4	210	Total					
			Sun	nmary foi	r Subcatchment ES4:		
Runoff	=	21.0 cf	fs @ 12.2	28 hrs, Vol	ume= 98,397 cf, Depth= 2.81"		
			nod, UH=S nfall=7.15'		nted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs		
	rea (sf)		escription				
2	109,301 10,796			s cover, Go od, HSG B	bod, HSG B		
	120,097 120,097 120,097	61 V	Veighted A	· · ·			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
16.5	50	0.0400	0.05		Sheet Flow,		
3.2	600	0.0380	3.14		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps		
19.7	650	Total					
			Sun	nmary foi	r Subcatchment ES5:		
Runoff	=	14.5 ct	fs @ 12.2	28 hrs, Vol	ume= 68,015 cf, Depth= 2.71"		
			nod, UH=S nfall=7.15'		nted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs		
A	rea (sf)	CN D	escription				
2	230,675			,	bod, HSG B		
	<u>70,465</u> 301,140			od, HSG B			
	301,14060Weighted Average301,140100.00% Pervious Area						

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
18.6	50	0.0300	0.04		Sheet Flow,
					Woods: Dense underbrush n= 0.800 P2= 3.10"
0.8	180	0.0500	3.60		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
10 /	230	Total			

19.4 230 Total

Summary for Subcatchment ES5A:

Runoff = 7.9 cfs @ 12.28 hrs, Volume= 36,751 cf, Depth= 2.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

_	A	rea (sf)	CN E	Description		
	1	03,925	61 >	75% Gras	s cover, Go	ood, HSG B
_		65,001	55 V	Voods, Go	od, HSG B	
	1	68,926	59 V	Veighted A	verage	
	1	68,926	1	00.00% Pe	ervious Are	а
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	18.6	50	0.0300	0.04		Sheet Flow,
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	0.3	130	0.1600	6.44		Shallow Concentrated Flow,
_						Unpaved Kv= 16.1 fps
	10 0	100	Total			

18.9 180 Total

Summary for Reach DP1: Parker River

Inflow Area	a =	338,407 sf,	0.00% Impervious,	Inflow Depth = 2.61"	for 50 Year event
Inflow	=	14.5 cfs @	12.35 hrs, Volume=	73,622 cf	
Outflow	=	14.5 cfs @	12.35 hrs, Volume=	73,622 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2:

Inflow Area =		285,950 sf,	0.00% Impervious,	Inflow Depth = 2.57"	for 50 Year event
Inflow =	:	14.8 cfs @	12.20 hrs, Volume=	61,243 cf	
Outflow =	:	14.8 cfs @	12.20 hrs, Volume=	61,243 cf, Att	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2A:

Inflow Area	a =	84,051 sf,	0.00% Impervious,	Inflow Depth = 2.71 "	for 50 Year event
Inflow	=	4.7 cfs @	12.19 hrs, Volume=	18,984 cf	
Outflow	=	4.7 cfs @	12.19 hrs, Volume=	18,984 cf, Atte	en= 0%, Lag= 0.0 min

Summary for Reach DP3:

Inflow Area =	275,467 sf,	0.00% Impervious,	Inflow Depth = 2.53"	for 50 Year event
Inflow =	12.1 cfs @	12.27 hrs, Volume=	58,039 cf	
Outflow =	12.1 cfs @	12.27 hrs, Volume=	58,039 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3A:

Inflow Area =	115,072 sf,	0.00% Impervious,	Inflow Depth = 2.41"	for 50 Year event
Inflow =	4.6 cfs @	12.33 hrs, Volume=	23,145 cf	
Outflow =	4.6 cfs @	12.33 hrs, Volume=	23,145 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP4:

Inflow Area =		420,097 sf,	0.00% Impervious,	Inflow Depth = 2.81"	for 50 Year event
Inflow	=	21.0 cfs @	12.28 hrs, Volume=	98,397 cf	
Outflow	=	21.0 cfs @	12.28 hrs, Volume=	98,397 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5:

Inflow Area =		470,066 sf,	0.00% Impervious,	Inflow Depth = 2.67"	for 50 Year event
Inflow	=	22.4 cfs @	12.28 hrs, Volume=	104,766 cf	
Outflow	=	22.4 cfs @	12.28 hrs, Volume=	104,766 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5A:

Inflow Area	a =	168,926 sf,	0.00% Impervious,	Inflow Depth = 2.61"	for 50 Year event
Inflow	=	7.9 cfs @	12.28 hrs, Volume=	36,751 cf	
Outflow	=	7.9 cfs @	12.28 hrs, Volume=	36,751 cf, Atte	en= 0%, Lag= 0.0 min

Willow Road Existing Conditions	Type III 24-hr 100 Year Rainfall=8	.10"
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Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

SubcatchmentES1:	Runoff Area=338,407 sf 0.00% Impervious Runoff Depth=3.30" Flow Length=350' Tc=23.4 min CN=59 Runoff=18.5 cfs 92,960 cf
SubcatchmentES2:	Runoff Area=201,899 sf 0.00% Impervious Runoff Depth=3.18" Flow Length=615' Tc=13.8 min CN=58 Runoff=13.2 cfs 53,582 cf
SubcatchmentES2A:	Runoff Area=84,051 sf 0.00% Impervious Runoff Depth=3.41" Flow Length=150' Tc=13.5 min CN=60 Runoff=6.0 cfs 23,874 cf
SubcatchmentES3:	Runoff Area=160,395 sf 0.00% Impervious Runoff Depth=3.30" Flow Length=540' Tc=16.8 min CN=59 Runoff=10.1 cfs 44,060 cf
Subcatchment ES3A:	Runoff Area=115,072 sf 0.00% Impervious Runoff Depth=3.07" Flow Length=210' Tc=22.4 min CN=57 Runoff=5.9 cfs 29,473 cf
Subcatchment ES4:	Runoff Area=420,097 sf 0.00% Impervious Runoff Depth=3.52" Flow Length=650' Tc=19.7 min CN=61 Runoff=26.6 cfs 123,266 cf
Subcatchment ES5:	Runoff Area=301,140 sf 0.00% Impervious Runoff Depth=3.41" Flow Length=230' Tc=19.4 min CN=60 Runoff=18.5 cfs 85,537 cf
Subcatchment ES5A:	Runoff Area=168,926 sf 0.00% Impervious Runoff Depth=3.30" Flow Length=180' Tc=18.9 min CN=59 Runoff=10.1 cfs 46,404 cf
Reach DP1: Parker River	Inflow=18.5 cfs 92,960 cf Outflow=18.5 cfs 92,960 cf
Reach DP2:	Inflow=19.1 cfs 77,457 cf Outflow=19.1 cfs 77,457 cf
Reach DP2A:	Inflow=6.0 cfs 23,874 cf Outflow=6.0 cfs 23,874 cf
Reach DP3:	Inflow=15.6 cfs 73,533 cf Outflow=15.6 cfs 73,533 cf
Reach DP3A:	Inflow=5.9 cfs 29,473 cf Outflow=5.9 cfs 29,473 cf
Reach DP4:	Inflow=26.6 cfs 123,266 cf Outflow=26.6 cfs 123,266 cf
Reach DP5:	Inflow=28.6 cfs 131,941 cf Outflow=28.6 cfs 131,941 cf
Reach DP5A:	Inflow=10.1 cfs 46,404 cf Outflow=10.1 cfs 46,404 cf

Total Runoff Area = 1,789,987 sf Runoff Volume = 499,157 cf Average Runoff Depth = 3.35" 100.00% Pervious = 1,789,987 sf 0.00% Impervious = 0 sf

Page 34

Summary for Subcatchment ES1:

Runoff = 18.5 cfs @ 12.35 hrs, Volume= 92,960 cf, Depth= 3.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"

_	A	rea (sf)	CN I	Description		
	2	00,998	61 :	>75% Gras	s cover, Go	ood, HSG B
_	1	37,409	55	Noods, Go	od, HSG B	
	3	38,407		Neighted A		
	338,407 100.00% Pervious Area			100.00% Pe	ervious Are	a
	Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
_	21.8	50	0.0200	0.04		Sheet Flow,
	1.6	300	0.0400	3.22		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
	23.4	350	Total			

Summary for Subcatchment ES2:

Volume=	53,582 cf, Depth= 3.18"
,	, Volume=

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"

_	A	rea (sf)	CN E	Description		
	1	00,828	61 >	75% Gras	s cover, Go	bod, HSG B
101,071 55 Woods, Good, HSG B						
	201,899 58 Weighted Average			Veighted A	verage	
	2	01,899	1	00.00% Pe	ervious Are	а
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	11.5	50	0.1000	0.07		Sheet Flow,
	2.3	565	0.0670	4.17		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
	10.0	C1E	Tatal			

13.8 615 Total

Summary for Subcatchment ES2A:

Runoff = 6.0 cfs @ 12.19 hrs, Volume= 23,874 cf, Depth= 3.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"

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Type III 24-hr 100 Year Rainfall=8.10" Printed 11/18/2020 HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLC Page 36

	A	rea (sf)	CN	Description					
_		63,556	61	>75% Grass cover, Good, HSG B					
_		20,495	55	Woods, Go	od, HSG B				
		84,051 60 Weighted Average							
	84,051 100.00% Pervious Area				ervious Are	a			
	_								
	Tc	Length	Slope	,	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	13.2	50	0.0700	0.06		Sheet Flow,			
						Woods: Dense underbrush n= 0.800 P2= 3.10"			
	0.3	100	0.1000	5.09		Shallow Concentrated Flow,			
_						Unpaved Kv= 16.1 fps			

150 Total 13.5

Summary for Subcatchment ES3:

10.1 cfs @ 12.24 hrs, Volume= 44,060 cf, Depth= 3.30" Runoff =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"

_	A	rea (sf)	CN [Description					
	1	06,813	61 >	75% Gras	s cover, Go	ood, HSG B			
_		53,582	55 V	Woods, Good, HSG B					
	1	60,395	59 V	Veighted A	verage				
	1	60,395	1	00.00% Pe	ervious Are	а			
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	14.1	50	0.0600	0.06		Sheet Flow,			
						Woods: Dense underbrush n= 0.800 P2= 3.10"			
	2.7	490	0.0350	3.01		Shallow Concentrated Flow,			
_						Unpaved Kv= 16.1 fps			
	16.8	540	Total						

Summary for Subcatchment ES3A:

5.9 cfs @ 12.32 hrs, Volume= 29,473 cf, Depth= 3.07" Runoff =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"

Area (sf)	CN	Description		
36,688	61	>75% Grass cover, Good, HSG B		
78,384	55	Woods, Good, HSG B		
115,072	57	Weighted Average		
115,072		100.00% Pervious Area		

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TIYUIUCA		-Ja 5/1100	401 @ 202		Fage 37	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
21.8	50	0.0200	0.04		Sheet Flow,	
0.6	160	0.0750	4.41		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps	
22.4	210	Total				
			Sun	nmary foi	r Subcatchment ES4:	
Runoff	=	26.6 c	fs @ 12.2	28 hrs, Volu	ume= 123,266 cf, Depth= 3.52"	
	Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"					
A	rea (sf)	CN D	escription			
	09,301 10,796				ood, HSG B	
-	20,097		Veighted A	od, HSG B		
	20,097			ervious Are	a	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
16.5	50	0.0400	0.05		Sheet Flow,	
3.2	600	0.0380	3.14		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps	
19.7	650	Total				
			Sun	nmary foi	r Subcatchment ES5:	
Runoff	=	18.5 c	fs @ 12.2	27 hrs, Volu	ume= 85,537 cf, Depth= 3.41"	
	Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"					
	rea (sf)		escription			
	30,675			,	ood, HSG B	
	70,465			od, HSG B		
	01,140 01,140		Veighted A 00.00% Pe	verage ervious Are	a	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	

 (min)
 (feet)
 (ft/ft)
 (ft/sec)
 (cfs)

 18.6
 50
 0.0300
 0.04
 Sheet Flow, Woods: Dense underbrush n= 0.800
 P2= 3.10"

 0.8
 180
 0.0500
 3.60
 Shallow Concentrated Flow, Unpaved Kv= 16.1 fps

19.4 230 Total

Summary for Subcatchment ES5A:

Runoff 10.1 cfs @ 12.28 hrs, Volume= 46,404 cf, Depth= 3.30" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"

	A	rea (sf)	CN I	Description					
_	103,925 61 >75% Grass cover, Good, HSG B								
_		65,001	55 \	Woods, Good, HSG B					
	1	68,926	59 \	Neighted A	verage				
168,926 100.00% Pervious Area						a			
_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	18.6	50	0.0300	0.04		Sheet Flow,			
	0.3	130	0.1600	6.44		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
_	10.0	100	Total						

18.9 180 Total

Summary for Reach DP1: Parker River

Inflow Area =	338,407 sf,	0.00% Impervious,	Inflow Depth = 3.30"	for 100 Year event
Inflow =	18.5 cfs @	12.35 hrs, Volume=	92,960 cf	
Outflow =	18.5 cfs @	12.35 hrs, Volume=	92,960 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2:

Inflow Area =		285,950 sf,	0.00% Impervious,	Inflow Depth = 3.25"	for 100 Year event
Inflow	=	19.1 cfs @	12.19 hrs, Volume=	77,457 cf	
Outflow	=	19.1 cfs @	12.19 hrs, Volume=	77,457 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2A:

Inflow Area =		84,051 sf,	0.00% Impervious,	Inflow Depth = 3.41"	for 100 Year event
Inflow	=	6.0 cfs @	12.19 hrs, Volume=	23,874 cf	
Outflow	=	6.0 cfs @	12.19 hrs, Volume=	23,874 cf, Att	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3:

Inflow Area =	275,467 sf,	0.00% Impervious,	Inflow Depth = 3.20"	for 100 Year event
Inflow =	15.6 cfs @	12.27 hrs, Volume=	73,533 cf	
Outflow =	15.6 cfs @	12.27 hrs, Volume=	73,533 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3A:

Inflow Area =	115,072 sf,	0.00% Impervious,	Inflow Depth = 3.07"	for 100 Year event
Inflow =	5.9 cfs @	12.32 hrs, Volume=	29,473 cf	
Outflow =	5.9 cfs @	12.32 hrs, Volume=	29,473 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP4:

Inflow Area =	=	420,097 sf,	0.00% Impervious,	Inflow Depth = 3.52"	for 100 Year event
Inflow =	:	26.6 cfs @	12.28 hrs, Volume=	123,266 cf	
Outflow =	:	26.6 cfs @	12.28 hrs, Volume=	123,266 cf, Att	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5:

Inflow Area =	470,066 sf,	0.00% Impervious,	Inflow Depth = 3.37"	for 100 Year event
Inflow =	28.6 cfs @	12.27 hrs, Volume=	131,941 cf	
Outflow =	28.6 cfs @	12.27 hrs, Volume=	131,941 cf, Atte	n= 0%, Lag= 0.0 min

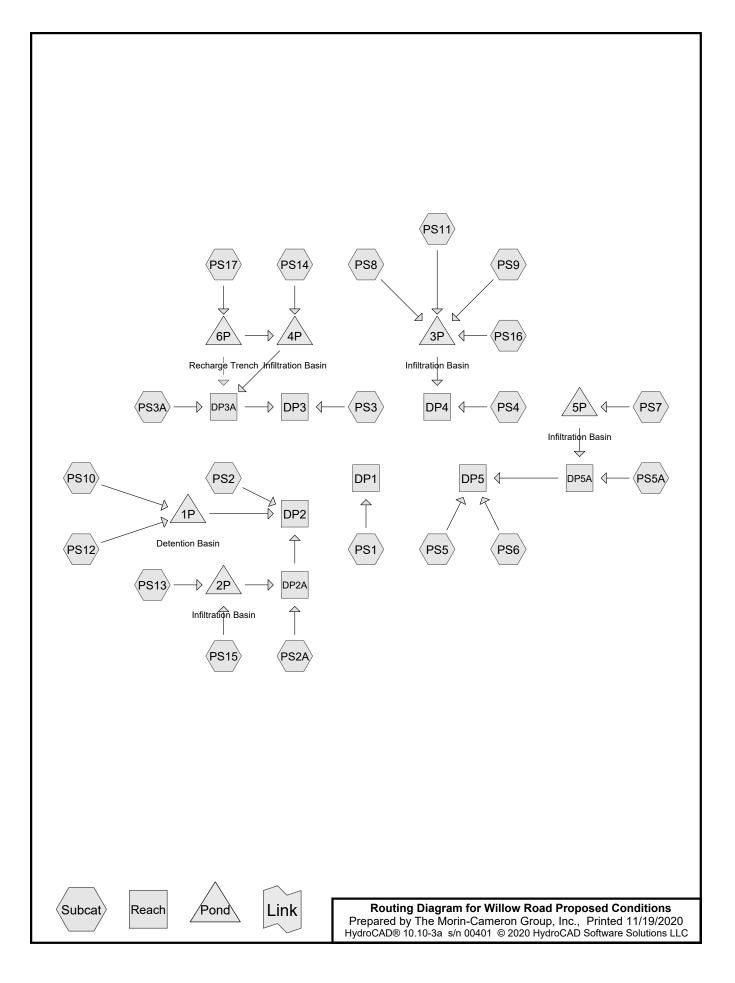
Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5A:

Inflow Area =		168,926 sf,	0.00% Impervious,	Inflow Depth = 3.30"	for 100 Year event
Inflow	=	10.1 cfs @	12.28 hrs, Volume=	46,404 cf	
Outflow	=	10.1 cfs @	12.28 hrs, Volume=	46,404 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

APPENDIX C: PROPOSED CONDITIONS HYDROLOGIC ANALYSIS



Willow Road Proposed Conditions Prepared by The Morin-Cameron Group, Inc. HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLC

Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
760,819	61	>75% Grass cover, Good, HSG B (PS1, PS10, PS11, PS12, PS13, PS14, PS2,
		PS2A, PS3, PS3A, PS4, PS5, PS5A, PS6, PS7, PS8, PS9)
10,734	96	Gravel surface, HSG B (PS11)
115,808	98	Paved roads w/curbs & sewers, HSG B (PS10, PS11, PS6, PS7, PS8, PS9)
171,380	98	Roofs, HSG B (PS11, PS13, PS15, PS16, PS17, PS6, PS7, PS9)
62,140	98	Unconnected pavement, HSG B (PS1, PS10, PS12, PS13, PS14, PS2, PS2A,
		PS3, PS3A, PS4, PS5, PS5A, PS6, PS7, PS8, PS9)
10,888	98	Unconnected roofs, HSG B (PS1, PS2, PS4)
658,218	55	Woods, Good, HSG B (PS1, PS11, PS2, PS2A, PS3, PS3A, PS4, PS5, PS5A,
		PS6)
1,789,987	66	TOTAL AREA

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Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
0	HSG A	
1,789,987	HSG B	PS1, PS10, PS11, PS12, PS13, PS14, PS15, PS16, PS17, PS2, PS2A, PS3, PS3A, PS4, PS5, PS5A, PS6, PS7, PS8, PS9
0	HSG C	
0	HSG D	
0	Other	
1,789,987		TOTAL AREA

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HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground
(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	Cover
0	760,819	0	0	0	760,819	>75% Grass cover, Good
0	10,734	0	0	0	10,734	Gravel surface
0	115,808	0	0	0	115,808	Paved roads w/curbs & sewers
0	171,380	0	0	0	171,380	Roofs
0	62,140	0	0	0	62,140	Unconnected pavement
0	10,888	0	0	0	10,888	Unconnected roofs
0	658,218	0	0	0	658,218	Woods, Good
0	1,789,987	0	0	0	1,789,987	TOTAL AREA

Ground Covers (all nodes)

Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

SubcatchmentPS1:	Runoff Area=343,774 sf 1.74% Impervious Runoff Depth=0.36" Flow Length=197' Tc=22.5 min CN=58 Runoff=1.2 cfs 10,181 cf
SubcatchmentPS10:	Runoff Area=78,810 sf 59.90% Impervious Runoff Depth=1.64" Tc=6.0 min CN=83 Runoff=3.5 cfs 10,784 cf
SubcatchmentPS11:	Runoff Area=72,767 sf 37.18% Impervious Runoff Depth=1.37" Tc=6.0 min CN=79 Runoff=2.6 cfs 8,288 cf
SubcatchmentPS12:	Runoff Area=45,344 sf 3.81% Impervious Runoff Depth=0.50" Tc=6.0 min CN=62 Runoff=0.4 cfs 1,883 cf
Subcatchment PS13:	Runoff Area=25,606 sf 30.26% Impervious Runoff Depth=0.95" Tc=6.0 min CN=72 Runoff=0.6 cfs 2,037 cf
Subcatchment PS14:	Runoff Area=22,124 sf 10.42% Impervious Runoff Depth=0.54" Tc=6.0 min UI Adjusted CN=63 Runoff=0.2 cfs 991 cf
SubcatchmentPS15:	Runoff Area=21,777 sf 100.00% Impervious Runoff Depth=3.01" Tc=6.0 min CN=98 Runoff=1.6 cfs 5,458 cf
SubcatchmentPS16:	Runoff Area=21,777 sf 100.00% Impervious Runoff Depth=3.01" Tc=6.0 min CN=98 Runoff=1.6 cfs 5,458 cf
SubcatchmentPS17:	Runoff Area=27,221 sf 100.00% Impervious Runoff Depth=3.01" Tc=6.0 min CN=98 Runoff=2.0 cfs 6,822 cf
SubcatchmentPS2:	Runoff Area=119,197 sf 5.18% Impervious Runoff Depth=0.39" Flow Length=520' Tc=13.7 min UI Adjusted CN=59 Runoff=0.5 cfs 3,864 cf
SubcatchmentPS2A:	Runoff Area=52,258 sf 2.20% Impervious Runoff Depth=0.32" Flow Length=180' Tc=11.2 min UI Adjusted CN=57 Runoff=0.2 cfs 1,407 cf
SubcatchmentPS3:	Runoff Area=97,067 sf 3.56% Impervious Runoff Depth=0.36" Flow Length=785' Tc=16.3 min UI Adjusted CN=58 Runoff=0.4 cfs 2,875 cf
SubcatchmentPS3A:	Runoff Area=67,954 sf 3.39% Impervious Runoff Depth=0.32" Flow Length=130' Tc=22.0 min UI Adjusted CN=57 Runoff=0.2 cfs 1,830 cf
SubcatchmentPS4:	Runoff Area=171,976 sf 9.20% Impervious Runoff Depth=0.46" Flow Length=100' Tc=7.6 min UI Adjusted CN=61 Runoff=1.3 cfs 6,599 cf
SubcatchmentPS5:	Runoff Area=73,892 sf 3.12% Impervious Runoff Depth=0.36" Flow Length=230' Tc=19.4 min CN=58 Runoff=0.3 cfs 2,188 cf
SubcatchmentPS5A:	Runoff Area=95,000 sf 1.21% Impervious Runoff Depth=0.29" Flow Length=150' Tc=18.9 min UI Adjusted CN=56 Runoff=0.3 cfs 2,314 cf

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SubcatchmentPS6:	Runoff Area=168,938 sf 15.67% Impervious Runoff Depth=0.54" Flow Length=220' Tc=9.2 min UI Adjusted CN=63 Runoff=1.6 cfs 7,565 cf
SubcatchmentPS7:	Runoff Area=95,556 sf 32.02% Impervious Runoff Depth=1.01" Tc=6.0 min CN=73 Runoff=2.4 cfs 8,030 cf
Subcatchment PS8:	Runoff Area=39,073 sf 71.28% Impervious Runoff Depth=1.95" Tc=6.0 min CN=87 Runoff=2.0 cfs 6,350 cf
Subcatchment PS9:	Runoff Area=149,876 sf 53.46% Impervious Runoff Depth=1.50" Tc=6.0 min CN=81 Runoff=6.0 cfs 18,742 cf
Reach DP1:	Inflow=1.2 cfs 10,181 cf Outflow=1.2 cfs 10,181 cf
Reach DP2:	Inflow=1.1 cfs 17,860 cf Outflow=1.1 cfs 17,860 cf
Reach DP2A:	Inflow=0.2 cfs 1,407 cf Outflow=0.2 cfs 1,407 cf
Reach DP3:	Inflow=0.7 cfs 4,927 cf Outflow=0.7 cfs 4,927 cf
Reach DP3A:	Inflow=0.4 cfs 2,052 cf Outflow=0.4 cfs 2,052 cf
Reach DP4:	Inflow=1.3 cfs 6,599 cf Outflow=1.3 cfs 6,599 cf
Reach DP5:	Inflow=1.7 cfs 12,067 cf Outflow=1.7 cfs 12,067 cf
Reach DP5A:	Inflow=0.3 cfs 2,314 cf Outflow=0.3 cfs 2,314 cf
Pond 1P: Detention Basin	Peak Elev=106.45' Storage=5,436 cf Inflow=3.9 cfs 12,667 cf Outflow=0.5 cfs 12,589 cf
Pond 2P: Infiltration Basin	Peak Elev=108.38' Storage=3,619 cf Inflow=2.2 cfs 7,494 cf Discarded=0.1 cfs 7,494 cf Primary=0.0 cfs 0 cf Outflow=0.1 cfs 7,494 cf
Pond 3P: Infiltration Basin	Peak Elev=106.69' Storage=26,169 cf Inflow=12.3 cfs 38,838 cf Discarded=0.3 cfs 25,031 cf Primary=0.0 cfs 0 cf Outflow=0.3 cfs 25,031 cf
Pond 4P: Infiltration Basin	Peak Elev=117.94' Storage=2,521 cf Inflow=2.1 cfs 4,910 cf Discarded=0.2 cfs 4,688 cf Primary=0.2 cfs 222 cf Outflow=0.4 cfs 4,910 cf
Pond 5P: Infiltration Basin	Peak Elev=122.02' Storage=2,508 cf Inflow=2.4 cfs 8,030 cf Discarded=0.4 cfs 8,030 cf Primary=0.0 cfs 0 cf Outflow=0.4 cfs 8,030 cf
	Deck Eleventito 241 Otomerce 400 of Unflowed 0 of a C 222 of

Pond 6P: Recharge TrenchPeak Elev=119.31' Storage=489 cfInflow=2.0 cfs6,822 cfDiscarded=0.0 cfs2,903 cfPrimary=1.9 cfs3,919 cfSecondary=0.0 cfs0 cfOutflow=2.0 cfs6,822 cf

Total Runoff Area = 1,789,987 sf Runoff Volume = 113,665 cf Average Runoff Depth = 0.76" 79.88% Pervious = 1,429,771 sf 20.12% Impervious = 360,216 sf

Page 7

Summary for Subcatchment PS1:

Runoff = 1.2 cfs @ 12.50 hrs, Volume= 10,181 cf, Depth= 0.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"

A	rea (sf)	CN [Description					
2	202,359	55 \	Woods, Good, HSG B					
1	35,428	61 >	75% Grass	s cover, Go	ood, HSG B			
	3,265	98 l	Jnconnecte	ed pavemer	nt, HSG B			
	2,722	98 l	Jnconnecte	d roofs, HS	SG B			
3	343,774	58 \	Veighted A	verage				
3	37,787	ç	98.26% Pervious Area					
	5,987	-	1.74% Impervious Area					
	5,987		100.00% Unconnected					
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
21.8	50	0.0200	0.04		Sheet Flow,			
					Woods: Dense underbrush n= 0.800 P2= 3.10"			
0.7	147	0.0480	3.53		Shallow Concentrated Flow,			
					Unpaved Kv= 16.1 fps			
22.5	197	Total						

Summary for Subcatchment PS10:

Runoff = 3.5 cfs @ 12.09 hrs, Volume= 10,784 cf, Depth= 1.64"

A	rea (sf)	CN	CN Description								
	43,871	98	98 Paved roads w/curbs & sewers, HSG B								
	31,599	61	>75% Gras	s cover, Go	bod, HSG B						
	3,340	98	Unconnecte	ed pavemer	nt, HSG B						
	78,810	83	83 Weighted Average								
	31,599		40.10% Pervious Area								
	47,211	:	59.90% Impervious Area								
	3,340		7.07% Unconnected								
Тс	Length	Slope	Velocity	Capacity	Description						
(min)	(feet)	(ft/ft)		(cfs)	•						
6.0					Direct Entry,						

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Summary for Subcatchment PS11:

Runoff = 2.6 cfs @ 12.09 hrs, Volume= 8,288 cf, Depth= 1.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"

A	rea (sf)	CN	CN Description						
	13,154	55	Woods, Go	od, HSG B					
	21,827	61	>75% Gras	s cover, Go	od, HSG B				
	10,719	98	Paved road	s w/curbs &	sewers, HSG B				
	16,333	98	Roofs, HSG	БB					
	10,734	96	Gravel surface, HSG B						
	72,767	79	79 Weighted Average						
	45,715		62.82% Pervious Area						
	27,052		37.18% Impervious Area						
Тс	Length	Slope		Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft) (ft/sec)	(cfs)					
6.0					Direct Entry,				
					-				

Summary for Subcatchment PS12:

Runoff = 0.4 cfs @ 12.12 hrs, Volume= 1,883 cf, Depth= 0.50	Runoff =	0.4 cfs @	12.12 hrs,	Volume=	1,883 cf, Depth= 0.50"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"

Area (sf)	CN	Description				
43,615	61	>75% Gras	s cover, Go	ood, HSG B		
1,729	98	Unconnecte	ed pavemer	nt, HSG B		
45,344	62	Weighted A	verage			
43,615		96.19% Pervious Area				
1,729		3.81% Impervious Area				
1,729		100.00% Unconnected				
Tc Length	Slop	be Velocity	Capacity	Description		
(min) (feet)	(ft/		(cfs)	Decemption		
6.0	•			Direct Entry,		

Summary for Subcatchment PS13:

Runoff = 0.6 cfs @ 12.10 hrs, Volume= 2,037 cf, Depth= 0.95"

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Type III 24-hr 2 Year Rainfall=3.24" Printed 11/19/2020 Page 10

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Area (s	sf) CN	Description					
17,85	57 61	>75% Grass cover, Good, HSG B					
5,44	14 98	Roofs, HSG B					
2,30)5 98	Unconnected pavement, HSG B					
25,60	06 72	Weighted Average					
17,85	57	69.74% Pervious Area					
7,74	19	30.26% Impervious Area					
2,30)5	29.75% Unconnected					
Tc Len							
(min) (fe	et) (ft/	/ft) (ft/sec) (cfs)					
6.0		Direct Entry,					

Summary for Subcatchment PS14:

Runoff = 0.2 cfs @ 12.11 hrs, Volume= 991 cf, Dep	pth= 0.54"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"

Α	rea (sf)	CN	Adj De	Description					
	19,819	61	>7	5% Grass co	over, Good, HSG B				
	2,305	98	Un	connected p	avement, HSG B				
	22,124	65	63 Weighted Average, UI Adjusted						
	19,819		89.58% Pervious Area						
	2,305		10.	10.42% Impervious Area					
	2,305		100	100.00% Unconnected					
_									
Тс	Length	Slope	Velocity		Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec	(cfs)					
6.0					Direct Entry,				

Direct Entry,

Summary for Subcatchment PS15:

Runoff = 1.6 cfs @ 12.08 hrs, Volume= 5,458 cf, Depth= 3.01"

Are	ea (sf)	CN I	Description					
2	21,777	98	Roofs, HSG B					
2	21,777		100.00% In	npervious A	Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry,			

Summary for Subcatchment PS16:

Page 11

Runoff 1.6 cfs @ 12.08 hrs, Volume= 5,458 cf, Depth= 3.01" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"

-	rea (sf) 21,777	<u>CN</u> 98	Descrip Roofs, I					
	21,777		,	6 Impervious	Area			
Tc (min)	Length (feet)	Slop (ft/f			•			
6.0					Direct Entry	/,		
	Summary for Subcatchment PS17:							
Runoff	=	2.0	cfs @	12.08 hrs, Vo	olume=	6,822 cf, Depth= 3.01"		
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"								
Area (sf) CN Description								
	27,221	98	Roofs, H	HSG B				
	27,221		100.00%	6 Impervious	Area			
Та	Longth	Clar		it. Consoit	Description			

Tc Length Slope Velocity Capacity Description (feet) (ft/ft) (ft/sec) (cfs) (min)

6.0

Direct Entry,

Summary for Subcatchment PS2:

0.5 cfs @ 12.32 hrs, Volume= 3,864 cf, Depth= 0.39" Runoff =

Area (sf)	CN	Adj	Description
61,041	55		Woods, Good, HSG B
51,977	61		>75% Grass cover, Good, HSG B
3,457	98		Unconnected pavement, HSG B
2,722	98		Unconnected roofs, HSG B
119,197	60	59	Weighted Average, UI Adjusted
113,018			94.82% Pervious Area
6,179			5.18% Impervious Area
6,179			100.00% Unconnected

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
11.5	50	0.1000	0.07		Sheet Flow,				
2.2	470	0.0500	3.60		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
13.7	520	Total							
			Sum	mary for	Subcatchment PS2A:				
Runoff	=	0.2 c	fs @ 12.3	6 hrs, Volu	ume= 1,407 cf, Depth= 0.32"				
Type III 2	24-hr 2 Y	′ear Rain	fall=3.24"	-	ted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs				
	rea (sf)			ription	122.2				
	35,762	55		ds, Good, H					
	15,344 1,152	61 98			ver, Good, HSG B				
					avement, HSG B				
	52,258 51,106	58)% Perviou	age, UI Adjusted				
	1,152			% Impervio					
	1,152			0% Uncon					
	1,102		100.0						
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	•				
10.7	50	0.1200	0.08		Sheet Flow,				
					Woods: Dense underbrush n= 0.800 P2= 3.10"				
0.5	130	0.0850	4.69		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
11.2	180	Total							
			-	-					

Summary for Subcatchment PS3:

Runoff = 0.4 cfs @ 12.41 hrs, Volume= 2,875 cf, Depth= 0.36"

Area (sf)	CN	Adj	Description
50,666	55		Woods, Good, HSG B
42,944	61		>75% Grass cover, Good, HSG B
3,457	98		Unconnected pavement, HSG B
97,067	59	58	Weighted Average, UI Adjusted
93,610			96.44% Pervious Area
3,457			3.56% Impervious Area
3,457			100.00% Unconnected

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<u>Ingalo on (</u>	00 10.10	04 0/11 00			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.5	50	0.1000	0.07		Sheet Flow,
4.8	735	0.0250	2.55		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
16.3	785	Total			
			Sum	mary for	^r Subcatchment PS3A:
Runoff	=	0.2 c	fs @ 12.5	52 hrs, Vol	lume= 1,830 cf, Depth= 0.32"
Type III 2		′ear Rain	fall=3.24"	CS, Weigh	nted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs
	53,432	55		ds, Good, I	HSG B
	12,217	61			over, Good, HSG B
	2,305	98			pavement, HSG B
	67,954				age, UI Adjusted
	65,649			1% Perviou	
	2,305		3.39	% Impervio	bus Area
	2,305		100.	00% Uncor	nnected
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.8	50	0.0200	0.04		Sheet Flow,
					Woods: Dense underbrush n= 0.800 P2= 3.10"
0.2	80	0.1250	5.69		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
22.0	130	Total			· · ·
			Sun	amary fo	r Subcatchment PS4

Summary for Subcatchment PS4:

Runoff = 1.3 cfs @ 12.15 hrs, Volume= 6,599 cf, Depth= 0.46"

Area (sf)	CN	Adj	Description
48,637	55		Woods, Good, HSG B
107,523	61		>75% Grass cover, Good, HSG B
10,372	98		Unconnected pavement, HSG B
5,444	98		Unconnected roofs, HSG B
171,976	63	61	Weighted Average, UI Adjusted
156,160			90.80% Pervious Area
15,816			9.20% Impervious Area
15,816			100.00% Unconnected

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	7.5	50	0.0100	0.11		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.10"
	0.1	50	0.2400	7.89		Shallow Concentrated Flow,
_						Unpaved Kv= 16.1 fps
	7.6	100	Total			

Summary for Subcatchment PS5:

Runoff 0.3 cfs @ 12.46 hrs, Volume= 2,188 cf, Depth= 0.36" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"

A	rea (sf)	CN E	N Description				
	48,067	55 V	Voods, Go	od, HSG B			
	23,521	61 >	75% Gras	s cover, Go	bod, HSG B		
	2,304	98 L	Inconnecte	ed pavemer	nt, HSG B		
	73,892	58 V	Veighted A	verage			
	71,588	9	6.88% Per	vious Area			
	2,304	3	.12% Impe	ervious Are	а		
	2,304	1	00.00% Ui	nconnected	1		
Тс	Length	Slope	Velocity	Capacity	Description		
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)			
18.6	50	0.0300	0.04		Sheet Flow,		
					Woods: Dense underbrush n= 0.800 P2= 3.10"		
0.8	180	0.0500	3.60		Shallow Concentrated Flow,		
					Unpaved Kv= 16.1 fps		
19.4	230	Total					

Summary for Subcatchment PS5A:

Runoff 0.3 cfs @ 12.50 hrs, Volume= 2,314 cf, Depth= 0.29" =

Area (sf)	CN	Adj	Description
77,272	55		Woods, Good, HSG B
16,576	61		>75% Grass cover, Good, HSG B
1,152	98		Unconnected pavement, HSG B
95,000	57	56	Weighted Average, UI Adjusted
93,848			98.79% Pervious Area
1,152			1.21% Impervious Area
1,152			100.00% Unconnected

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
18.6	50	0.0300	0.04		Sheet Flow,			
0.3	100	0.1000	5.09		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
18.9	150	Total						
	Summary for Subcatchment PS6:							
Runoff	=	1.6 ct	fs @ 12.1	l6 hrs, Vol	ume= 7,565 cf, Depth= 0.54"			
Type III 2	Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"							
	rea (sf)			cription				
	67,828 74,644	55 61		ds, Good, H				
	11,625	98			ver, Good, HSG B avement, HSG B			
	13,498	98		s, HSG B				
	1,343	98		,	curbs & sewers, HSG B			
1	68,938	64	63 Weig	hted Avera	age, UI Adjusted			
1	42,472		84.3	3% Perviou	is Area			
	26,466			7% Impervi				
	11,625		43.9	2% Unconr	nected			
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
8.7	50	0.0500	0.10		Sheet Flow,			
0.5	170	0.1120	5.39		Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
9.2	220	Total						

Type III 24-hr 2 Year Rainfall=3.24"

Willow Road Proposed Conditions

Summary for Subcatchment PS7:

Runoff	=	2.4 cfs @	12.10 hrs, Volu	ume=	8,030 cf, Depth= 1.01"
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Area (sf)	CN	Description
64,959	61	>75% Grass cover, Good, HSG B
10,888	98	Roofs, HSG B
7,062	98	Unconnected pavement, HSG B
12,647	98	Paved roads w/curbs & sewers, HSG B
95,556	73	Weighted Average
64,959		67.98% Pervious Area
30,597		32.02% Impervious Area
7,062		23.08% Unconnected

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Tc (min)		lope Velo (ft/ft) (ft/s	city Capacity sec) (cfs)	Description		
6.0				Direct Entry	/,	
			Summary fo	r Subcatch	ment PS8	3:
Runoff	=	2.0 cfs @	12.09 hrs, Vol	lume=	6,350 cf,	Depth= 1.95"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.24"						
Are	ea (sf) CN	N Descrip	otion			
	5,064 98		roads w/curbs		GВ	
	2,787 98 1,222 6 ²		nected paveme Grass cover, G			
	9,073 87		ed Average	, <u> </u>		
	1,222	-	Pervious Area			
	7,851		Impervious Ar	rea		
	2,787	10.01%	6 Unconnected			
Тс	Length S	lope Velo	city Capacity	Description		
(min)			sec) (cfs)	•		
6.0				Direct Entry	/,	
	Summary for Subcatchment PS9:					
Runoff	=	6.0 cfs @	12.09 hrs, Vol	lume=	18,742 cf,	Depth= 1.50"

Area ((sf) CN	Description
22,1	64 98	Paved roads w/curbs & sewers, HSG B
69,7	747 61	>75% Grass cover, Good, HSG B
3,5	523 98	Unconnected pavement, HSG B
54,4	42 98	Roofs, HSG B
149,8	876 81	Weighted Average
69,7	'47	46.54% Pervious Area
80,1	29	53.46% Impervious Area
3,5	523	4.40% Unconnected
		ope Velocity Capacity Description t/ft) (ft/sec) (cfs)
6.0		Direct Entry,

Summary for Reach DP1:

Inflow Area =	343,774 sf,	1.74% Impervious,	Inflow Depth = 0.36"	for 2 Year event
Inflow =	1.2 cfs @	12.50 hrs, Volume=	10,181 cf	
Outflow =	1.2 cfs @	12.50 hrs, Volume=	10,181 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2:

Inflow Area =	342,992 sf,	25.01% Impervious,	Inflow Depth > 0.62"	for 2 Year event
Inflow =	1.1 cfs @	12.41 hrs, Volume=	17,860 cf	
Outflow =	1.1 cfs @	12.41 hrs, Volume=	17,860 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2A:

Inflow Area =	99,641 sf, 30.	.79% Impervious,	Inflow Depth = 0.17 "	for 2 Year event
Inflow =	0.2 cfs @ 12.3	.36 hrs, Volume=	1,407 cf	
Outflow =	0.2 cfs @ 12.3	.36 hrs, Volume=	1,407 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3:

Inflow Area	a =	214,366 sf,	16.46% Impervious,	Inflow Depth = 0.28"	for 2 Year event
Inflow	=	0.7 cfs @	12.51 hrs, Volume=	4,927 cf	
Outflow	=	0.7 cfs @	12.51 hrs, Volume=	4,927 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3A:

Inflow Area	a =	117,299 sf,	27.14% Impervious,	Inflow Depth = 0.21"	for 2 Year event
Inflow	=	0.4 cfs @	12.53 hrs, Volume=	2,052 cf	
Outflow	=	0.4 cfs @	12.53 hrs, Volume=	2,052 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP4:

Inflow Area =	455,469 sf,	37.90% Impervious,	Inflow Depth = 0.17"	for 2 Year event
Inflow =	1.3 cfs @	12.15 hrs, Volume=	6,599 cf	
Outflow =	1.3 cfs @	12.15 hrs, Volume=	6,599 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5:

Inflow Area	a =	433,386 sf,	13.96% Impervious,	Inflow Depth = 0.33"	for 2 Year event
Inflow	=	1.7 cfs @	12.18 hrs, Volume=	12,067 cf	
Outflow	=	1.7 cfs @	12.18 hrs, Volume=	12,067 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5A:

Inflow Area	a =	190,556 sf,	16.66% Impervious,	Inflow Depth = 0.15'	for 2 Year event
Inflow	=	0.3 cfs @	12.50 hrs, Volume=	2,314 cf	
Outflow	=	0.3 cfs @	12.50 hrs, Volume=	2,314 cf, Att	ten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Pond 1P: Detention Basin

Inflow Area =	124,154 sf, 39.42% Impervious,	Inflow Depth = 1.22" for 2 Year event
Inflow =	3.9 cfs @ 12.09 hrs, Volume=	12,667 cf
Outflow =	0.5 cfs @ 12.88 hrs, Volume=	12,589 cf, Atten= 87%, Lag= 47.4 min
Primary =	0.5 cfs @ 12.88 hrs, Volume=	12,589 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 106.45' @ 12.88 hrs Surf.Area= 4,645 sf Storage= 5,436 cf

Plug-Flow detention time= 201.5 min calculated for 12,589 cf (99% of inflow) Center-of-Mass det. time= 197.8 min (1,041.4 - 843.6)

Volume	Invert	Avail.Sto	rage Storag	e Description	
#1	105.00'	26,98	B7 cf Custo	m Stage Data (Pris	smatic)Listed below (Recalc)
_	-	<i>.</i> .		a a /	
Elevatio	on Su	ırf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
105.0	00	2,562	0	0	
106.0	00	4,302	3,432	3,432	
108.0)0	5,832	10,134	13,566	
110.0	00	7,589	13,421	26,987	
Device	Routing	Invert	Outlet Devic	es	
#1	Primary	98.00'	12.0" Roun	d Culvert L= 40.0	' Ke= 0.500
			Inlet / Outlet	Invert= 98.00' / 96.	.00' S= 0.0500 '/' Cc= 0.900
			n= 0.012, F	low Area= 0.79 sf	
#2	Device 1	105.00'	3.0" Vert. O	rifice/Grate C= 0.	.600 Limited to weir flow at low heads
#3	Device 1	106.00'	4.0" Vert. O	rifice/Grate C= 0.	.600 Limited to weir flow at low heads
#4	Device 1	107.60'		0" H Vert. Orifice/	
			Limited to w	eir flow at low head	s
#5	Device 1	108.90'	4.0' long x	0.5' breadth Broad	d-Crested Rectangular Weir
				0.20 0.40 0.60 0.	
				sh) 2.80 2.92 3.08	
			, u		

Primary OutFlow Max=0.5 cfs @ 12.88 hrs HW=106.45' TW=0.00' (Dynamic Tailwater) **1=Culvert** (Passes 0.5 cfs of 10.7 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.3 cfs @ 5.54 fps)

-3=Orifice/Grate (Orifice Controls 0.2 cfs @ 2.55 fps)

-4=Orifice/Grate (Controls 0.0 cfs)

-5=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond 2P: Infiltration Basin

Inflow Area =	47,383 sf, 62.31% Impervious,	Inflow Depth = 1.90" for 2 Year event
Inflow =	2.2 cfs @ 12.09 hrs, Volume=	7,494 cf
Outflow =	0.1 cfs @ 14.03 hrs, Volume=	7,494 cf, Atten= 94%, Lag= 116.4 min
Discarded =	0.1 cfs @ 14.03 hrs, Volume=	7,494 cf
Primary =	0.0 cfs @ 0.00 hrs, Volume=	0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 108.38' @ 14.03 hrs Surf.Area= 2,412 sf Storage= 3,619 cf

Plug-Flow detention time= 302.2 min calculated for 7,492 cf (100% of inflow) Center-of-Mass det. time= 302.2 min (1,088.7 - 786.5)

Volume	Inve	ert Avail.Sto	rage Storage	Description		
#1	106.0	0' 8,7	99 cf Custom	Stage Data (Coni	c)Listed below (R	ecalc)
Elevatio (fee 106.0 108.0	et) 00	Surf.Area (sq-ft) 781 2.086	Inc.Store (cubic-feet) 0 2,762	Cum.Store (cubic-feet) 0 2,762	Wet.Area (sq-ft) 781 2,112	
110.0		2,080 4,059	6,037	8,799	4,123	
Device	Routing	Invert	Outlet Devices	6		
#1	Primary	109.50'		2.0' breadth Broad 20 0.40 0.60 0.8		
#2	Discarde	d 106.00'	2.85 3.07 3.2) 2.54 2.61 2.61 20 3.32 afiltration over Su		

Discarded OutFlow Max=0.1 cfs @ 14.03 hrs HW=108.38' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.1 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=106.00' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Controls 0.0 cfs)

Summary for Pond 3P: Infiltration Basin

Prepare	Willow Road Proposed Conditions Prepared by The Morin-Cameron Group, Inc. HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solut					/ear Rainfall=3.24" Printed 11/19/2020 Page 20
Inflow A Inflow Outflow Discarde Primary	= = ed = =	12.3 cfs @ 1 0.3 cfs @ 1 0.3 cfs @ 1 0.0 cfs @	2.09 hrs, Volun 7.90 hrs, Volun 7.90 hrs, Volun 0.00 hrs, Volun	ne= 25,031 ne= 25,031 ne= 0	cf cf, Atten= 98%, cf cf	′ear event Lag= 348.8 min
				0-36.00 hrs, dt= 0.01 68 sf Storage= 26,		
			nin calculated fo nin (1,342.7 - 82	r 25,031 cf (64% of 25.3)	inflow)	
Volume	Inver	t Avail.Sto	rage Storage I	Description		
#1	104.00	' 83,59	98 cf Custom	Stage Data (Conic)	Listed below (R	ecalc)
Elevatio (fee		urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft <u>)</u>	
104.0		8,168	0	0	8,168	
105.0		9,203	8,680	8,680	9,254	
106.0		10,294	9,743	18,424	10,400	
108.0		15,794	25,893	44,316	15,959	
110.0	00	23,758	39,282	83,598	23,984	
Device	Routing	Invert	Outlet Devices	i		
#1	Primary	106.50'	Inlet / Outlet In	Culvert L= 34.0' k vert= 106.50' / 106. crete pipe, finished,	00' S= 0.0147 '	
#2	Device 1	107.00'		ice/Grate C= 0.60		
#2	Device 1	108.00'		ice/Grate C= 0.600		
#4	Device 1	109.00'		rifice/Grate C= 0.6		
				flow at low heads		
#5	Primary	109.50'	Head (feet) 0. 2.50 3.00 3.5 Coef. (English)	.0' breadth Broad-(20 0.40 0.60 0.80 0 4.00 4.50 5.00 () 2.38 2.54 2.69 2 3 2.76 2.79 2.88 (1.00 1.20 1.40 5.50 .68 2.67 2.67	0 1.60 1.80 2.00
#6	Discarded	104.00'		filtration over Surfa		e-In= 0.01'
Discard	ed OutFlov	Max=0.3 cfs	@ 17.90 hrs H	W=106.69' (Free D	ischarge)	

Discarded OutFlow Max=0.3 cfs @ 17.90 hrs HW=106.69' (Free Discharge) **G=Exfiltration** (Exfiltration Controls 0.3 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=104.00' TW=0.00' (Dynamic Tailwater) -1=Culvert (Controls 0.0 cfs) -2=Orifice/Grate (Controls 0.0 cfs) -3=Orifice/Grate (Controls 0.0 cfs) -4=Orifice/Grate (Controls 0.0 cfs)

-5=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond 4P: Infiltration Basin

Inflow Area =	49,345 sf, 59.84% Impervious	, Inflow Depth = 1.19" for 2 Year event
Inflow =	2.1 cfs @ 12.09 hrs, Volume=	= 4,910 cf
Outflow =	0.4 cfs @ 12.53 hrs, Volume=	4,910 cf, Atten= 81%, Lag= 26.3 min
Discarded =	0.2 cfs @ 12.53 hrs, Volume=	= 4,688 cf
Primary =	0.2 cfs @ 12.53 hrs, Volume=	= 222 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 117.94' @ 12.53 hrs Surf.Area= 3,836 sf Storage= 2,521 cf

Plug-Flow detention time= 121.7 min calculated for 4,910 cf (100% of inflow) Center-of-Mass det. time= 121.7 min (898.9 - 777.2)

Volume	Invert	Avail.Sto	rage Storage	Description		
#1	117.00'	4,9	51 cf Custom	Stage Data (Coni	c)Listed below (Red	calc)
Elevatio (fee		ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
117.0	0	1,691	0	0	1,691	
118.0 118.5		4,012 4,726	2,769 2,182	2,769 4,951	4,019 4,743	
Device	Routing	Invert	Outlet Devices	6		
#1	Primary	117.90'			d-Crested Rectang	
			2.50 3.00) 2.69 2.72 2.75	0 1.00 1.20 1.40 2.85 2.98 3.08 3.	
#2	Primary	118.10'	25.0' long x '	I.0' breadth Broad	d-Crested Rectang 0 1.00 1.20 1.40	
#3	Discarded	117.00'	Coef. (English 3.30 3.31 3.3	32	2.85 2.98 3.08 3.	
				· · · · · · · · · · · · · · · · · · ·		

Discarded OutFlow Max=0.2 cfs @ 12.53 hrs HW=117.94' (Free Discharge) **3=Exfiltration** (Exfiltration Controls 0.2 cfs)

Primary OutFlow Max=0.2 cfs @ 12.53 hrs HW=117.94' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.2 cfs @ 0.52 fps) 2=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond 5P: Infiltration Basin

Inflow Area =	95,556 sf, 32.02% Impervious	, Inflow Depth = 1.01" for _2 Year event
Inflow =	2.4 cfs @ 12.10 hrs, Volume=	= 8,030 cf
Outflow =	0.4 cfs @ 12.66 hrs, Volume=	= 8,030 cf, Atten= 83%, Lag= 34.0 min
Discarded =	0.4 cfs @ 12.66 hrs, Volume=	= 8,030 cf
Primary =	0.0 cfs $\overline{@}$ 0.00 hrs, Volume=	= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

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Peak Elev= 122.02' @ 12.66 hrs Surf.Area= 7,450 sf Storage= 2,508 cf

Plug-Flow detention time= 59.7 min calculated for 8,030 cf (100% of inflow) Center-of-Mass det. time= 59.7 min (924.3 - 864.6)

Volume	Inve	rt Avail.Sto	rage Storage	e Description	
#1	121.5	0' 20,80	63 cf Custor	m Stage Data (P	rismatic)Listed below (Recalc)
Elevatio		Surf.Area	Inc.Store	Cum.Store	
(fee	t)	(sq-ft)	(cubic-feet)	(cubic-feet)	
121.5	0	2,680	0	0	
121.7	5	4,316	875	875	
122.0	0	7,408	1,466	2,340	
124.0	0	11,115	18,523	20,863	
Device	Routing	Invert	Outlet Devic	es	
#1	Primary	122.75'		0.20 0.40 0.60	oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00
#2	Discardeo	d 121.50'	Coef. (Englis 2.85 3.07 3	sh) 2.54 2.61 2. .20 3.32	61 2.60 2.66 2.70 2.77 2.89 2.88 Surface area Phase-In= 0.01'
#2	Discalue	J 121.00	2.410 11/11/1		Sunace alea i nase-in- 0.01

Discarded OutFlow Max=0.4 cfs @ 12.66 hrs HW=122.02' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.4 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=121.50' TW=0.00' (Dynamic Tailwater) ☐ 1=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond 6P: Recharge Trench

Inflow Area =	27,221 sf,100.00% Impervious,	Inflow Depth = 3.01" for 2 Year event
Inflow =	2.0 cfs @ 12.08 hrs, Volume=	6,822 cf
Outflow =	2.0 cfs @ 12.08 hrs, Volume=	6,822 cf, Atten= 0%, Lag= 0.0 min
Discarded =	0.0 cfs @ 8.70 hrs, Volume=	2,903 cf
Primary =	1.9 cfs @ 12.08 hrs, Volume=	3,919 cf
Secondary =	0.0 cfs $\overline{@}$ 0.00 hrs, Volume=	0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 119.31' @ 12.08 hrs Surf.Area= 720 sf Storage= 489 cf

Plug-Flow detention time= 52.6 min calculated for 6,822 cf (100% of inflow) Center-of-Mass det. time= 52.6 min (808.8 - 756.1)

Volume	Invert	Avail.Storage	Storage Description
#1	115.50'	392 cf	Custom Stage Data (Prismatic)Listed below (Recalc)
			1,080 cf Overall - 101 cf Embedded = 979 cf x 40.0% Voids
#2	116.17'	94 cf	6.0" Round Pipe Storage Inside #1
			L= 480.0'
			101 cf Overall - 0.1" Wall Thickness = 94 cf
#3	117.00'	12 cf	0.50'D x 10.00'H Vertical Cone/Cylinder x 6 -Impervious
		498 cf	Total Available Storage

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Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
115.50	720	0	0
117.00	720	1,080	1,080

Device	Routing	Invert	Outlet Devices	
#1	Discarded	115.50'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'	
#2	Primary	118.00'	4.0" Horiz. Orifice/Grate X 4.00 C= 0.600	
			Limited to weir flow at low heads	
#3	Secondary	120.00'	4.0" Horiz. Orifice/Grate X 4.00 C= 0.600	
			Limited to weir flow at low heads	

Discarded OutFlow Max=0.0 cfs @ 8.70 hrs HW=115.62' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=1.9 cfs @ 12.08 hrs HW=119.31' TW=117.57' (Dynamic Tailwater) →2=Orifice/Grate (Orifice Controls 1.9 cfs @ 5.51 fps)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=115.50' TW=0.00' (Dynamic Tailwater) -3=Orifice/Grate (Controls 0.0 cfs)

Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

SubcatchmentPS1:	Runoff Area=343,774 sf 1.74% Impervious Runoff Depth=1.24" Flow Length=197' Tc=22.5 min CN=58 Runoff=6.4 cfs 35,390 cf
Subcatchment PS10:	Runoff Area=78,810 sf 59.90% Impervious Runoff Depth=3.28" Tc=6.0 min CN=83 Runoff=6.9 cfs 21,560 cf
SubcatchmentPS11:	Runoff Area=72,767 sf 37.18% Impervious Runoff Depth=2.91" Tc=6.0 min CN=79 Runoff=5.7 cfs 17,617 cf
SubcatchmentPS12:	Runoff Area=45,344 sf 3.81% Impervious Runoff Depth=1.51" Tc=6.0 min CN=62 Runoff=1.7 cfs 5,717 cf
SubcatchmentPS13:	Runoff Area=25,606 sf 30.26% Impervious Runoff Depth=2.29" Tc=6.0 min CN=72 Runoff=1.6 cfs 4,888 cf
SubcatchmentPS14:	Runoff Area=22,124 sf 10.42% Impervious Runoff Depth=1.59" Tc=6.0 min UI Adjusted CN=63 Runoff=0.9 cfs 2,923 cf
SubcatchmentPS15:	Runoff Area=21,777 sf 100.00% Impervious Runoff Depth=4.88" Tc=6.0 min CN=98 Runoff=2.5 cfs 8,861 cf
SubcatchmentPS16:	Runoff Area=21,777 sf 100.00% Impervious Runoff Depth=4.88" Tc=6.0 min CN=98 Runoff=2.5 cfs 8,861 cf
SubcatchmentPS17:	Runoff Area=27,221 sf 100.00% Impervious Runoff Depth=4.88" Tc=6.0 min CN=98 Runoff=3.1 cfs 11,077 cf
SubcatchmentPS2:	Runoff Area=119,197 sf 5.18% Impervious Runoff Depth=1.30" Flow Length=520' Tc=13.7 min UI Adjusted CN=59 Runoff=2.9 cfs 12,942 cf
SubcatchmentPS2A:	Runoff Area=52,258 sf 2.20% Impervious Runoff Depth=1.17" Flow Length=180' Tc=11.2 min UI Adjusted CN=57 Runoff=1.2 cfs 5,091 cf
SubcatchmentPS3:	Runoff Area=97,067 sf 3.56% Impervious Runoff Depth=1.24" Flow Length=785' Tc=16.3 min UI Adjusted CN=58 Runoff=2.0 cfs 9,993 cf
SubcatchmentPS3A:	Runoff Area=67,954 sf 3.39% Impervious Runoff Depth=1.17" Flow Length=130' Tc=22.0 min UI Adjusted CN=57 Runoff=1.2 cfs 6,620 cf
SubcatchmentPS4:	Runoff Area=171,976 sf 9.20% Impervious Runoff Depth=1.44" Flow Length=100' Tc=7.6 min UI Adjusted CN=61 Runoff=5.8 cfs 20,662 cf
SubcatchmentPS5:	Runoff Area=73,892 sf 3.12% Impervious Runoff Depth=1.24" Flow Length=230' Tc=19.4 min CN=58 Runoff=1.5 cfs 7,607 cf
Subcatchment PS5A:	Runoff Area=95,000 sf 1.21% Impervious Runoff Depth=1.10" Flow Length=150' Tc=18.9 min UI Adjusted CN=56 Runoff=1.6 cfs 8,740 cf

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Subcatchment PS6: Flow Leng	Runoff Area=168,938 sf 15.67% Impervious Runoff Depth=1.59" ht=220' Tc=9.2 min UI Adjusted CN=63 Runoff=6.0 cfs 22,320 cf
SubcatchmentPS7:	Runoff Area=95,556 sf 32.02% Impervious Runoff Depth=2.37" Tc=6.0 min CN=73 Runoff=6.1 cfs 18,912 cf
SubcatchmentPS8:	Runoff Area=39,073 sf 71.28% Impervious Runoff Depth=3.68" Tc=6.0 min CN=87 Runoff=3.8 cfs 11,984 cf
SubcatchmentPS9:	Runoff Area=149,876 sf 53.46% Impervious Runoff Depth=3.09" Tc=6.0 min CN=81 Runoff=12.5 cfs 38,613 cf
Reach DP1:	Inflow=6.4 cfs 35,390 cf Outflow=6.4 cfs 35,390 cf
Reach DP2:	Inflow=4.8 cfs 45,853 cf Outflow=4.8 cfs 45,853 cf
Reach DP2A:	Inflow=1.2 cfs 5,737 cf Outflow=1.2 cfs 5,737 cf
Reach DP3:	Inflow=5.1 cfs 20,266 cf Outflow=5.1 cfs 20,266 cf
Reach DP3A:	Inflow=3.1 cfs 10,273 cf Outflow=3.1 cfs 10,273 cf
Reach DP4:	Inflow=5.8 cfs 38,315 cf Outflow=5.8 cfs 38,315 cf
Reach DP5:	Inflow=8.0 cfs 38,667 cf Outflow=8.0 cfs 38,667 cf
Reach DP5A:	Inflow=1.6 cfs 8,740 cf Outflow=1.6 cfs 8,740 cf
Pond 1P: Detention Basin	Peak Elev=107.79' Storage=12,351 cf Inflow=8.6 cfs 27,277 cf Outflow=1.1 cfs 27,175 cf
Pond 2P: Infiltration Basin Discarded=0	Peak Elev=109.53' Storage=6,998 cf Inflow=4.1 cfs 13,749 cf .2 cfs 13,015 cf Primary=0.2 cfs 646 cf Outflow=0.4 cfs 13,660 cf
Pond 3P: Infiltration Basin Discarded=0.4 of	Peak Elev=108.35' Storage=50,106 cf Inflow=24.4 cfs 77,075 cf cfs 33,907 cf Primary=0.6 cfs 17,653 cf Outflow=1.0 cfs 51,560 cf
Pond 4P: Infiltration Basin Discarded=0.	Peak Elev=118.09' Storage=3,140 cf Inflow=3.3 cfs 10,360 cf 2 cfs 6,886 cf Primary=2.2 cfs 3,474 cf Outflow=2.5 cfs 10,360 cf
Pond 5P: Infiltration Basin Discarded	Peak Elev=122.74' Storage=8,325 cf Inflow=6.1 cfs 18,912 cf =0.5 cfs 18,912 cf Primary=0.0 cfs 0 cf Outflow=0.5 cfs 18,912 cf
Pond 6P: Recharge Trench Discarded=0.0 cfs 3,460 cf Primary=2.5	Peak Elev=120.14' Storage=490 cf Inflow=3.1 cfs 11,077 cf cfs 7,437 cf Secondary=0.6 cfs 179 cf Outflow=3.1 cfs 11,077 cf

Total Runoff Area = 1,789,987 sf Runoff Volume = 280,378 cf Average Runoff Depth = 1.88" 79.88% Pervious = 1,429,771 sf 20.12% Impervious = 360,216 sf

Summary for Subcatchment PS1:

Runoff = 6.4 cfs @ 12.37 hrs, Volume= 35,390 cf, Depth= 1.24"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"

A	rea (sf)	CN E	Description				
2	02,359	55 V	Voods, Go	od, HSG B			
1	35,428	61 >	75% Gras	s cover, Go	ood, HSG B		
	3,265	98 L	Jnconnecte	ed pavemer	nt, HSG B		
	2,722	98 L	Inconnecte	ed roofs, HS	SG B		
3	43,774	58 V	Veighted A	verage			
3	37,787	ç	8.26% Per	vious Area			
	5,987	1	.74% Impe	ervious Area	а		
	5,987	1	100.00% Unconnected				
Тс	Length	Slope		Capacity	Description		
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)			
21.8	50	0.0200	0.04		Sheet Flow,		
					Woods: Dense underbrush n= 0.800 P2= 3.10"		
0.7	147	0.0480	3.53		Shallow Concentrated Flow,		
					Unpaved Kv= 16.1 fps		
22.5	197	Total					

Summary for Subcatchment PS10:

Runoff = 6.9 cfs @ 12.09 hrs, Volume= 21,560 cf, Depth= 3.28"

A	rea (sf)	CN	Description						
	43,871	98	Paved road	s w/curbs &	& sewers, HSG B				
:	31,599	61	>75% Grass	s cover, Go	lood, HSG B				
	3,340	98	Unconnecte	d pavemer	ent, HSG B				
	78,810	83	Weighted A	verage					
:	31,599		40.10% Pervious Area						
	47,211		59.90% Impervious Area						
	3,340		7.07% Unconnected						
_									
Тс	Length	Slope		Capacity					
<u>(min)</u>	(feet)	(ft/ft) (ft/sec)	(cfs)					
6.0					Direct Entry,				

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Summary for Subcatchment PS11:

Runoff = 5.7 cfs @ 12.09 hrs, Volume= 17,617 cf, Depth= 2.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"

A	rea (sf)	CN	Description					
	13,154	55	Woods, Go	od, HSG B				
	21,827	61	>75% Gras	s cover, Go	od, HSG B			
	10,719	98	Paved road	s w/curbs &	sewers, HSG B			
	16,333	98	Roofs, HSG	БB				
	10,734	96	6 Gravel surface, HSG B					
	72,767	79	Weighted A	verage				
	45,715		62.82% Per	vious Area				
	27,052		37.18% Imp	ervious Ar	ea			
Тс	Length	Slope		Capacity	Description			
<u>(min)</u>	(feet)	(ft/ft) (ft/sec)	(cfs)				
6.0					Direct Entry,			
					-			

Summary for Subcatchment PS12:

Runoff	=	1.7 cfs @	12.10 hrs,	Volume=	5,717 cf, Depth= 1.51"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"

Area (sf)	CN	Description		
43,615	61	>75% Gras		
1,729	98	Unconnecte	ed pavemer	nt, HSG B
45,344	62	Weighted A	verage	
43,615		96.19% Per	vious Area	
1,729		3.81% Impe	ervious Area	a
1,729		100.00% Ü	nconnected	1
Tc Length	Slop	be Velocity	Capacity	Description
(min) (feet)	(ft/	ft) (ft/sec)	(cfs)	
6.0				Direct Entry,

Summary for Subcatchment PS13:

Runoff = 1.6 cfs @ 12.09 hrs, Volume= 4,888 cf, Depth= 2.29"

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Type III 24-hr 10 Year Rainfall=5.12" Printed 11/19/2020 HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLC Page 29

Area (sf)	CN	Description						
17,857	61	>75% Grass cover, Good, HSG B						
5,444	98	Roofs, HSG B						
2,305	98	Unconnected pavement, HSG B						
25,606	72	Weighted Average						
17,857		69.74% Pervious Area						
7,749		30.26% Impervious Area						
2,305		29.75% Unconnected						
Tc Length								
(min) (feet)	(ft/	ft) (ft/sec) (cfs)						

6.0

Direct Entry,

Summary for Subcatchment PS14:

Runoff	=	0.9 cfs @	12.10 hrs,	Volume=	2,923 cf, Depth= 1.59"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"

A	rea (sf)	CN /	Adj Des	cription				
	19,819	61	>75	% Grass co	ver, Good, HSG B			
	2,305	98	Unc	onnected pa	avement, HSG B			
	22,124	65	63 Wei	ghted Avera	age, UI Adjusted			
	19,819		89.5	8% Perviou	us Area			
	2,305		10.42% Impervious Area					
	2,305		100	00% Uncor	nnected			
_		~		.	_			
Тс	Length	Slope	Velocity	Capacity	Description			
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)				
6.0					Direct Entry,			

Direct Entry,

Summary for Subcatchment PS15:

Runoff = 2.5 cfs @ 12.08 hrs, Volume= 8,861 cf, Depth= 4.88"

A	rea (sf)	CN	Description		
	21,777	98	Roofs, HSG	βB	
	21,777		100.00% Im	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
<u>(11111)</u> 6.0	(leel)	וועונ		(015)	Direct Entry,
0.0					Direct Entry,

Summary for Subcatchment PS16:

Runoff = 2.5 cfs @ 12.08 hrs, Volume= 8,861 cf, Depth= 4.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"

Area (sf) CN Description							
21,777 98 Roofs, HSG B							
21,777 100.00% Impervious Area							
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)							
6.0 Direct Entry,							
Summary for Subcatchment PS17:							
Runoff = 3.1 cfs @ 12.08 hrs, Volume= 11,077 cf, Depth= 4.88"							
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"							
Area (sf) CN Description							
27,221 98 Roofs, HSG B							
27,221 100.00% Impervious Area							
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)							
6.0 Direct Entry,							

Summary for Subcatchment PS2:

Runoff = 2.9 cfs @ 12.21 hrs, Volume= 12,942 cf, Depth= 1.30"

Area (sf)	CN	Adj	Description
61,041	55		Woods, Good, HSG B
51,977	61		>75% Grass cover, Good, HSG B
3,457	98		Unconnected pavement, HSG B
2,722	98		Unconnected roofs, HSG B
119,197	60	59	Weighted Average, UI Adjusted
113,018			94.82% Pervious Area
6,179			5.18% Impervious Area
6,179			100.00% Unconnected

Prepare	d by The	e Morin-C		Group, Inc	Type III 24-hr 10 Year Rainfall=5.12"c.Printed 11/19/2020c.Page 31			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
11.5	50	0.1000	0.07		Sheet Flow,			
2.2	470	0.0500	3.60		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
13.7	520	Total			· · · · · · · · · · · · · · · · · · ·			
			Sum	mary for	Subcatchment PS2A:			
Runoff	=	1.2 c	fs @ 12.1	8 hrs, Vol	ume= 5,091 cf, Depth= 1.17"			
	Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"							
A	rea (sf)		Adj Desc	cription				
	35,762	55		ds, Good, I				
	15,344	61			ver, Good, HSG B			
	1,152	<u>98</u> 58			avement, HSG B			
	52,258 51,106	00		0% Perviou	age, UI Adjusted			
	1,152			% Impervio				
	1,152			00% Uncor				
Т	1	Olama	Mala aite e	0	Description			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
10.7	50	0.1200	0.08	(0.0)	Sheet Flow,			
0.5	130	0.0850	4.69		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
11.2	180	Total						
			Sun	nmary for	r Subcatchment PS3:			

summary for Subcatchment PS3:

2.0 cfs @ 12.26 hrs, Volume= 9,993 cf, Depth= 1.24" Runoff =

Area (sf)	CN	Adj	Description
50,666	55		Woods, Good, HSG B
42,944	61		>75% Grass cover, Good, HSG B
3,457	98		Unconnected pavement, HSG B
97,067	59	58	Weighted Average, UI Adjusted
93,610			96.44% Pervious Area
3,457			3.56% Impervious Area
3,457			100.00% Unconnected

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<u> </u>	HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLC Page 32								
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
11.5	50	0.1000	0.07		Sheet Flow,				
4.8	735	0.0250	2.55		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
16.3	785	Total							
1010		1 o tai							
			Sum	mary for	Subcatchment PS3A:				
Runoff	=	1.2 c	fs @ 12.3	5 hrs, Vol	ume= 6,620 cf, Depth= 1.17"				
Type III 2	Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"								
	<u>rea (sf)</u>	<u>CN</u> 55		ription ds, Good, I	ISC P				
	53,432 12,217	55 61			ver, Good, HSG B				
	2,305	98		Unconnected pavement, HSG B					
	67,954				age, UI Adjusted				
	65,649			1% Perviou					
	2,305		3.39	% Impervio	us Area				
	2,305		100.0	00% Uncor	inected				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	<u>(ft/ft)</u>	(ft/sec)	(cfs)					
21.8	50	0.0200	0.04		Sheet Flow, Woods: Dense underbrush n= 0.800 P2= 3.10"				
0.2	80	0.1250	5.69		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
22.0	130	Total							
			Sun	omary fo	r Subcatchment PS4				

Summary for Subcatchment PS4:

Runoff = 5.8 cfs @ 12.12 hrs, Volume= 20,662 cf, Depth= 1.44"

Area (sf)	CN	Adj	Description
48,637	55		Woods, Good, HSG B
107,523	61		>75% Grass cover, Good, HSG B
10,372	98		Unconnected pavement, HSG B
5,444	98		Unconnected roofs, HSG B
171,976	63	61	Weighted Average, UI Adjusted
156,160			90.80% Pervious Area
15,816			9.20% Impervious Area
15,816			100.00% Unconnected

Willow Road Proposed Conditions

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.5	50	0.0100	0.11		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.10"
0.1	50	0.2400	7.89		Shallow Concentrated Flow,

Unpaved Kv= 16.1 fps

7.6 100 Total

Summary for Subcatchment PS5:

Runoff = 1.5 cfs @ 12.31 hrs, Volume= 7,607 cf, Depth= 1.24"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"

A	rea (sf)	CN Description						
	48,067	55 Woods, Good, HSG B						
	23,521	61 >	75% Gras	s cover, Go	bod, HSG B			
	2,304	98 L	Inconnecte	ed pavemer	nt, HSG B			
	73,892	58 V	Veighted A	verage				
	71,588	9	6.88% Per	vious Area				
	2,304	3	.12% Impe	ervious Are	a			
	2,304	1	00.00% Ui	nconnected	1			
_				• •				
Tc	Length	Slope	Velocity	Capacity	Description			
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)				
18.6	50	0.0300	0.04		Sheet Flow,			
					Woods: Dense underbrush n= 0.800 P2= 3.10"			
0.8	180	0.0500	3.60		Shallow Concentrated Flow,			
					Unpaved Kv= 16.1 fps			
19.4	230	Total						

Summary for Subcatchment PS5A:

Runoff = 1.6 cfs @ 12.31 hrs, Volume= 8,740 cf, Depth= 1.10"

Area (sf)	CN	Adj	Description
77,272	55		Woods, Good, HSG B
16,576	61		>75% Grass cover, Good, HSG B
1,152	98		Unconnected pavement, HSG B
95,000	57	56	Weighted Average, UI Adjusted
93,848			98.79% Pervious Area
1,152			1.21% Impervious Area
1,152			100.00% Unconnected

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Tc min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
18.6	50	0.0300	0.04		Sheet Flow,
0.3	100	0.1000	5.09		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
18.9	150	Total			
noff	=	6.0 c		-	r Subcatchment PS6: ume= 22,320 cf, Depth= 1.59"
					ted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs
А	rea (sf)	CN /	Adj Deso	cription	
	67,828	55	Woo	ds, Good, H	HSG B
74,644 61 >75% Grass cover, Good, HSG B					
		61	>75	% Grass co	ver, Good, HSG B
	74,644 11,625	98			avement, HSG B
	11,625 13,498		Unco Root	onnected pa fs, HSG B	avement, HSG B
	11,625	98	Unco Root	onnected pa fs, HSG B	
1	11,625 13,498 1,343 68,938	98 98 98	Unco Root Pave 63 Weig	onnected pa fs, HSG B ed roads w/ ghted Avera	avement, HSG B curbs & sewers, HSG B age, UI Adjusted
1	11,625 13,498 1,343	98 98 98	Unco Root Pave 63 Weig 84.3	onnected pa fs, HSG B ed roads w/	avement, HSG B curbs & sewers, HSG B age, UI Adjusted is Area
	pare roCAl Tc nin) 18.6 0.3 18.9 18.9	pared by The <u>roCAD® 10.10-</u> Tc Length <u>nin) (feet)</u> 18.6 50 0.3 100 18.9 150 18.9 150 18.9 150 0ff = noff by SCS TF e III 24-hr 10 <u>Area (sf)</u> 67,828	pared by The Morin-(roCAD® 10.10-3a s/n 00 Tc Length Slope nin) (feet) (ft/ft) 18.6 50 0.0300 0.3 100 0.1000 18.9 150 Total noff = 6.0 c noff by SCS TR-20 mether e III 24-hr 10 Year Rai Area (sf) CN 7 67,828 55 5	pared by The Morin-Cameron for CAD® 10.10-3a s/n 00401 © 202 Tc Length Slope Velocity nin) (feet) (ft/ft) (ft/sec) 18.6 50 0.0300 0.04 0.3 100 0.1000 5.09 18.9 150 Total Sun off = 6.0 cfs @ 12.7 off by SCS TR-20 method, UH=S e III 24-hr 10 Year Rainfall=5.12' Area (sf) CN Adj Desc 67,828 55 Woo	pared by The Morin-Cameron Group, Inc. roCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Tc Length Slope Velocity Capacity Tc Length Slope Velocity Capacity nin) (feet) (ft/ft) (ft/sec) (cfs) 18.6 50 0.0300 0.04 0.3 100 0.1000 5.09 I8.9 150 Total Summary for noff = 6.0 cfs @ 12.14 hrs, Voltation off by SCS TR-20 method, UH=SCS, Weighe e III 24-hr 10 Year Rainfall=5.12" Area (sf) CN Adj Description 67,828 55 Woods, Good, H 55 Woods, Good, H

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8.7	50	0.0500	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.10"
0.5	170	0.1120	5.39		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
	<u>(min)</u> 8.7	8.7 50	(min) (feet) (ft/ft) 8.7 50 0.0500	(min) (feet) (ft/ft) (ft/sec) 8.7 50 0.0500 0.10	(min) (feet) (ft/ft) (ft/sec) (cfs) 8.7 50 0.0500 0.10

9.2 220 Total

11,625

Summary for Subcatchment PS7:

Runoff = 6.1 cfs @ 12.09 hrs, Volume= 18,912 cf, Depth= 2.37"

43.92% Unconnected

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"

Area (sf)	CN	Description
64,959	61	>75% Grass cover, Good, HSG B
10,888	98	Roofs, HSG B
7,062	98	Unconnected pavement, HSG B
12,647	98	Paved roads w/curbs & sewers, HSG B
95,556	73	Weighted Average
64,959		67.98% Pervious Area
30,597		32.02% Impervious Area
7,062		23.08% Unconnected

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Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)					
6.0 Direct Entry,					
Summary for Subcatchment PS8:					
Runoff = 3.8 cfs @ 12.09 hrs, Volume= 11,984 cf, Depth= 3.68"					
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"					
Area (sf) CN Description					
25,064 98 Paved roads w/curbs & sewers, HSG B 2,787 98 Unconnected pavement, HSG B					
11,222 61 >75% Grass cover, Good, HSG B					
39,073 87 Weighted Average 11,222 28.72% Pervious Area 27,851 71.28% Impervious Area 2,787 10.01% Unconnected					
Tc Length Slope Velocity Capacity Description					
(min) (feet) (ft/ft) (ft/sec) (cfs) 6.0 Direct Entry,					
0.0 Direct Entry,					
Summary for Subcatchment PS9:					
Runoff = 12.5 cfs @ 12.09 hrs, Volume= 38,613 cf, Depth= 3.09"					
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=5.12"					

Type III 24-hr 10 Year Rainfall=5.12"

Area (sf)	CN	Description
22,164	98	Paved roads w/curbs & sewers, HSG B
69,747	61	>75% Grass cover, Good, HSG B
3,523	98	Unconnected pavement, HSG B
54,442	98	Roofs, HSG B
149,876	81	Weighted Average
69,747		46.54% Pervious Area
80,129		53.46% Impervious Area
3,523		4.40% Unconnected
Tc Length (min) (feet)	Slop (ft/	
6.0		Direct Entry,

Summary for Reach DP1:

Inflow Area =	343,774 sf,	1.74% Impervious,	Inflow Depth = 1.24"	for 10 Year event
Inflow =	6.4 cfs @	12.37 hrs, Volume=	35,390 cf	
Outflow =	6.4 cfs @	12.37 hrs, Volume=	35,390 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2:

Inflow Area =	342,992 sf,	25.01% Impervious,	Inflow Depth > 1.60"	for 10 Year event
Inflow =	4.8 cfs @	12.20 hrs, Volume=	45,853 cf	
Outflow =	4.8 cfs @	12.20 hrs, Volume=	45,853 cf, Att	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2A:

Inflow Area =	99,641 sf,	30.79% Impervious,	Inflow Depth = 0.69"	for 10 Year event
Inflow =	1.2 cfs @	12.18 hrs, Volume=	5,737 cf	
Outflow =	1.2 cfs @	12.18 hrs, Volume=	5,737 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3:

Inflow Area	a =	214,366 sf,	16.46% Impervious,	Inflow Depth = 1.13"	for 10 Year event
Inflow	=	5.1 cfs @	12.23 hrs, Volume=	20,266 cf	
Outflow	=	5.1 cfs @	12.23 hrs, Volume=	20,266 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3A:

Inflow Area	a =	117,299 sf,	27.14% Impervious,	Inflow Depth = 1.05"	for 10 Year event
Inflow	=	3.1 cfs @	12.22 hrs, Volume=	10,273 cf	
Outflow	=	3.1 cfs @	12.22 hrs, Volume=	10,273 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP4:

Inflow Area =	=	455,469 sf,	37.90% Impervious,	Inflow Depth = 1.01"	for 10 Year event
Inflow =	:	5.8 cfs @	12.12 hrs, Volume=	38,315 cf	
Outflow =	:	5.8 cfs @	12.12 hrs, Volume=	38,315 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5:

Inflow Area	a =	433,386 sf,	13.96% Impervious,	Inflow Depth = 1.07"	for 10 Year event
Inflow	=	8.0 cfs @	12.17 hrs, Volume=	38,667 cf	
Outflow	=	8.0 cfs @	12.17 hrs, Volume=	38,667 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5A:

Inflow Area	a =	190,556 sf,	16.66% Impervious,	Inflow Depth = 0.55"	for 10 Year event
Inflow	=	1.6 cfs @	12.31 hrs, Volume=	8,740 cf	
Outflow	=	1.6 cfs @	12.31 hrs, Volume=	8,740 cf, Att	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Pond 1P: Detention Basin

Inflow Area =	124,154 sf, 39.42% Impervious,	Inflow Depth = 2.64" for 10 Year event
Inflow =	8.6 cfs @ 12.09 hrs, Volume=	27,277 cf
Outflow =	1.1 cfs @ 12.72 hrs, Volume=	27,175 cf, Atten= 87%, Lag= 37.8 min
Primary =	1.1 cfs @ 12.72 hrs, Volume=	27,175 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 107.79' @ 12.72 hrs Surf.Area= 5,670 sf Storage= 12,351 cf

Plug-Flow detention time= 198.5 min calculated for 27,167 cf (100% of inflow) Center-of-Mass det. time= 196.4 min (1,020.5 - 824.1)

Volume	Invert	Avail.Sto	rage Storage	Description	
#1	105.00'	26,98	B7 cf Custom	Stage Data (Prism	atic)Listed below (Recalc)
Elevatio (fee		ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
105.0 106.0)0)0	2,562 4,302	0 3,432	0 3,432	
108.0 110.0		5,832 7,589	10,134 13,421	13,566 26,987	
Device	Routing	Invert	Outlet Device:	S	
#1	Primary	98.00'	Inlet / Outlet I	Culvert L= 40.0' nvert= 98.00' / 96.00 w Area= 0.79 sf	Ke= 0.500)' S= 0.0500 '/' Cc= 0.900
#2 #3 #4	Device 1 Device 1 Device 1	105.00' 106.00' 107.60'	3.0" Vert. Ori 4.0" Vert. Ori 10.0" W x 3.0	fice/Grate C= 0.60	00 Limited to weir flow at low heads 00 Limited to weir flow at low heads cate C= 0.600
#5	Device 1	108.90'	Head (feet) 0	5' breadth Broad-C .20 0.40 0.60 0.80 i) 2.80 2.92 3.08 3	

Primary OutFlow Max=1.1 cfs @ 12.72 hrs HW=107.79' TW=0.00' (Dynamic Tailwater) **1=Culvert** (Passes 1.1 cfs of 11.5 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.4 cfs @ 7.86 fps)

-3=Orifice/Grate (Orifice Controls 0.4 cfs @ 7.80 fps)

-4=Orifice/Grate (Orifice Controls 0.2 cfs @ 1.39 fps)

-5=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond 2P: Infiltration Basin

Inflow Area =	47,383 sf, 62.31% Impervious,	Inflow Depth = 3.48" for 10 Year event
Inflow =	4.1 cfs @ 12.09 hrs, Volume=	13,749 cf
Outflow =	0.4 cfs @ 12.95 hrs, Volume=	13,660 cf, Atten= 90%, Lag= 51.8 min
Discarded =	0.2 cfs @ 12.95 hrs, Volume=	13,015 cf
Primary =	0.2 cfs @ 12.95 hrs, Volume=	646 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 109.53' @ 12.95 hrs Surf.Area= 3,532 sf Storage= 6,998 cf

Plug-Flow detention time= 401.5 min calculated for 13,657 cf (99% of inflow) Center-of-Mass det. time= 397.4 min (1,178.4 - 780.9)

Volume	Invert	: Avail.Sto	rage Storage I	Description		
#1	106.00'	8,79	99 cf Custom	Stage Data (Coni	c) Listed below (R	ecalc)
Elevatio (fee 106.0 108.0 110.0	20 20 20	urf.Area (sq-ft) 781 2,086 4,059	Inc.Store (cubic-feet) 0 2,762 6,037	Cum.Store (cubic-feet) 0 2,762 8,799	Wet.Area (sq-ft) 781 2,112 4,123	
Device	Routing	Invert	Outlet Devices			
#1	Primary	109.50'		20 0.40 0.60 0.8		
#2	Discarded	106.00'	2.85 3.07 3.2) 2.54 2.61 2.61 0 3.32 filtration over Su		

Discarded OutFlow Max=0.2 cfs @ 12.95 hrs HW=109.53' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.2 cfs)

Primary OutFlow Max=0.2 cfs @ 12.95 hrs HW=109.53' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Weir Controls 0.2 cfs @ 0.40 fps)

Summary for Pond 3P: Infiltration Basin

					Year Rainfall=5.12" Printed 11/19/2020 Page <u>39</u>	
Inflow Outflow Discarde Primary	\mathbf{O}					
Peak Ele	ev= 108.35'	@ 15.50 hrs	Surf.Area= 17,0	79 sf Storage= 5	0,106 cf	
			nin calculated for nin (1,251.5 - 80	r 51,545 cf (67% c)8.4)	of inflow)	
Volume	Inver		rage Storage [-		
#1	104.00	83,59	98 cf Custom	Stage Data (Coni	c) Listed below (R	ecalc)
Elevatio (fee		urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
104.0		8,168	0	0	8,168	
105.0		9,203	8,680	8,680	9,254	
106.0 108.0		10,294 15,794	9,743 25,893	18,424 44,316	10,400 15,959	
110.0		23,758	39,282	83,598	23,984	
Device	Routing	Invert	Outlet Devices			
#1	Primary	106.50'		Culvert L= 34.0'	Ke= 0.600	
<i>"</i>	r minary	100.00		vert= 106.50' / 100		'/' Cc= 0.900
				crete pipe, finished		
#2	Device 1	107.00'				eir flow at low heads
#3	Device 1	108.00'				eir flow at low heads
#4	Device 1	109.00'		rifice/Grate C= (
#5	Primary	109.50'	Limited to weir flow at low heads 20.0' long x 4.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.38 2.54 2.69 2.68 2.67 2.67 2.65 2.66 2.66 2.68 2.72 2.73 2.76 2.79 2.88 3.07 3.32			
#6	Discarded	104.00'	1.020 in/hr Ex	filtration over Su	rface area Phas	se-In= 0.01'
Discard	ed OutFlow	Max=0.4 cfs	@ 15.50 hrs HV	V=108.35' (Free	Discharge)	

Discarded OutFlow Max=0.4 cfs @ 15.50 hrs HW=108.35' (Free Discharge) **G=Exfiltration** (Exfiltration Controls 0.4 cfs)

Primary OutFlow Max=0.6 cfs @ 15.50 hrs HW=108.35' TW=0.00' (Dynamic Tailwater) 1=Culvert (Passes 0.6 cfs of 4.1 cfs potential flow) 2=Orifice/Grate (Orifice Controls 0.3 cfs @ 5.33 fps) -3=Orifice/Grate (Orifice Controls 0.3 cfs @ 2.02 fps) -4=Orifice/Grate (Controls 0.0 cfs) 5=Bread Created Bactangular Wair (Controls 0.0 cfc)

-5=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

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Summary for Pond 4P: Infiltration Basin

Inflow Area =	49,345 sf,	59.84% Impervious,	Inflow Depth = 2.52" for 10 Year event
Inflow =	3.3 cfs @	12.09 hrs, Volume=	10,360 cf
Outflow =	2.5 cfs @	12.18 hrs, Volume=	10,360 cf, Atten= 26%, Lag= 5.6 min
Discarded =	0.2 cfs @	12.18 hrs, Volume=	6,886 cf
Primary =	2.2 cfs @	12.18 hrs, Volume=	3,474 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 118.09' @ 12.18 hrs Surf.Area= 4,138 sf Storage= 3,140 cf

Plug-Flow detention time= 88.9 min calculated for 10,358 cf (100% of inflow) Center-of-Mass det. time= 88.9 min (868.3 - 779.3)

Volume	Inve	rt Avail.Sto	torage Storage Description			
#1	117.0	0' 4,9	951 cf Custom	n Stage Data (Coni	c) Listed below (Re	calc)
Elevatio	on	Surf.Area	Inc.Store	Cum.Store	Wet.Area	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	(sq-ft)	
117.0	00	1,691	0	0	1,691	
118.0	00	4,012	2,769	2,769	4,019	
118.5	50	4,726	2,182	4,951	4,743	
Device	Routing	Invert	Outlet Device	S		
#1	Primary	117.90'			d-Crested Rectang 30 1.00 1.20 1.40	
					2.85 2.98 3.08 3	.20 3.28 3.31
#2	Primary	118.10'	U U		d-Crested Rectang 0 1.00 1.20 1.40	
#3	Discarde	d 117.00'	3.30 3.31 3.	32	2.85 2.98 3.08 3 rface area Phase	
					- · · ·	

Discarded OutFlow Max=0.2 cfs @ 12.18 hrs HW=118.09' (Free Discharge) **-3=Exfiltration** (Exfiltration Controls 0.2 cfs)

Primary OutFlow Max=2.2 cfs @ 12.18 hrs HW=118.09' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 2.2 cfs @ 1.18 fps) 2=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond 5P: Infiltration Basin

Inflow Area =	95,556 sf, 32.02% Impervious	, Inflow Depth = 2.37" for 10 Year event
Inflow =	6.1 cfs @ 12.09 hrs, Volume	= 18,912 cf
Outflow =	0.5 cfs @ 13.63 hrs, Volume	= 18,912 cf, Atten= 92%, Lag= 92.3 min
Discarded =	0.5 cfs @ 13.63 hrs, Volume	= 18,912 cf
Primary =	0.0 cfs @ 0.00 hrs, Volume	= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

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Peak Elev= 122.74' @ 13.63 hrs Surf.Area= 8,779 sf Storage= 8,325 cf

Plug-Flow detention time= 179.1 min calculated for 18,906 cf (100% of inflow) Center-of-Mass det. time= 179.0 min (1,017.8 - 838.8)

Volume	Inve	rt Avail.Sto	rage Storag	ge Description	
#1	121.5	0' 20,86	63 cf Custo	om Stage Data (P	rismatic)Listed below (Recalc)
Elevatio		Surf.Area	Inc.Store	Cum.Store	
(fee	1	(sq-ft)	(cubic-feet)	(cubic-feet)	
121.5	-	2,680	0	0	
121.7	5	4,316	875	875	
122.0	0	7,408	1,466	2,340	
124.0	0	11,115	18,523	20,863	
Device	Routing	Invert	Outlet Device	ces	
#1	Primary	122.75'		0.20 0.40 0.60	oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			Coef. (Engli 2.85 3.07		61 2.60 2.66 2.70 2.77 2.89 2.88
#2	Discardeo	d 121.50'	2.410 in/hr	Exfiltration over	Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.5 cfs @ 13.63 hrs HW=122.74' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.5 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=121.50' TW=0.00' (Dynamic Tailwater) ☐ 1=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond 6P: Recharge Trench

Inflow Area =	27,221 sf,100.00% Impervious,	Inflow Depth = 4.88" for 10 Year event
Inflow =	3.1 cfs @ 12.08 hrs, Volume=	11,077 cf
Outflow =	3.1 cfs @ 12.08 hrs, Volume=	11,077 cf, Atten= 0%, Lag= 0.0 min
Discarded =	0.0 cfs @ 6.83 hrs, Volume=	3,460 cf
Primary =	2.5 cfs @ 12.08 hrs, Volume=	7,437 cf
Secondary =	0.6 cfs @ 12.08 hrs, Volume=	179 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 120.14' @ 12.08 hrs Surf.Area= 720 sf Storage= 490 cf

Plug-Flow detention time= 44.0 min calculated for 11,077 cf (100% of inflow) Center-of-Mass det. time= 44.0 min (791.7 - 747.6)

Volume	Invert	Avail.Storage	Storage Description
#1	115.50'	392 cf	Custom Stage Data (Prismatic)Listed below (Recalc)
			1,080 cf Overall - 101 cf Embedded = 979 cf x 40.0% Voids
#2	116.17'	94 cf	6.0" Round Pipe Storage Inside #1
			L= 480.0'
			101 cf Overall - 0.1" Wall Thickness = 94 cf
#3	117.00'	12 cf	0.50'D x 10.00'H Vertical Cone/Cylinder x 6 -Impervious
		498 cf	Total Available Storage

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Elevation	Surf.Area	Inc.Store	Cum.Store	
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)	
115.50	720	0	0	
117.00	720	1,080	1,080	
Device Routing	Invert	Outlet Devices		

#1	Discarded	115.50'	2.410 in/hr Exfiltration over Sur	face area	Phase-In= 0.01'
#2	Primary	118.00'	4.0" Horiz. Orifice/Grate X 4.00	C= 0.600	
			Limited to weir flow at low heads		
#3	Secondary	120.00'	4.0" Horiz. Orifice/Grate X 4.00	C= 0.600	
			Limited to weir flow at low heads		

Discarded OutFlow Max=0.0 cfs @ 6.83 hrs HW=115.62' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=2.5 cfs @ 12.08 hrs HW=120.14' TW=117.99' (Dynamic Tailwater) **2=Orifice/Grate** (Orifice Controls 2.5 cfs @ 7.04 fps)

Secondary OutFlow Max=0.6 cfs @ 12.08 hrs HW=120.14' TW=0.00' (Dynamic Tailwater) -3=Orifice/Grate (Orifice Controls 0.6 cfs @ 1.80 fps)

Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment PS1:	Runoff Area=343,774 sf 1.74% Impervious Runoff Depth=1.94" Flow Length=197' Tc=22.5 min CN=58 Runoff=10.7 cfs 55,579 cf
Subcatchment PS10:	Runoff Area=78,810 sf 59.90% Impervious Runoff Depth=4.36" Tc=6.0 min CN=83 Runoff=9.1 cfs 28,643 cf
SubcatchmentPS11:	Runoff Area=72,767 sf 37.18% Impervious Runoff Depth=3.94" Tc=6.0 min CN=79 Runoff=7.7 cfs 23,890 cf
SubcatchmentPS12:	Runoff Area=45,344 sf 3.81% Impervious Runoff Depth=2.29" Tc=6.0 min CN=62 Runoff=2.7 cfs 8,658 cf
SubcatchmentPS13:	Runoff Area=25,606 sf 30.26% Impervious Runoff Depth=3.23" Tc=6.0 min CN=72 Runoff=2.2 cfs 6,897 cf
SubcatchmentPS14:	Runoff Area=22,124 sf 10.42% Impervious Runoff Depth=2.38" Tc=6.0 min UI Adjusted CN=63 Runoff=1.4 cfs 4,390 cf
SubcatchmentPS15:	Runoff Area=21,777 sf 100.00% Impervious Runoff Depth=6.05" Tc=6.0 min CN=98 Runoff=3.1 cfs 10,982 cf
SubcatchmentPS16:	Runoff Area=21,777 sf 100.00% Impervious Runoff Depth=6.05" Tc=6.0 min CN=98 Runoff=3.1 cfs 10,982 cf
SubcatchmentPS17:	Runoff Area=27,221 sf 100.00% Impervious Runoff Depth=6.05" Tc=6.0 min CN=98 Runoff=3.9 cfs 13,727 cf
Subcatchment PS2:	Runoff Area=119,197 sf 5.18% Impervious Runoff Depth=2.03" Flow Length=520' Tc=13.7 min UI Adjusted CN=59 Runoff=4.8 cfs 20,129 cf
SubcatchmentPS2A:	Runoff Area=52,258 sf 2.20% Impervious Runoff Depth=1.85" Flow Length=180' Tc=11.2 min UI Adjusted CN=57 Runoff=2.0 cfs 8,077 cf
Subcatchment PS3:	Runoff Area=97,067 sf 3.56% Impervious Runoff Depth=1.94" Flow Length=785' Tc=16.3 min UI Adjusted CN=58 Runoff=3.4 cfs 15,693 cf
Subcatchment PS3A:	Runoff Area=67,954 sf 3.39% Impervious Runoff Depth=1.85" Flow Length=130' Tc=22.0 min UI Adjusted CN=57 Runoff=2.0 cfs 10,503 cf
Subcatchment PS4:	Runoff Area=171,976 sf 9.20% Impervious Runoff Depth=2.20" Flow Length=100' Tc=7.6 min UI Adjusted CN=61 Runoff=9.3 cfs 31,558 cf
Subcatchment PS5:	Runoff Area=73,892 sf 3.12% Impervious Runoff Depth=1.94" Flow Length=230' Tc=19.4 min CN=58 Runoff=2.4 cfs 11,946 cf
Subcatchment PS5A:	Runoff Area=95,000 sf 1.21% Impervious Runoff Depth=1.77" Flow Length=150' Tc=18.9 min UI Adjusted CN=56 Runoff=2.8 cfs 14,016 cf

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Subcatchment PS6: Flow Leng	Runoff Area=168,938 sf 15.67% Impervious Runoff Depth=2.38" gth=220' Tc=9.2 min UI Adjusted CN=63 Runoff=9.4 cfs 33,525 cf
SubcatchmentPS7:	Runoff Area=95,556 sf 32.02% Impervious Runoff Depth=3.33" Tc=6.0 min CN=73 Runoff=8.6 cfs 26,523 cf
SubcatchmentPS8:	Runoff Area=39,073 sf 71.28% Impervious Runoff Depth=4.80" Tc=6.0 min CN=87 Runoff=4.9 cfs 15,614 cf
SubcatchmentPS9:	Runoff Area=149,876 sf 53.46% Impervious Runoff Depth=4.15" Tc=6.0 min CN=81 Runoff=16.6 cfs 51,819 cf
Reach DP1:	Inflow=10.7 cfs 55,579 cf Outflow=10.7 cfs 55,579 cf
Reach DP2:	Inflow=9.5 cfs 69,162 cf Outflow=9.5 cfs 69,162 cf
Reach DP2A:	Inflow=3.5 cfs 11,846 cf Outflow=3.5 cfs 11,846 cf
Reach DP3:	Inflow=8.0 cfs 32,577 cf Outflow=8.0 cfs 32,577 cf
Reach DP3A:	Inflow=5.3 cfs 16,884 cf Outflow=5.3 cfs 16,884 cf
Reach DP4:	Inflow=9.4 cfs 69,765 cf Outflow=9.4 cfs 69,765 cf
Reach DP5:	Inflow=13.0 cfs 64,256 cf Outflow=13.0 cfs 64,256 cf
Reach DP5A:	Inflow=4.3 cfs 18,784 cf Outflow=4.3 cfs 18,784 cf
Pond 1P: Detention Basin	Peak Elev=108.48' Storage=16,491 cf Inflow=11.8 cfs 37,300 cf Outflow=1.9 cfs 37,187 cf
Pond 2P: Infiltration Basin Discarded=0.2	Peak Elev=109.61' Storage=7,317 cf Inflow=5.3 cfs 17,879 cf 2 cfs 13,859 cf Primary=2.0 cfs 3,769 cf Outflow=2.2 cfs 17,628 cf
Pond 3P: Infiltration Basin Discarded=0.5 of	Peak Elev=109.02' Storage=62,346 cf Inflow=32.3 cfs 102,304 cf cfs 36,917 cf Primary=1.2 cfs 38,207 cf Outflow=1.7 cfs 75,124 cf
	Peak Elev=118.13' Storage=3,313 cf Inflow=4.0 cfs 13,999 cf .2 cfs 8,102 cf Primary=3.4 cfs 5,898 cf Outflow=3.7 cfs 13,999 cf
	Peak Elev=122.93' Storage=10,008 cf Inflow=8.6 cfs 26,523 cf 5 cfs 21,754 cf Primary=1.9 cfs 4,768 cf Outflow=2.4 cfs 26,523 cf
Pond 6P: Recharge Trench Discarded=0.0 cfs 3,635 cf Primary=2.6	Peak Elev=120.52' Storage=490 cf Inflow=3.9 cfs 13,727 cf 5 cfs 9,609 cf Secondary=1.2 cfs 483 cf Outflow=3.9 cfs 13,727 cf

Total Runoff Area = 1,789,987 sf Runoff Volume = 403,151 cf Average Runoff Depth = 2.70" 79.88% Pervious = 1,429,771 sf 20.12% Impervious = 360,216 sf

Summary for Subcatchment PS1:

Runoff = 10.7 cfs @ 12.33 hrs, Volume= 55,579 cf, Depth= 1.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

A	rea (sf)	CN E	Description				
2	02,359	55 V	Woods, Good, HSG B				
1	35,428	61 >	75% Gras	s cover, Go	ood, HSG B		
	3,265	98 L	Inconnecte	ed pavemer	nt, HSG B		
	2,722	<u>98 L</u>	Inconnecte	ed roofs, HS	SG B		
343,774 58 Weighted Average							
3	37,787	g	98.26% Pervious Area				
	5,987 1.			1.74% Impervious Area			
	5,987 100.00% Unconnected			nconnected			
Тс	Length	Slope	Velocity	Capacity	Description		
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)			
21.8	50	0.0200	0.04		Sheet Flow,		
					Woods: Dense underbrush n= 0.800 P2= 3.10"		
0.7	147	0.0480	3.53		Shallow Concentrated Flow,		
					Unpaved Kv= 16.1 fps		
22.5	197	Total					

Summary for Subcatchment PS10:

Runoff = 9.1 cfs @ 12.09 hrs, Volume= 28,643 cf, Depth= 4.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

A	rea (sf)	CN	Description							
	43,871	98	Paved road	s w/curbs &	& sewers, HSG B					
	31,599	61	>75% Gras	s cover, Go	ood, HSG B					
	3,340	98	Unconnecte	ed pavemer	nt, HSG B					
	78,810	83	Weighted A	verage						
	31,599		40.10% Pervious Area							
	47,211	59.90% Impervious Area								
	3,340		7.07% Unco	onnected						
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description					
6.0					Direct Entry,					

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Summary for Subcatchment PS11:

Runoff = 7.7 cfs @ 12.09 hrs, Volume= 23,890 cf, Depth= 3.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

Α	rea (sf)	CN	Description						
	13,154	55	Woods, Go	od, HSG B	3				
	21,827	61	>75% Gras	s cover, Go	lood, HSG B				
	10,719	98	Paved road	s w/curbs &	& sewers, HSG B				
	16,333	98	Roofs, HSG	БB					
	10,734	96	Gravel surfa	ace, HSG E	В				
	72,767	79	Weighted Average						
	45,715		62.82% Pervious Area						
	27,052		37.18% Impervious Area						
_				•	— • • •				
Tc	Length	Slope	,	Capacity	•				
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)					
6.0					Direct Entry,				

Summary for Subcatchment PS12:

Runoff	=	2.7 cfs @	12.09 hrs,	Volume=	8,658 cf, Depth= 2.29"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

Area (sf)	CN	Description					
43,615	61	>75% Gras	s cover, Go	ood, HSG B			
1,729	98	Unconnecte	ed pavemer	nt, HSG B			
45,344	62	Weighted Average					
43,615		96.19% Pervious Area					
1,729		3.81% Impervious Area					
1,729		100.00% Ui	nconnected	l			
Tc Length	Slop	be Velocity	Capacity	Description			
(min) (feet)	(ft/		(cfs)	Decemption			
6.0	•			Direct Entry,			

Summary for Subcatchment PS13:

Runoff = 2.2 cfs @ 12.09 hrs, Volume= 6,897 cf, Depth= 3.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

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Type III 24-hr 25 Year Rainfall=6.29" Printed 11/19/2020 HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLC Page 48

Area (s	f) CN	Description					
17,85	7 61	>75% Grass cover, Good, HSG B					
5,44	4 98	Roofs, HSG B					
2,30	5 98	Unconnected pavement, HSG B					
25,60	6 72	Weighted Average					
17,85	7	69.74% Pervious Area					
7,74	9	30.26% Impervious Area					
2,30	5	29.75% Unconnected					
Tc Leng	, i						
(min) (fee	et) (ft/	ft) (ft/sec) (cfs)					

6.0

Direct Entry,

Summary for Subcatchment PS14:

Runoff	=	1.4 cfs @	12.09 hrs,	Volume=	4,390 cf, Depth= 2.38"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

_	Ai	rea (sf)	CN	Adj	Description				
-		19,819	61	:	>75% Grass cover, Good, HSG B				
_		2,305	98		Unconnected pavement, HSG B				
		22,124	65	63	Weighted Average, UI Adjusted				
		19,819			89.58% Pervious Área				
		2,305			10.42% Impervious Area				
		2,305			100.00% Unconnected				
	_								
	Tc	Length	Slope	Velo	city Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/s	sec) (cfs)				

6.0

Direct Entry,

Summary for Subcatchment PS15:

Runoff = 3.1 cfs @ 12.08 hrs, Volume= 10,982 cf, Depth= 6.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

A	rea (sf)	CN	Description		
	21,777	98	Roofs, HSG	βB	
	21,777		100.00% In	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Summary for Subcatchment PS16:

Runoff = 3.1 cfs @ 12.08 hrs, Volume= 10,982 cf, Depth= 6.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

Area (sf	f) CN Description	
21,77	7 98 Roofs, HSG B	
21,77	7 100.00% Impervious Area	
Tc Leng	gth Slope Velocity Capacity Description	
(min) (fee	et) (ft/ft) (ft/sec) (cfs)	
6.0	Direct Entry,	
	Summary for Subcatchment PS17:	
Runoff =	3.9 cfs @ 12.08 hrs, Volume= 13,727 cf, Depth= 6.05"	
	S TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs 25 Year Rainfall=6.29"	
Area (sf	f) CN Description	
27,22	21 98 Roofs, HSG B	
27,22		
,		
Tc Leng	gth Slope Velocity Capacity Description	
(min) (fee	et) (ft/ft) (ft/sec) (cfs)	
6.0	Direct Entry,	

Summary for Subcatchment PS2:

Runoff = 4.8 cfs @ 12.20 hrs, Volume= 20,129 cf, Depth= 2.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

Area (sf)	CN	Adj	Description
61,041	55		Woods, Good, HSG B
51,977	61		>75% Grass cover, Good, HSG B
3,457	98		Unconnected pavement, HSG B
2,722	98		Unconnected roofs, HSG B
119,197	60	59	Weighted Average, UI Adjusted
113,018			94.82% Pervious Area
6,179			5.18% Impervious Area
6,179			100.00% Unconnected

Prepare	d by The	Morin-C		Group, Inc	Type III 24-hr 25 Year Rainfall=6.29" Printed 11/19/2020 Software Solutions LLC Page 50
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.5	50	0.1000	0.07		Sheet Flow,
2.2	470	0.0500	3.60		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
13.7	520	Total			
			Sum	mary for	Subcatchment PS2A:
Runoff	=	2.0 ct	fs @ 12.1	7 hrs, Vol	ume= 8,077 cf, Depth= 1.85"
Type III :	24-hr 25	Year Rai	nfall=6.29'		ted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs
A	<u>rea (sf)</u>			ription	
	35,762 15,344	55 61		ds, Good, H ⁄a Grass co	ver, Good, HSG B
	1,152	98			avement, HSG B
	52,258 51,106 1,152 1,152		57 Weig 97.8 2.20		age, UI Adjusted is Area us Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.7	50	0.1200	0.08		Sheet Flow,
0.5	130	0.0850	4.69		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
11.2	180	Total			
			Sun	nmary for	r Subcatchment PS3:

Summary for Subcatchment PS3:

Runoff = 3.4 cfs @ 12.24 hrs, Volume= 15,693 cf, Depth= 1.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

Area (sf)	CN	Adj	Description
50,666	55		Woods, Good, HSG B
42,944	61		>75% Grass cover, Good, HSG B
3,457	98		Unconnected pavement, HSG B
97,067	59	58	Weighted Average, UI Adjusted
93,610			96.44% Pervious Area
3,457			3.56% Impervious Area
3,457			100.00% Unconnected

Prepare	d by The	Morin-C		Group, Inc	Type III 24-hr 25 Year Rainfall=6.29"c.Printed 11/19/2020D Software Solutions LLCPage 51
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.5	50	0.1000	0.07		Sheet Flow,
4.8	735	0.0250	2.55		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
16.3	785	Total			
			Sum	mary for	Subcatchment PS3A:
Runoff	=	2.0 c	fs @ 12.3	84 hrs, Volu	ume= 10,503 cf, Depth= 1.85"
			nod, UH=S nfall=6.29"		nted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs
A	rea (sf)	CN A	Adj Desc	ription	
	53,432 12,217 2,305	55 61 98	>75%		HSG B iver, Good, HSG B avement, HSG B
	67,954	58			age, UI Adjusted
	65,649 2,305			1% Perviou % Impervio	
	2,305			0% Uncon	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.8	50	0.0200	0.04	(010)	Sheet Flow,
0.2	80	0.1250	5.69		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
22.0	130	Total			
			Sun	nmary for	r Subcatchment PS4:

Summary for Subcatchment PS4:

Runoff = 9.3 cfs @ 12.12 hrs, Volume= 31,558 cf, Depth= 2.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

CN	Adj	Description
55		Woods, Good, HSG B
61		>75% Grass cover, Good, HSG B
98		Unconnected pavement, HSG B
98		Unconnected roofs, HSG B
63	61	Weighted Average, UI Adjusted
		90.80% Pervious Area
		9.20% Impervious Area
		100.00% Unconnected
	55 61 98 98	55 61 98 98

Willow Road Proposed Conditions

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	7.5	50	0.0100	0.11		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.10"
	0.1	50	0.2400	7.89		Shallow Concentrated Flow,
_						Unpaved Kv= 16.1 fps

7.6 100 Total

Summary for Subcatchment PS5:

Runoff = 2.4 cfs @ 12.29 hrs, Volume= 11,946 cf, Depth= 1.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

A	rea (sf)	CN E	Description		
	48,067	55 V	Voods, Go	od, HSG B	
	23,521	61 >	75% Gras	s cover, Go	bod, HSG B
	2,304	98 L	Inconnecte	ed pavemei	nt, HSG B
	73,892	58 V	Veighted A	verage	
	71,588	9	6.88% Per	vious Area	l
	2,304	3	.12% Impe	ervious Are	а
	2,304	1	00.00% Ui	nconnected	t
-				o	
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
18.6	50	0.0300	0.04		Sheet Flow,
					Woods: Dense underbrush n= 0.800 P2= 3.10"
0.8	180	0.0500	3.60		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
19.4	230	Total			

Summary for Subcatchment PS5A:

Runoff = 2.8 cfs @ 12.29 hrs, Volume= 14,016 cf, Depth= 1.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

Area (sf)	CN	Adj	Description
77,272	55		Woods, Good, HSG B
16,576	61		>75% Grass cover, Good, HSG B
1,152	98		Unconnected pavement, HSG B
95,000	57	56	Weighted Average, UI Adjusted
93,848			98.79% Pervious Area
1,152			1.21% Impervious Area
1,152			100.00% Unconnected

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Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	
18.6 50 0.0300 0.04 Sheet Flow, Woods: Dense underbrush n= 0.800 P2= 3.10"	
0.3 100 0.1000 5.09 Shallow Concentrated Flow, Unpaved Kv= 16.1 fps	
18.9 150 Total	
Summary for Subcatchment PS6:	
Runoff = 9.4 cfs @ 12.14 hrs, Volume= 33,525 cf, Depth= 2.38"	
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"	
Area (sf) CN Adj Description	
67,828 55 Woods, Good, HSG B	
74,644 61 >75% Grass cover, Good, HSG B	
11,625 98 Unconnected pavement, HSG B	
13,498 98 Roofs, HSG B	
1,343 98 Paved roads w/curbs & sewers, HSG B	
168,938 64 63 Weighted Average, UI Adjusted	
142,472 84.33% Pervious Area	
26,466 15.67% Impervious Area	
11,625 43.92% Unconnected	
TcLengthSlopeVelocityCapacityDescription(min)(feet)(ft/ft)(ft/sec)(cfs)8.7500.05000.10Sheet Flow,	

 8.7
 50
 0.0500
 0.10
 Sheet Flow, Woods: Light underbrush
 n= 0.400
 P2= 3.10"

 0.5
 170
 0.1120
 5.39
 Shallow Concentrated Flow, Unpaved
 Unpaved
 Kv= 16.1 fps

9.2 220 Total

Summary for Subcatchment PS7:

Runoff = 8.6 cfs @ 12.09 hrs, Volume= 26,523 cf, Depth= 3.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

Area (sf)	CN	Description
64,959	61	>75% Grass cover, Good, HSG B
10,888	98	Roofs, HSG B
7,062	98	Unconnected pavement, HSG B
12,647	98	Paved roads w/curbs & sewers, HSG B
95,556	73	Weighted Average
64,959		67.98% Pervious Area
30,597		32.02% Impervious Area
7,062		23.08% Unconnected

Willow Road Proposed Conditions Prepared by The Morin-Cameron Group, Inc. HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solution					<i>Il 24-hr 25 Year Rainfall=6.29"</i> Printed 11/19/2020 <u>Page 54</u>		
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description		
6.0					Direct Entry	y,	
			Su	mmary fo	r Subcatch	ment PS8	3:
Runoff	=	4.9 0	cfs @ 12	.09 hrs, Vol	ume=	15,614 cf,	Depth= 4.80"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"						0-36.00 hrs, dt= 0.01 hrs	
A	rea (sf)	CN I	Descriptio	n			
	25,064 2,787 11,222	98	Unconnec	ds w/curbs & ted pavemei ss cover, Go		G B	
	39,073 11,222 27,851 2,787	-	71.28% In	Average ervious Area pervious Ar nconnected			
Tc (min)	Length (feet)	Slope (ft/ft)			Description		
6.0					Direct Entry	y ,	
	Summary for Subcatchment PS9:						
Runoff	=	16.6 0	cfs @ 12	.09 hrs, Vol	ume=	51,819 cf,	Depth= 4.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Year Rainfall=6.29"

Ar	ea (sf)	CN	Description				
	22,164	98	Paved road	s w/curbs &	& sewers, HSG B		
(69,747	61	>75% Gras	s cover, Go	ood, HSG B		
	3,523	98	Unconnecte	ed pavemer	ent, HSG B		
	54,442	98	Roofs, HSG	БB			
14	49,876	81	Weighted A	verage			
(69,747		46.54% Pervious Area				
8	30,129		53.46% Impervious Area				
	3,523		4.40% Unco	onnected			
Та	Longth	Slope	Volocity	Conocity	Description		
	Length	Slope		Capacity	•		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
6.0					Direct Entry,		

Summary for Reach DP1:

Inflow Area =	343,774 sf,	1.74% Impervious,	Inflow Depth = 1.94"	for 25 Year event
Inflow =	10.7 cfs @	12.33 hrs, Volume=	55,579 cf	
Outflow =	10.7 cfs @	12.33 hrs, Volume=	55,579 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2:

Inflow Area =	342,992 sf,	25.01% Impervious,	Inflow Depth > 2.42"	for 25 Year event
Inflow =	9.5 cfs @	12.26 hrs, Volume=	69,162 cf	
Outflow =	9.5 cfs @	12.26 hrs, Volume=	69,162 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2A:

Inflow Area	a =	99,641 sf,	30.79% Impervious,	Inflow Depth = 1.43 "	for 25 Year event
Inflow	=	3.5 cfs @	12.29 hrs, Volume=	11,846 cf	
Outflow	=	3.5 cfs @	12.29 hrs, Volume=	11,846 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3:

Inflow Area	a =	214,366 sf,	16.46% Impervious,	Inflow Depth = 1.82"	for 25 Year event
Inflow	=	8.0 cfs @	12.22 hrs, Volume=	32,577 cf	
Outflow	=	8.0 cfs @	12.22 hrs, Volume=	32,577 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3A:

Inflow Area =	117,299 sf,	27.14% Impervious,	Inflow Depth = 1.73 "	for 25 Year event
Inflow =	5.3 cfs @	12.12 hrs, Volume=	16,884 cf	
Outflow =	5.3 cfs @	12.12 hrs, Volume=	16,884 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP4:

Inflow Area =	455,469 sf,	37.90% Impervious,	Inflow Depth = 1.84"	for 25 Year event
Inflow =	9.4 cfs @	12.12 hrs, Volume=	69,765 cf	
Outflow =	9.4 cfs @	12.12 hrs, Volume=	69,765 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5:

Inflow Area =	433,386 sf,	13.96% Impervious,	Inflow Depth = 1.78"	for 25 Year event
Inflow =	13.0 cfs @	12.16 hrs, Volume=	64,256 cf	
Outflow =	13.0 cfs @	12.16 hrs, Volume=	64,256 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5A:

Inflow Area	a =	190,556 sf,	16.66% Impervious,	Inflow Depth = 1.18"	for 25 Year event
Inflow	=	4.3 cfs @	12.40 hrs, Volume=	18,784 cf	
Outflow	=	4.3 cfs @	12.40 hrs, Volume=	18,784 cf, Att	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Pond 1P: Detention Basin

Inflow Area =	124,154 sf, 39.42% Imperviou	us, Inflow Depth = 3.61" for 25 Year event
Inflow =	11.8 cfs @ 12.09 hrs, Volum	e= 37,300 cf
Outflow =	1.9 cfs @ 12.58 hrs, Volum	e= 37,187 cf, Atten= 84%, Lag= 29.3 min
Primary =	1.9 cfs @ 12.58 hrs, Volum	e= 37,187 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 108.48' @ 12.58 hrs Surf.Area= 6,257 sf Storage= 16,491 cf

Plug-Flow detention time= 180.5 min calculated for 37,187 cf (100% of inflow) Center-of-Mass det. time= 178.6 min (994.8 - 816.1)

Volume	Invert	Avail.Sto	rage Storag	e Description	
#1	105.00'	26,98	B7 cf Custo	m Stage Data (Pris	smatic)Listed below (Recalc)
_	-	<i>.</i> .		a a /	
Elevatio	on Su	ırf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
105.0	00	2,562	0	0	
106.0	00	4,302	3,432	3,432	
108.0)0	5,832	10,134	13,566	
110.0	00	7,589	13,421	26,987	
Device	Routing	Invert	Outlet Devic	es	
#1	Primary	98.00'	12.0" Roun	d Culvert L= 40.0	' Ke= 0.500
			Inlet / Outlet	Invert= 98.00' / 96.	.00' S= 0.0500 '/' Cc= 0.900
			n= 0.012, F	low Area= 0.79 sf	
#2	Device 1	105.00'	3.0" Vert. O	rifice/Grate C= 0.	.600 Limited to weir flow at low heads
#3	Device 1	106.00'	4.0" Vert. O	rifice/Grate C= 0.	.600 Limited to weir flow at low heads
#4	Device 1	107.60'		0" H Vert. Orifice/	
			Limited to w	eir flow at low head	s
#5	Device 1	108.90'	4.0' long x	0.5' breadth Broad	d-Crested Rectangular Weir
				0.20 0.40 0.60 0.	
				sh) 2.80 2.92 3.08	
			, u		

Primary OutFlow Max=1.9 cfs @ 12.58 hrs HW=108.48' TW=0.00' (Dynamic Tailwater) **1=Culvert** (Passes 1.9 cfs of 11.9 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 0.4 cfs @ 8.82 fps)

-3=Orifice/Grate (Orifice Controls 0.6 cfs @ 7.33 fps)

-4=Orifice/Grate (Orifice Controls 0.9 cfs @ 4.19 fps)

-5=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond 2P: Infiltration Basin

Inflow Area =	47,383 sf, 62.31% Impervious,	Inflow Depth = 4.53" for 25 Year event
Inflow =	5.3 cfs @ 12.09 hrs, Volume=	17,879 cf
Outflow =	2.2 cfs @ 12.31 hrs, Volume=	17,628 cf, Atten= 59%, Lag= 13.3 min
Discarded =	0.2 cfs @ 12.31 hrs, Volume=	13,859 cf
Primary =	2.0 cfs @ 12.31 hrs, Volume=	3,769 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 109.61' @ 12.31 hrs Surf.Area= 3,628 sf Storage= 7,317 cf

Plug-Flow detention time= 334.2 min calculated for 17,623 cf (99% of inflow) Center-of-Mass det. time= 325.3 min (1,103.3 - 778.0)

Volume	Inver	t Avail.Sto	rage Storage	Description		
#1	106.00	' 8,7	99 cf Custom	Stage Data (Coni	c)Listed below (Re	ecalc)
Elevatio (fee 106.0 108.0 110.0	et) 00 00	Gurf.Area (sq-ft) 781 2,086 4,059	Inc.Store (cubic-feet) 0 2,762 6,037	Cum.Store (cubic-feet) 0 2,762 8,799	Wet.Area (sq-ft) 781 2,112 4,123	
Device	Routing	Invert	Outlet Devices	6		
#1	Primary	109.50'		2.0' breadth Broad 20 0.40 0.60 0.8 0		
#2	Discarded	106.00'	2.85 3.07 3.2) 2.54 2.61 2.61 0 3.32 filtration over Su		

Discarded OutFlow Max=0.2 cfs @ 12.31 hrs HW=109.61' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.2 cfs)

Primary OutFlow Max=2.0 cfs @ 12.31 hrs HW=109.61' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Weir Controls 2.0 cfs @ 0.86 fps)

Summary for Pond 3P: Infiltration Basin

Prepare	ed by The N		on Group, Inc.	Tyµ oftware Solutions Ll		Year Rainfall=6.29" Printed 11/19/2020 Page 58
Inflow A Inflow Outflow Discarde Primary	= = ed =	32.3 cfs @ 1 1.7 cfs @ 1 0.5 cfs @ 1	5.31% Imperviou 2.09 hrs, Volum 4.44 hrs, Volum 4.44 hrs, Volum 4.44 hrs, Volum	ne= 75,124 ne= 36,917	cf cf, Atten= 95% ′cf	Year event , Lag= 141.1 min
Routing	by Dyn-Sto	r-Ind method, ⁻	Fime Span= 0.00	0-36.00 hrs, dt= 0.0 51 sf Storage= 62)1 hrs	
Center-o	of-Mass det	. time= 380.5 n	nin (1,181.8 - 80	,	f inflow)	
Volume #1	Inver 104.00		rage Storage E 98 cf Custom \$	Description Stage Data (Conic) isted below (R	
π I	104.00	00,00		Stage Data (Sonn		
Elevatio (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft <u>)</u>	
104.0	00	8,168	0	0	8,168	
105.0	00	9,203	8,680	8,680	9,254	
106.0		10,294	9,743	18,424	10,400	
108.0		15,794	25,893	44,316	15,959	
110.0	00	23,758	39,282	83,598	23,984	
Device	Routing	Invert	Outlet Devices			
#1	Primary	106.50'		Culvert L= 34.0' vert= 106.50' / 106		'/' Co- 0.900
				crete pipe, finished		
#2	Device 1	107.00'				eir flow at low heads
#3	Device 1	108.00'				eir flow at low heads
#4	Device 1	109.00'		rifice/Grate C= 0		
				flow at low heads		
#5	Primary	109.50'	Head (feet) 0.2	.0' breadth Broad 20 0.40 0.60 0.80 0 4.00 4.50 5.00	0 1.00 1.20 1.4	ngular Weir 0 1.60 1.80 2.00
			Coef. (English) 2.68 2.72 2.73	2.38 2.54 2.69 3 2.76 2.79 2.88	2.68 2.67 2.67 3.07 3.32	
#6	Discarded	104.00'	1.020 in/hr Ext	filtration over Sur	face area Phas	se-In= 0.01'
Discard	ed OutFlov	v Max=0.5 cfs	@ 14 44 hrs HV	V=109.02' (Free I	Discharge)	

Discarded OutFlow Max=0.5 cfs @ 14.44 hrs HW=109.02' (Free Discharge) **G=Exfiltration** (Exfiltration Controls 0.5 cfs)

Primary OutFlow Max=1.2 cfs @ 14.44 hrs HW=109.02' TW=0.00' (Dynamic Tailwater) 1=Culvert (Passes 1.2 cfs of 5.0 cfs potential flow) 2=Orifice/Grate (Orifice Controls 0.3 cfs @ 6.63 fps)

-3=Orifice/Grate (Orifice Controls 0.8 cfs @ 4.22 fps) -4=Orifice/Grate (Weir Controls 0.1 cfs @ 0.45 fps)

-5=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

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Summary for Pond 4P: Infiltration Basin

Inflow Area =	49,345 sf,	59.84% Impervious,	Inflow Depth = 3.40" for 25 Year event
Inflow =	4.0 cfs @	12.09 hrs, Volume=	13,999 cf
Outflow =	3.7 cfs @	12.14 hrs, Volume=	13,999 cf, Atten= 8%, Lag= 2.8 min
Discarded =	0.2 cfs @	12.14 hrs, Volume=	8,102 cf
Primary =	3.4 cfs @	12.14 hrs, Volume=	5,898 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 118.13' @ 12.14 hrs Surf.Area= 4,196 sf Storage= 3,313 cf

Plug-Flow detention time= 79.7 min calculated for 13,995 cf (100% of inflow) Center-of-Mass det. time= 79.6 min (860.1 - 780.5)

Volume	Inve	rt Avail.Sto	rage Storage	Description		
#1	117.00	0' 4,9	51 cf Custom	Stage Data (Coni	c) Listed below (Rec	alc)
Elevatio	9 nc	Surf.Area	Inc.Store	Cum.Store	Wet.Area	
(fee		(sq-ft)	(cubic-feet)	(cubic-feet)	(sq-ft)	
117.0	00	1,691	0	0	1,691	
118.0	00	4,012	2,769	2,769	4,019	
118.5	50	4,726	2,182	4,951	4,743	
Device	Routing	Invert	Outlet Devices	6		
#1	Primary	117.90'			d-Crested Rectangu	
			()	.20 0.40 0.60 0.8	0 1.00 1.20 1.40	1.60 1.80 2.00
			2.50 3.00		205 200 200 20	20 2 20 2 21
			3.30 3.31 3.3		2.85 2.98 3.08 3.2	20 3.20 3.31
#2	Primary	118.10'			d-Crested Rectangu	ılar Weir
	i iiiiai y	110110	U		0 1.00 1.20 1.40	
			2.50 3.00			
					2.85 2.98 3.08 3.2	20 3.28 3.31
			3.30 3.31 3.3			
#3	Discardeo	117.00'	2.410 in/hr Ex	diltration over Su	rface area Phase-	ln= 0.01'
.			0 40 44 5 1			

Discarded OutFlow Max=0.2 cfs @ 12.14 hrs HW=118.13' (Free Discharge) **-3=Exfiltration** (Exfiltration Controls 0.2 cfs)

Primary OutFlow Max=3.4 cfs @ 12.14 hrs HW=118.13' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 3.0 cfs @ 1.30 fps) 2=Broad-Crested Rectangular Weir (Weir Controls 0.4 cfs @ 0.48 fps)

Summary for Pond 5P: Infiltration Basin

Inflow Area =	95,556 sf, 32.02% Impervious	, Inflow Depth = 3.33" for 25 Year event
Inflow =	8.6 cfs @ 12.09 hrs, Volume	= 26,523 cf
Outflow =	2.4 cfs @ 12.46 hrs, Volume	= 26,523 cf, Atten= 72%, Lag= 22.3 min
Discarded =	0.5 cfs @ 12.46 hrs, Volume	= 21,754 cf
Primary =	1.9 cfs @ 12.46 hrs, Volume	= 4,768 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

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Peak Elev= 122.93' @ 12.46 hrs Surf.Area= 9,127 sf Storage= 10,008 cf

Plug-Flow detention time= 159.7 min calculated for 26,523 cf (100% of inflow) Center-of-Mass det. time= 159.7 min (988.7 - 829.0)

Volume	Inve	ert Avail.Sto	rage Storage	Description	
#1	121.5	0' 20,8	63 cf Custon	n Stage Data (P	rismatic)Listed below (Recalc)
Elevatio		Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
121.5	50	2,680	0	0	
121.7	75	4,316	875	875	
122.0	00	7,408	1,466	2,340	
124.0	00	11,115	18,523	20,863	
Device	Routing	Invert	Outlet Device	S	
#1	Primary	122.75'		0.20 0.40 0.60	oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00
				n) 2.54 2.61 2.	61 2.60 2.66 2.70 2.77 2.89 2.88
#2	Discarde	d 121.50'	2.410 in/hr E	xfiltration over	Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.5 cfs @ 12.46 hrs HW=122.93' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.5 cfs)

Summary for Pond 6P: Recharge Trench

Inflow Area =	27,221 sf,100.00% Impervious,	Inflow Depth = 6.05" for 25 Year event
Inflow =	3.9 cfs @ 12.08 hrs, Volume=	13,727 cf
Outflow =	3.9 cfs @ 12.09 hrs, Volume=	13,727 cf, Atten= 0%, Lag= 0.1 min
Discarded =	0.0 cfs @ 5.51 hrs, Volume=	3,635 cf
Primary =	2.6 cfs @ 12.08 hrs, Volume=	9,609 cf
Secondary =	1.2 cfs @ 12.09 hrs, Volume=	483 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 120.52' @ 12.09 hrs Surf.Area= 720 sf Storage= 490 cf

Plug-Flow detention time= 38.8 min calculated for 13,724 cf (100% of inflow) Center-of-Mass det. time= 38.9 min (783.3 - 744.5)

Volume	Invert	Avail.Storage	Storage Description
#1	115.50'	392 cf	Custom Stage Data (Prismatic)Listed below (Recalc)
			1,080 cf Overall - 101 cf Embedded = 979 cf x 40.0% Voids
#2	116.17'	94 cf	6.0" Round Pipe Storage Inside #1
			L= 480.0'
			101 cf Overall - 0.1" Wall Thickness = 94 cf
#3	117.00'	12 cf	0.50'D x 10.00'H Vertical Cone/Cylinder x 6 -Impervious
		498 cf	Total Available Storage

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Elevation	Surf.Area	Inc.Store	Cum.Store	
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)	
115.50	720	0	0	
117.00	720	1,080	1,080	
Device Routing	Invert	Outlet Devices		

#1	Discarded	115.50'	2.410 in/hr Exfiltration over Sur	face area	Phase-In= 0.01'
#2	Primary	118.00'	4.0" Horiz. Orifice/Grate X 4.00	C= 0.600	
			Limited to weir flow at low heads		
#3	Secondary	120.00'	4.0" Horiz. Orifice/Grate X 4.00	C= 0.600	
			Limited to weir flow at low heads		

Discarded OutFlow Max=0.0 cfs @ 5.51 hrs HW=115.62' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=2.6 cfs @ 12.08 hrs HW=120.51' TW=118.11' (Dynamic Tailwater) **2=Orifice/Grate** (Orifice Controls 2.6 cfs @ 7.45 fps)

Secondary OutFlow Max=1.2 cfs @ 12.09 hrs HW=120.51' TW=0.00' (Dynamic Tailwater) -3=Orifice/Grate (Orifice Controls 1.2 cfs @ 3.44 fps)

Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

SubcatchmentPS1:	Runoff Area=343,774 sf 1.74% Impervious Runoff Depth=2.51" Flow Length=197' Tc=22.5 min CN=58 Runoff=14.3 cfs 71,956 cf
SubcatchmentPS10:	Runoff Area=78,810 sf 59.90% Impervious Runoff Depth=5.17" Tc=6.0 min CN=83 Runoff=10.7 cfs 33,951 cf
SubcatchmentPS11:	Runoff Area=72,767 sf 37.18% Impervious Runoff Depth=4.72" Tc=6.0 min CN=79 Runoff=9.2 cfs 28,633 cf
Subcatchment PS12:	Runoff Area=45,344 sf 3.81% Impervious Runoff Depth=2.91" Tc=6.0 min CN=62 Runoff=3.5 cfs 11,003 cf
SubcatchmentPS13:	Runoff Area=25,606 sf 30.26% Impervious Runoff Depth=3.96" Tc=6.0 min CN=72 Runoff=2.7 cfs 8,444 cf
SubcatchmentPS14:	Runoff Area=22,124 sf 10.42% Impervious Runoff Depth=3.01" Tc=6.0 min UI Adjusted CN=63 Runoff=1.8 cfs 5,556 cf
SubcatchmentPS15:	Runoff Area=21,777 sf 100.00% Impervious Runoff Depth=6.91" Tc=6.0 min CN=98 Runoff=3.5 cfs 12,541 cf
SubcatchmentPS16:	Runoff Area=21,777 sf 100.00% Impervious Runoff Depth=6.91" Tc=6.0 min CN=98 Runoff=3.5 cfs 12,541 cf
SubcatchmentPS17:	Runoff Area=27,221 sf 100.00% Impervious Runoff Depth=6.91" Tc=6.0 min CN=98 Runoff=4.4 cfs 15,677 cf
SubcatchmentPS2:	Runoff Area=119,197 sf 5.18% Impervious Runoff Depth=2.61" Flow Length=520' Tc=13.7 min UI Adjusted CN=59 Runoff=6.3 cfs 25,932 cf
SubcatchmentPS2A:	Runoff Area=52,258 sf 2.20% Impervious Runoff Depth=2.41" Flow Length=180' Tc=11.2 min UI Adjusted CN=57 Runoff=2.7 cfs 10,511 cf
SubcatchmentPS3:	Runoff Area=97,067 sf 3.56% Impervious Runoff Depth=2.51" Flow Length=785' Tc=16.3 min UI Adjusted CN=58 Runoff=4.6 cfs 20,317 cf
SubcatchmentPS3A:	Runoff Area=67,954 sf 3.39% Impervious Runoff Depth=2.41" Flow Length=130' Tc=22.0 min UI Adjusted CN=57 Runoff=2.7 cfs 13,668 cf
SubcatchmentPS4:	Runoff Area=171,976 sf 9.20% Impervious Runoff Depth=2.81" Flow Length=100' Tc=7.6 min UI Adjusted CN=61 Runoff=12.0 cfs 40,281 cf
SubcatchmentPS5:	Runoff Area=73,892 sf 3.12% Impervious Runoff Depth=2.51" Flow Length=230' Tc=19.4 min CN=58 Runoff=3.3 cfs 15,466 cf
SubcatchmentPS5A:	Runoff Area=95,000 sf 1.21% Impervious Runoff Depth=2.32" Flow Length=150' Tc=18.9 min UI Adjusted CN=56 Runoff=3.8 cfs 18,337 cf

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SubcatchmentPS6:	Runoff Area=168,938 sf 15.67% Impervious Runoff Depth=3.01" Flow Length=220' Tc=9.2 min UI Adjusted CN=63 Runoff=12.1 cfs 42,425 cf
SubcatchmentPS7:	Runoff Area=95,556 sf 32.02% Impervious Runoff Depth=4.06" Tc=6.0 min CN=73 Runoff=10.5 cfs 32,369 cf
Subcatchment PS8:	Runoff Area=39,073 sf 71.28% Impervious Runoff Depth=5.62" Tc=6.0 min CN=87 Runoff=5.7 cfs 18,314 cf
Subcatchment PS9:	Runoff Area=149,876 sf 53.46% Impervious Runoff Depth=4.94" Tc=6.0 min CN=81 Runoff=19.7 cfs 61,758 cf
Reach DP1:	Inflow=14.3 cfs 71,956 cf Outflow=14.3 cfs 71,956 cf
Reach DP2:	Inflow=14.5 cfs 87,507 cf Outflow=14.5 cfs 87,507 cf
Reach DP2A:	Inflow=6.4 cfs 16,741 cf Outflow=6.4 cfs 16,741 cf
Reach DP3:	Inflow=10.3 cfs 42,581 cf Outflow=10.3 cfs 42,581 cf
Reach DP3A:	Inflow=6.9 cfs 22,264 cf Outflow=6.9 cfs 22,264 cf
Reach DP4:	Inflow=12.2 cfs 95,857 cf Outflow=12.2 cfs 95,857 cf
Reach DP5:	Inflow=18.8 cfs 85,175 cf Outflow=18.8 cfs 85,175 cf
Reach DP5A:	Inflow=7.3 cfs 27,283 cf Outflow=7.3 cfs 27,283 cf
Pond 1P: Detention Basin	Peak Elev=109.00' Storage=19,845 cf Inflow=14.2 cfs 44,953 cf Outflow=2.7 cfs 44,834 cf
Pond 2P: Infiltration Basin	Peak Elev=109.67' Storage=7,536 cf Inflow=6.2 cfs 20,985 cf Discarded=0.2 cfs 14,394 cf Primary=3.7 cfs 6,230 cf Outflow=3.9 cfs 20,624 cf
Pond 3P: Infiltration Basin	Peak Elev=109.24' Storage=66,868 cf Inflow=38.0 cfs 121,246 cf Discarded=0.5 cfs 38,017 cf Primary=3.8 cfs 55,576 cf Outflow=4.3 cfs 93,594 cf
Pond 4P: Infiltration Basin	Peak Elev=118.15' Storage=3,385 cf Inflow=4.5 cfs 16,790 cf Discarded=0.2 cfs 8,928 cf Primary=4.1 cfs 7,861 cf Outflow=4.3 cfs 16,790 cf
Pond 5P: Infiltration Basin	Peak Elev=123.02' Storage=10,855 cf Inflow=10.5 cfs 32,369 cf Discarded=0.5 cfs 23,422 cf Primary=3.6 cfs 8,946 cf Outflow=4.1 cfs 32,369 cf
Pond 6P: Recharge Trench Discarded=0.0 cfs 3,708 c	Peak Elev=120.87' Storage=491 cf Inflow=4.4 cfs 15,677 cf f Primary=2.8 cfs 11,234 cf Secondary=1.6 cfs 735 cf Outflow=4.4 cfs 15,677 cf

Total Runoff Area = 1,789,987 sf Runoff Volume = 499,678 cf Average Runoff Depth = 3.35" 79.88% Pervious = 1,429,771 sf 20.12% Impervious = 360,216 sf

Summary for Subcatchment PS1:

Runoff = 14.3 cfs @ 12.33 hrs, Volume= 71,956 cf, Depth= 2.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

A	rea (sf)	CN [Description						
2	02,359	55 V	55 Woods, Good, HSG B						
1	35,428	61 >	75% Gras	s cover, Go	bod, HSG B				
	3,265	98 l	Jnconnecte	ed pavemer	nt, HSG B				
	2,722	98 l	Inconnecte	ed roofs, HS	SG B				
3	43,774	58 V	Veighted A	verage					
3	37,787	ç	98.26% Per	vious Area					
	5,987	1	.74% Impe	ervious Area	а				
	5,987	1	00.00% Uı	nconnected	1				
Тс	Length	Slope		Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)					
21.8	50	0.0200	0.04		Sheet Flow,				
					Woods: Dense underbrush n= 0.800 P2= 3.10"				
0.7	147	0.0480	3.53		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
22.5	197	Total							

Summary for Subcatchment PS10:

Runoff = 10.7 cfs @ 12.09 hrs, Volume= 33,951 cf, Depth= 5.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

rea (sf)	CN Description										
43,871	98	98 Paved roads w/curbs & sewers, HSG B									
31,599	61 :	>75% Gras	s cover, Go	bod, HSG B							
3,340	98	Unconnecte	ed pavemer	nt, HSG B							
78,810	83	Weighted A	verage								
31,599	4	40.10% Pervious Area									
47,211	!	59.90% Imp	ervious Ar	ea							
3,340	-	7.07% Unco	onnected								
			- ··								
•				Description							
(feet)	(ft/ft)	(ft/sec)	(cfs)								
				Direct Entry,							
	43,871 31,599 3,340 78,810 31,599 47,211 3,340 Length	43,871 98 31,599 61 3,340 98 78,810 83 31,599 4 47,211 4 3,340 5 Length Slope	43,871 98 Paved road 31,599 61 >75% Grass 3,340 98 Unconnected 78,810 83 Weighted A 31,599 40.10% Per 47,211 59.90% Imp 3,340 7.07% Unco Length Slope Velocity	43,87198Paved roads w/curbs a31,59961>75% Grass cover, Grass cove							

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Summary for Subcatchment PS11:

Runoff = 9.2 cfs @ 12.09 hrs, Volume= 28,633 cf, Depth= 4.72"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

A	rea (sf)	CN Description							
	13,154	55	Woods, Go	od, HSG B	3				
	21,827	61	>75% Gras	s cover, Go	Good, HSG B				
	10,719	98	Paved road	s w/curbs &	& sewers, HSG B				
	16,333	98	Roofs, HSG	БB					
	10,734	96	Gravel surfa	ace, HSG E	В				
	72,767	79	79 Weighted Average						
	45,715		62.82% Per	vious Area	а				
	27,052		37.18% Imp	ervious Ar	rea				
_		~		•	–				
Тс	Length	Slope	,	Capacity	•				
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)					
6.0					Direct Entry,				

Summary for Subcatchment PS12:

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

Area (sf)	CN	CN Description							
43,615	61	>75% Gras	s cover, Go	ood, HSG B					
1,729	98	Unconnecte	ed pavemer	nt, HSG B					
45,344	62	Weighted A	verage						
43,615		96.19% Pervious Area							
1,729		3.81% Impervious Area							
1,729		100.00% Unconnected							
Tc Length	Slop	be Velocity	Capacity	Description					
(min) (feet)	(ft/		(cfs)	Decemption					
6.0	•			Direct Entry,					

Summary for Subcatchment PS13:

Runoff = 2.7 cfs @ 12.09 hrs, Volume= 8,444 cf, Depth= 3.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

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Type III 24-hr 50 Year Rainfall=7.15" Printed 11/19/2020 HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLC Page 67

Area	a (sf)	CN	Description							
17	7,857	61	>75% Grass	s cover, Go	od, HSG B					
5	5,444	98	Roofs, HSG	В						
2	2,305	98	Unconnecte	d pavemer	nt, HSG B					
25	5,606	72	Weighted A	verage						
17	7,857	(69.74% Pervious Area							
7	7,749	:	30.26% Impervious Area							
2	2,305	:	29.75% Unconnected							
Tc L		Slope		Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						

6.0

Direct Entry,

Summary for Subcatchment PS14:

Runoff = 1.8 cfs @ 12.09 hrs, Volume= 5,556 cf,	Depth= 3.01"
---	--------------

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

_	Area	(sf)	CN Adj Description						
-	19,	819	61		>75% Grass co	ver, Good, HSG B			
	2,	305	98		Unconnected pa	avement, HSG B			
	22,	124	65	65 63 Weighted Average, UI Adjusted					
	19,	819	89.58% Pervious Área						
	2,	305		10.42% Impervious Area					
	2,	305	100.00% Unconnected						
	Tc Le	ength	Slope		ocity Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/	sec) (cfs)				
	~ ~								

6.0

Direct Entry,

Summary for Subcatchment PS15:

Runoff = 3.5 cfs @ 12.08 hrs, Volume= 12,541 cf, Depth= 6.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

A	rea (sf)	CN	Description						
	21,777	98	Roofs, HSG B						
	21,777		100.00% Im	npervious A	Area				
	Length				Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	Disc of Factors				
6.0					Direct Entry,				

Summary for Subcatchment PS16:

Runoff = 3.5 cfs @ 12.08 hrs, Volume= 12,541 cf, Depth= 6.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

Area (sf) CN Description							
21,777 98 Roofs, HSG							
	npervious Area						
Tc Length Slope Velocity (min) (feet) (ft/ft) (ft/sec)	Capacity Description (cfs)						
6.0	Direct Entry,						
Sum	mary for Subcatchment PS17:						
Runoff = 4.4 cfs @ 12.0	08 hrs, Volume= 15,677 cf, Depth= 6.91"						
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"							
Area (sf) CN Description							
27,221 98 Roofs, HSC	B						
27,221 100.00% In	npervious Area						
Tc Length Slope Velocity (min) (feet) (ft/ft) (ft/sec)	Capacity Description (cfs)						
6.0	Direct Entry,						

Summary for Subcatchment PS2:

Runoff = 6.3 cfs @ 12.20 hrs, Volume= 25,932 cf, Depth= 2.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

Area (sf)	CN	Adj	Description
61,041	55		Woods, Good, HSG B
51,977	61		>75% Grass cover, Good, HSG B
3,457	98		Unconnected pavement, HSG B
2,722	98		Unconnected roofs, HSG B
119,197	60	59	Weighted Average, UI Adjusted
113,018			94.82% Pervious Area
6,179			5.18% Impervious Area
6,179			100.00% Unconnected

Willow Road Proposed ConditionsType III 24-hr50 Year Rainfall=7.15"Prepared by The Morin-Cameron Group, Inc.Printed 11/19/2020HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLCPage 69								
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
11.5	50	0.1000	0.07		Sheet Flow,			
2.2	470	0.0500	3.60		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
13.7	520	Total						
Summary for Subcatchment PS2A:								
Runoff	=	2.7 c	fs @ 12.1	l6 hrs, Vol	ume= 10,511 cf, Depth= 2.41"			
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"								
A	<u>rea (sf)</u>			cription	100 P			
	35,762 15,344	55 61		Woods, Good, HSG B >75% Grass cover, Good, HSG B				
	1,152	98			avement, HSG B			
	52,258 51,106 1,152 1,152		57 Weig 97.8 2.20		age, UI Adjusted is Area us Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
10.7	50	0.1200	0.08		Sheet Flow,			
0.5	130	0.0850	4.69		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
11.2	180	Total						
			Sun	nmary foi	r Subcatchment PS3:			

Runoff = 4.6 cfs @ 12.23 hrs, Volume= 20,317 cf, Depth= 2.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

Area (sf)	CN	Adj	Description
50,666	55		Woods, Good, HSG B
42,944	61		>75% Grass cover, Good, HSG B
3,457	98		Unconnected pavement, HSG B
97,067	59	58	Weighted Average, UI Adjusted
93,610			96.44% Pervious Area
3,457			3.56% Impervious Area
3,457			100.00% Unconnected

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.5	50	0.1000	0.07		Sheet Flow,
4.8	735	0.0250	2.55		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
16.3	785	Total			
10.5	700	Total			
			Sum	mary for	Subcatchment PS3A:
Runoff	=	2.7 c	fs @ 12.3	3 hrs, Vol	ume= 13,668 cf, Depth= 2.41"
			nod, UH=S nfall=7.15"		ted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs
A	rea (sf)	CN A	Adj Desc	ription	
	53,432	55	Woo	ds, Good, H	HSG B
	12,217	61	>75%	6 Grass co	ver, Good, HSG B
	2,305	98	Unco	onnected pa	avement, HSG B
	67,954	58	57 Weig	hted Avera	age, UI Adjusted
	65,649			1% Perviou	
	2,305			% Impervio	
	2,305		100.0	00% Uncor	nected
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	· · F · ·
21.8	50	0.0200	0.04		Sheet Flow,
		0.0200			Woods: Dense underbrush n= 0.800 P2= 3.10"
0.2	80	0.1250	5.69		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
22.0	130	Total			
			Sun	nmary for	r Subcatchment PS4:

Summary for Subcatchment PS4:

Runoff = 12.0 cfs @ 12.11 hrs, Volume= 40,281 cf, Depth= 2.81"

CN	Adj	Description
55		Woods, Good, HSG B
61		>75% Grass cover, Good, HSG B
98		Unconnected pavement, HSG B
98		Unconnected roofs, HSG B
63	61	Weighted Average, UI Adjusted
		90.80% Pervious Area
		9.20% Impervious Area
		100.00% Unconnected
	55 61 98 98	55 61 98 98

 Type III 24-hr
 50 Year Rainfall=7.15"

 Printed
 11/19/2020

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 Page 71

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	Тс	Length	Slope	Velocity		Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	7.5	50	0.0100	0.11		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.10"
	0.1	50	0.2400	7.89		Shallow Concentrated Flow,
_						Unpaved Kv= 16.1 fps
	7.6	100	Total			

Summary for Subcatchment PS5:

Runoff = 3.3 cfs @ 12.29 hrs, Volume= 15,466 cf, Depth= 2.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"

A	rea (sf)	CN E	Description			
	48,067	55 V	Voods, Go	od, HSG B		
	23,521	61 >	75% Gras	s cover, Go	bod, HSG B	
	2,304	98 L	Inconnecte	ed pavemer	nt, HSG B	
	73,892	58 V	Veighted A	verage		
	71,588	g	6.88% Per	vious Area		
	2,304	3	.12% Impe	ervious Are	а	
	2,304	1	100.00% Unconnected			
Тс	Length	Slope	Velocity	Capacity	Description	
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)		
18.6	50	0.0300	0.04		Sheet Flow,	
					Woods: Dense underbrush n= 0.800 P2= 3.10"	
0.8	180	0.0500	3.60		Shallow Concentrated Flow,	
					Unpaved Kv= 16.1 fps	
19.4	230	Total				

Summary for Subcatchment PS5A:

Runoff = 3.8 cfs @ 12.28 hrs, Volume= 18,337 cf, Depth= 2.32"

Area (sf)	CN	Adj	Description
77,272	55		Woods, Good, HSG B
16,576	61		>75% Grass cover, Good, HSG B
1,152	98		Unconnected pavement, HSG B
95,000	57	56	Weighted Average, UI Adjusted
93,848			98.79% Pervious Area
1,152			1.21% Impervious Area
1,152			100.00% Unconnected

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HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLCPaTc LengthSlopeVelocityCapacityDescription(min)(feet)(ft/ft)(ft/sec)(cfs)					· · · · ·	
18.6 0.3	50 100	0.0300 0.1000	0.04 5.09	Woods: Dense underbrush n= 0.800 P2= 3.10"		
18.9	150	Total				
	Summary for Subcatchment PS6:					
Runoff	=	12.1 ct	fs @ 12.1	13 hrs, Volu	ume= 42,425 cf, Depth= 3.01"	
	Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"					
A	rea (sf)	CN A	Adj Desc	cription		
	67,828	55		ds, Good, H		
74,644 61 >75% Grass cover, Good, HSG B						
	11,625 98 Unconnected pavement, HSG B 13,498 98 Roofs, HSG B					

A	rea (sf)	CN A	Adj Desc	ription				
	67,828	55	Woo	Woods, Good, HSG B				
	74,644	61	>75%	6 Grass co	ver, Good, HSG B			
	11,625	98	Unco	onnected pa	avement, HSG B			
	13,498	98	Roof	s, HSG B				
	1,343	98	Pave	d roads w/	curbs & sewers, HSG B			
1	68,938	64	63 Weig	hted Avera	age, UI Adjusted			
1	142,472 84.33% Pervious Área							
	26,466		15.67	7% Impervi	ous Area			
	11,625		43.92	43.92% Unconnected				
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
8.7	50	0.0500	0.10		Sheet Flow,			
				Woods: Light underbrush n= 0.400 P2= 3.10"				
0.5	170	0.1120	5.39	,				
				Unpaved Kv= 16.1 fps				
9.2	220	Total						

Summary for Subcatchment PS7:

Runoff = 10.5 cfs @ 12.09 hrs, Volume= 32,369 cf, Depth= 4.06"

Area (sf)	CN	Description			
64,959	61	>75% Grass cover, Good, HSG B			
10,888	98	Roofs, HSG B			
7,062	98	Unconnected pavement, HSG B			
12,647	98	Paved roads w/curbs & sewers, HSG B			
95,556	73	Weighted Average			
64,959		67.98% Pervious Area			
30,597		32.02% Impervious Area			
7,062		23.08% Unconnected			

Willow Road Proposed ConditionsType III 24-hr50 Year Rainfall=7.15"Prepared by The Morin-Cameron Group, Inc.Printed 11/19/2020HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLCPage 73						
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)						
6.0 Direct Entry,						
Summary for Subcatchment PS8:						
Runoff = 5.7 cfs @ 12.08 hrs, Volume= 18,314 cf, Depth= 5.62"						
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"						
Area (sf) CN Description						
25,064 98 Paved roads w/curbs & sewers, HSG B						
2,787 98 Unconnected pavement, HSG B						
<u>11,222 61 >75% Grass cover, Good, HSG B</u> 39,073 87 Weighted Average						
11,222 28.72% Pervious Area						
27,851 71.28% Impervious Area						
2,787 10.01% Unconnected						
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)						
6.0 Direct Entry,						
Summary for Subcatchment PS9:						
Runoff = 19.7 cfs @ 12.09 hrs, Volume= 61,758 cf, Depth= 4.94"						
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 50 Year Rainfall=7.15"						

Area (sf)	CN	Description					
22,164	98	Paved roads w/curbs & sewers, HSG B					
69,747	61	>75% Grass cover, Good, HSG B					
3,523	98	Unconnected pavement, HSG B					
54,442	98	Roofs, HSG B					
149,876	81	Weighted Average					
69,747		46.54% Pervious Area					
80,129		53.46% Impervious Area					
3,523		4.40% Unconnected					
Tc Length	Slop	pe Velocity Capacity Description					
(min) (feet)		/ft) (ft/sec) (cfs)					
6.0		Direct Entry,					

Summary for Reach DP1:

Inflow Area =	343,774 sf,	1.74% Impervious,	Inflow Depth = 2.51"	for 50 Year event
Inflow =	14.3 cfs @	12.33 hrs, Volume=	71,956 cf	
Outflow =	14.3 cfs @	12.33 hrs, Volume=	71,956 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2:

Inflow Area =	342,992 sf,	25.01% Impervious,	Inflow Depth > 3.0	6" for 50 Year event
Inflow =	14.5 cfs @	12.19 hrs, Volume=	87,507 cf	
Outflow =	14.5 cfs @	12.19 hrs, Volume=	87,507 cf, A	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2A:

Inflow Area =	99,641 sf,	30.79% Impervious,	Inflow Depth = 2.02"	for 50 Year event
Inflow =	6.4 cfs @	12.18 hrs, Volume=	16,741 cf	
Outflow =	6.4 cfs @	12.18 hrs, Volume=	16,741 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3:

Inflow Area	a =	214,366 sf,	16.46% Impervious,	Inflow Depth = 2.38"	for 50 Year event
Inflow	=	10.3 cfs @	12.15 hrs, Volume=	42,581 cf	
Outflow	=	10.3 cfs @	12.15 hrs, Volume=	42,581 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3A:

Inflow Area	a =	117,299 sf,	27.14% Impervious,	Inflow Depth = 2.28"	for 50 Year event
Inflow	=	6.9 cfs @	12.11 hrs, Volume=	22,264 cf	
Outflow	=	6.9 cfs @	12.11 hrs, Volume=	22,264 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP4:

Inflow Area =	455,469 sf,	37.90% Impervious,	Inflow Depth = 2.53"	for 50 Year event
Inflow =	12.2 cfs @	12.12 hrs, Volume=	95,857 cf	
Outflow =	12.2 cfs @	12.12 hrs, Volume=	95,857 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5:

Inflow Area =	433,386 sf,	13.96% Impervious,	Inflow Depth = 2.36"	for 50 Year event
Inflow =	18.8 cfs @	12.20 hrs, Volume=	85,175 cf	
Outflow =	18.8 cfs @	12.20 hrs, Volume=	85,175 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5A:

Inflow Area	a =	190,556 sf,	16.66% Impervious,	Inflow Depth = 1.72"	for 50 Year event
Inflow	=	7.3 cfs @	12.31 hrs, Volume=	27,283 cf	
Outflow	=	7.3 cfs @	12.31 hrs, Volume=	27,283 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Pond 1P: Detention Basin

Inflow Area =	124,154 sf, 39.42% Impervious,	Inflow Depth = 4.34" for 50 Year event
Inflow =	14.2 cfs @ 12.09 hrs, Volume=	44,953 cf
Outflow =	2.7 cfs @ 12.54 hrs, Volume=	44,834 cf, Atten= 81%, Lag= 27.4 min
Primary =	2.7 cfs @ 12.54 hrs, Volume=	44,834 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 109.00' @ 12.54 hrs Surf.Area= 6,712 sf Storage= 19,845 cf

Plug-Flow detention time= 172.2 min calculated for 44,834 cf (100% of inflow) Center-of-Mass det. time= 170.6 min (982.0 - 811.4)

Volume	Invert	Avail.Sto	rage Storag	age Storage Description		
#1	105.00'	26,98	B7 cf Custo	m Stage Data (Pris	smatic)Listed below (Recalc)	
_	-	<i>.</i> .		a a /		
Elevatio	on Su	ırf.Area	Inc.Store	Cum.Store		
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)		
105.0	00	2,562	0	0		
106.0	00	4,302	3,432	3,432		
108.0)0	5,832	10,134	13,566		
110.0	00	7,589	13,421	26,987		
Device	Routing	Invert	Outlet Devic	es		
#1	Primary	98.00'	12.0" Roun	d Culvert L= 40.0	' Ke= 0.500	
			Inlet / Outlet	Invert= 98.00' / 96.	.00' S= 0.0500 '/' Cc= 0.900	
			n= 0.012, F	low Area= 0.79 sf		
#2	Device 1	105.00'	3.0" Vert. O	rifice/Grate C= 0.	.600 Limited to weir flow at low heads	
#3	Device 1	106.00'	4.0" Vert. O	rifice/Grate C= 0.	.600 Limited to weir flow at low heads	
#4	Device 1	107.60'		0" H Vert. Orifice/		
			Limited to w	eir flow at low head	s	
#5	Device 1	108.90'	4.0' long x	0.5' breadth Broad	d-Crested Rectangular Weir	
				0.20 0.40 0.60 0.		
				sh) 2.80 2.92 3.08		
			, u			

Primary OutFlow Max=2.7 cfs @ 12.54 hrs HW=109.00' TW=0.00' (Dynamic Tailwater)

2=Orifice/Grate (Orifice Controls 0.5 cfs @ 9.48 fps)

-3=Orifice/Grate (Orifice Controls 0.7 cfs @ 8.11 fps)

-4=Orifice/Grate (Orifice Controls 1.1 cfs @ 5.44 fps)

-5=Broad-Crested Rectangular Weir (Weir Controls 0.4 cfs @ 0.89 fps)

Summary for Pond 2P: Infiltration Basin

Inflow Area =	47,383 sf, 62.31% Impervious, Inflow Depth = 5.31" for 50 Year event
Inflow =	6.2 cfs @ 12.09 hrs, Volume= 20,985 cf
Outflow =	3.9 cfs @ 12.18 hrs, Volume= 20,624 cf, Atten= 37%, Lag= 5.9 min
Discarded =	0.2 cfs @ 12.18 hrs, Volume= 14,394 cf
Primary =	3.7 cfs @ 12.18 hrs, Volume= 6,230 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 109.67' @ 12.18 hrs Surf.Area= 3,693 sf Storage= 7,536 cf

Plug-Flow detention time= 298.0 min calculated for 20,618 cf (98% of inflow) Center-of-Mass det. time= 287.2 min (1,063.1 - 776.0)

Volume	Inver	t Avail.Sto	rage Storage	Description		
#1	106.00)' 8,7	99 cf Custom	Stage Data (Coni	c) Listed below (Re	ecalc)
Elevatio (fee 106.0	et) 00	Surf.Area (sq-ft) 781	Inc.Store (cubic-feet) 0	Cum.Store (cubic-feet) 0	Wet.Area <u>(sq-ft)</u> 781	
108.0 110.0		2,086 4,059	2,762 6,037	2,762 8,799	2,112 4,123	
Device	Routing	Invert	Outlet Devices	,	.,	
#1	Primary	109.50'		2.0' breadth Broad 20 0.40 0.60 0.8 0		
#2	Discarded	106.00'	2.85 3.07 3.2) 2.54 2.61 2.61 0 3.32 filtration over Su		

Discarded OutFlow Max=0.2 cfs @ 12.18 hrs HW=109.67' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.2 cfs)

Primary OutFlow Max=3.7 cfs @ 12.18 hrs HW=109.67' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Weir Controls 3.7 cfs @ 1.06 fps)

Summary for Pond 3P: Infiltration Basin

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Inflow Are Inflow Outflow Discardeo Primary	= =	38.0 cfs @ 1 4.3 cfs @ 1 0.5 cfs @ 1	5.31% Impervio 2.09 hrs, Volum 2.79 hrs, Volum 2.79 hrs, Volum 2.79 hrs, Volum	ne= 121 ne= 93 ne= 38	oth = 5.13" for 5 ,246 cf ,594 cf, Atten= 89% ,017 cf ,576 cf	
			Гime Span= 0.00 Surf.Area= 20,5			
Center-of	-Mass det.	time= 324.9 n	nin calculated for nin (1,121.9 - 79	97.0)	% of inflow)	
Volume	Invert		rage Storage [<u> </u>
#1	104.00'	83,59	98 cf Custom	Stage Data (C	onic)Listed below (Recalc)
Elevatior (feet		urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
104.00	C	8,168	0	0	8,168	
105.00	C	9,203	8,680	8,680	9,254	
106.00	C	10,294	9,743	18,424	10,400	
108.00	C	15,794	25,893	44,316	15,959	
110.00	C	23,758	39,282	83,598	23,984	
Device	Deutine	lavant				
	Routing	Invert	Outlet Devices			
#1	Primary	106.50'			.0' Ke= 0.600	
					106.00' S= 0.014	
#2	Device 1	107.00'			shed, Flow Area= 0	veir flow at low heads
	Device 1 Device 1	107.00				veir flow at low heads
	Device 1 Device 1	108.00	24.0" Horiz. O			ven now at low neads
#4	Device I	109.00	Limited to weir			
#5	Primary	109.50'			oad-Crested Recta	angular Weir
10	Timary	100.00	Head (feet) 0.2 2.50 3.00 3.50 Coef. (English)	20 0.40 0.60 0 4.00 4.50 5 0 2.38 2.54 2	0.80 1.00 1.20 1.	40 1.60 1.80 2.00
#6	Discarded	104.00'			Surface area Pha	ase-In= 0.01'
Discarded OutFlow Max=0.5 cfs @ 12.79 hrs HW=109.24' (Free Discharge) ←6=Exfiltration (Exfiltration Controls 0.5 cfs)						

Primary OutFlow Max=3.8 cfs @ 12.79 hrs HW=109.24' TW=0.00' (Dynamic Tailwater) 1=Culvert (Passes 3.8 cfs of 5.3 cfs potential flow) 2=Orifice/Grate (Orifice Controls 0.3 cfs @ 7.01 fps) 3=Orifice/Grate (Orifice Controls 0.9 cfs @ 4.80 fps) 4=Orifice/Grate (Weir Controls 2.5 cfs @ 1.62 fps) Ferenced Constraint (Controls 0.9 cfs)

-5=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

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Summary for Pond 4P: Infiltration Basin

Inflow Area =	49,345 sf,	59.84% Impervious,	Inflow Depth = 4.08" for 50 Year event
Inflow =	4.5 cfs @	12.09 hrs, Volume=	16,790 cf
Outflow =	4.3 cfs @	12.12 hrs, Volume=	16,790 cf, Atten= 4%, Lag= 1.8 min
Discarded =	0.2 cfs @	12.12 hrs, Volume=	8,928 cf
Primary =	4.1 cfs @	12.12 hrs, Volume=	7,861 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 118.15' @ 12.12 hrs Surf.Area= 4,219 sf Storage= 3,385 cf

Plug-Flow detention time= 74.6 min calculated for 16,785 cf (100% of inflow) Center-of-Mass det. time= 74.5 min (855.5 - 781.0)

Volume	Inve	ert Avail.Sto	rage Storage Description				
#1 117.00' 4,9		51 cf Custor	1 cf Custom Stage Data (Conic)Listed below (Recalc)				
Elevatio	מר	Surf.Area	Inc.Store	Cum.Store	Wet.Area		
(fee		(sq-ft)	(cubic-feet)	(cubic-feet)	(sq-ft)		
117.0	00	1,691	0	0	1,691		
118.0		4,012	2,769	2,769	4,019		
118.8	50	4,726	2,182	4,951	4,743		
Device Routing Invert		Invert	Outlet Device	es			
#1	Primary	117.90'		10.0' long x 1.0' breadth Broad-Crested Rectangular Weir			
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00				
				sh) 2.69 2.72 2.75	285 298 308 3	20 3 28 3 31	
			3.30 3.31 3		2.00 2.00 0.00 0.	20 0.20 0.01	
#2	Primary	118.10'	25.0' long x	1.0' breadth Broad	d-Crested Rectang	ular Weir	
				0.20 0.40 0.60 0.8	30 1.00 1.20 1.40	1.60 1.80 2.00	
			2.50 3.00			~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	
				sh) 2.69 2.72 2.75	2.85 2.98 3.08 3.	20 3.28 3.31	
#3	Discarde	d 117.00'	3.30 3.31 3	.32 Exfiltration over Su	rface area Dhace	$l_{n-1} = 0.01!$	
#3	Discalue	u 117.00	2.410 111/111 6		Tiace area Fliase	-111- 0.01	
<u>.</u>							

Discarded OutFlow Max=0.2 cfs @ 12.12 hrs HW=118.15' (Free Discharge) **-3=Exfiltration** (Exfiltration Controls 0.2 cfs)

Primary OutFlow Max=4.1 cfs @ 12.12 hrs HW=118.15' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 3.4 cfs @ 1.35 fps) 2=Broad-Crested Rectangular Weir (Weir Controls 0.7 cfs @ 0.60 fps)

Summary for Pond 5P: Infiltration Basin

Inflow Area =	95,556 sf, 32.02% Impervious	, Inflow Depth = 4.06" for 50 Year event
Inflow =	10.5 cfs @ 12.09 hrs, Volume=	= 32,369 cf
Outflow =	4.1 cfs @ 12.34 hrs, Volume=	= 32,369 cf, Atten= 61%, Lag= 15.2 min
Discarded =	0.5 cfs @ 12.34 hrs, Volume=	= 23,422 cf
Primary =	3.6 cfs @ 12.34 hrs, Volume=	= 8,946 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

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Peak Elev= 123.02' @ 12.34 hrs Surf.Area= 9,297 sf Storage= 10,855 cf

Plug-Flow detention time= 144.8 min calculated for 32,369 cf (100% of inflow) Center-of-Mass det. time= 144.8 min (968.1 - 823.3)

Volume	Inve	ert Avail.Sto	rage Storage	e Storage Description		
#1 121.50		20,8	63 cf Custor	Custom Stage Data (Prismatic)Listed below (Recalc)		
		Surf.Area	Inc.Store	Cum.Store		
(feet)		(sq-ft)	(cubic-feet)	(cubic-feet)		
121.50		2,680	0	0		
121.75		4,316	875	875		
122.00		7,408	1,466	2,340		
124.00		11,115	18,523	20,863		
Device Routing		Invert	Outlet Devic	es		
#1 Primary 122.75		10.0' long x 2.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50				
#2 Discarded 121.50'		Coef. (Englis 2.85 3.07 3	sh) 2.54 2.61 2. .20 3.32	61 2.60 2.66 2.70 2.77 2.89 2.88 Surface area Phase-In= 0.01'		

Discarded OutFlow Max=0.5 cfs @ 12.34 hrs HW=123.02' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.5 cfs)

Primary OutFlow Max=3.6 cfs @ 12.34 hrs HW=123.02' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Weir Controls 3.6 cfs @ 1.33 fps)

Summary for Pond 6P: Recharge Trench

Inflow Area =	27,221 sf,100.00% Impervious,	Inflow Depth = 6.91" for 50 Year event
Inflow =	4.4 cfs @ 12.08 hrs, Volume=	15,677 cf
Outflow =	4.4 cfs @ 12.08 hrs, Volume=	15,677 cf, Atten= 0%, Lag= 0.1 min
Discarded =	0.0 cfs @ 4.66 hrs, Volume=	3,708 cf
Primary =	2.8 cfs @ 12.08 hrs, Volume=	11,234 cf
Secondary =	1.6 cfs @ 12.08 hrs, Volume=	735 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 120.87' @ 12.08 hrs Surf.Area= 720 sf Storage= 491 cf

Plug-Flow detention time= 35.6 min calculated for 15,677 cf (100% of inflow) Center-of-Mass det. time= 35.6 min (778.3 - 742.7)

Volume	Invert	Avail.Storage	Storage Description	
#1	115.50'	392 cf	Custom Stage Data (Prismatic)Listed below (Recalc)	
			1,080 cf Overall - 101 cf Embedded = 979 cf x 40.0% Voids	
#2	116.17'	94 cf	6.0" Round Pipe Storage Inside #1	
			L= 480.0'	
			101 cf Overall - 0.1" Wall Thickness = 94 cf	
#3	117.00'	12 cf	0.50'D x 10.00'H Vertical Cone/Cylinder x 6 -Impervious	
		498 cf	Total Available Storage	

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	Elevatio (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
115.50 117.00			720 720	0 1,080	0 1,080
	Device	Routing	Invert	Outlet Devices	

Device	Rouling	Inven	Outlet Devices	
#1	Discarded	115.50'	2.410 in/hr Exfiltration over Surface area Pha	ase-In= 0.01'
#2	Primary	118.00'	4.0" Horiz. Orifice/Grate X 4.00 C= 0.600	
			Limited to weir flow at low heads	
#3	Secondary	120.00'	4.0" Horiz. Orifice/Grate X 4.00 C= 0.600	
			Limited to weir flow at low heads	

Discarded OutFlow Max=0.0 cfs @ 4.66 hrs HW=115.62' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=2.8 cfs @ 12.08 hrs HW=120.86' TW=118.14' (Dynamic Tailwater) **2=Orifice/Grate** (Orifice Controls 2.8 cfs @ 7.94 fps)

Secondary OutFlow Max=1.6 cfs @ 12.08 hrs HW=120.86' TW=0.00' (Dynamic Tailwater) -3=Orifice/Grate (Orifice Controls 1.6 cfs @ 4.47 fps) Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

SubcatchmentPS1:	Runoff Area=343,774 sf 1.74% Impervious Runoff Depth=3.18" Flow Length=197' Tc=22.5 min CN=58 Runoff=18.4 cfs 91,235 cf
SubcatchmentPS10:	Runoff Area=78,810 sf 59.90% Impervious Runoff Depth=6.07" Tc=6.0 min CN=83 Runoff=12.5 cfs 39,884 cf
SubcatchmentPS11:	Runoff Area=72,767 sf 37.18% Impervious Runoff Depth=5.60" Tc=6.0 min CN=79 Runoff=10.8 cfs 33,965 cf
Subcatchment PS12:	Runoff Area=45,344 sf 3.81% Impervious Runoff Depth=3.63" Tc=6.0 min CN=62 Runoff=4.4 cfs 13,732 cf
SubcatchmentPS13:	Runoff Area=25,606 sf 30.26% Impervious Runoff Depth=4.78" Tc=6.0 min CN=72 Runoff=3.3 cfs 10,205 cf
SubcatchmentPS14:	Runoff Area=22,124 sf 10.42% Impervious Runoff Depth=3.75" Tc=6.0 min UI Adjusted CN=63 Runoff=2.2 cfs 6,909 cf
SubcatchmentPS15:	Runoff Area=21,777 sf 100.00% Impervious Runoff Depth=7.86" Tc=6.0 min CN=98 Runoff=4.0 cfs 14,264 cf
SubcatchmentPS16:	Runoff Area=21,777 sf 100.00% Impervious Runoff Depth=7.86" Tc=6.0 min CN=98 Runoff=4.0 cfs 14,264 cf
SubcatchmentPS17:	Runoff Area=27,221 sf 100.00% Impervious Runoff Depth=7.86" Tc=6.0 min CN=98 Runoff=5.0 cfs 17,830 cf
SubcatchmentPS2:	Runoff Area=119,197 sf 5.18% Impervious Runoff Depth=3.30" Flow Length=520' Tc=13.7 min UI Adjusted CN=59 Runoff=8.1 cfs 32,743 cf
SubcatchmentPS2A:	Runoff Area=52,258 sf 2.20% Impervious Runoff Depth=3.07" Flow Length=180' Tc=11.2 min UI Adjusted CN=57 Runoff=3.5 cfs 13,385 cf
SubcatchmentPS3:	Runoff Area=97,067 sf 3.56% Impervious Runoff Depth=3.18" Flow Length=785' Tc=16.3 min UI Adjusted CN=58 Runoff=5.9 cfs 25,761 cf
SubcatchmentPS3A:	Runoff Area=67,954 sf 3.39% Impervious Runoff Depth=3.07" Flow Length=130' Tc=22.0 min UI Adjusted CN=57 Runoff=3.5 cfs 17,405 cf
SubcatchmentPS4:	Runoff Area=171,976 sf 9.20% Impervious Runoff Depth=3.52" Flow Length=100' Tc=7.6 min UI Adjusted CN=61 Runoff=15.2 cfs 50,462 cf
SubcatchmentPS5:	Runoff Area=73,892 sf 3.12% Impervious Runoff Depth=3.18" Flow Length=230' Tc=19.4 min CN=58 Runoff=4.2 cfs 19,610 cf
SubcatchmentPS5A:	Runoff Area=95,000 sf 1.21% Impervious Runoff Depth=2.96" Flow Length=150' Tc=18.9 min UI Adjusted CN=56 Runoff=5.0 cfs 23,456 cf

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Subcatchment PS6: Flow Length	Runoff Area=168,938 sf 15.67% Impervious Runoff Depth=3.75" n=220' Tc=9.2 min UI Adjusted CN=63 Runoff=15.2 cfs 52,757 cf
SubcatchmentPS7:	Runoff Area=95,556 sf 32.02% Impervious Runoff Depth=4.90" Tc=6.0 min CN=73 Runoff=12.6 cfs 39,008 cf
SubcatchmentPS8:	Runoff Area=39,073 sf 71.28% Impervious Runoff Depth=6.55" Tc=6.0 min CN=87 Runoff=6.6 cfs 21,318 cf
SubcatchmentPS9:	Runoff Area=149,876 sf 53.46% Impervious Runoff Depth=5.84" Tc=6.0 min CN=81 Runoff=23.1 cfs 72,898 cf
Reach DP1:	Inflow=18.4 cfs 91,235 cf Outflow=18.4 cfs 91,235 cf
Reach DP2:	Inflow=19.1 cfs 108,682 cf Outflow=19.1 cfs 108,682 cf
Reach DP2A:	Inflow=9.4 cfs 22,447 cf Outflow=9.4 cfs 22,447 cf
Reach DP3:	Inflow=12.9 cfs 54,353 cf Outflow=12.9 cfs 54,353 cf
Reach DP3A:	Inflow=8.4 cfs 28,592 cf Outflow=8.4 cfs 28,592 cf
Reach DP4:	Inflow=16.0 cfs 125,817 cf Outflow=16.0 cfs 125,817 cf
Reach DP5:	Inflow=26.9 cfs 109,719 cf Outflow=26.9 cfs 109,719 cf
Reach DP5A:	Inflow=10.8 cfs 37,351 cf Outflow=10.8 cfs 37,351 cf
Pond 1P: Detention Basin	Peak Elev=109.29' Storage=21,824 cf Inflow=16.9 cfs 53,616 cf Outflow=5.3 cfs 53,492 cf
Pond 2P: Infiltration Basin Discarded=0.2	Peak Elev=109.74' Storage=7,780 cf Inflow=7.3 cfs 24,469 cf cfs 14,929 cf Primary=6.0 cfs 9,063 cf Outflow=6.2 cfs 23,992 cf
Pond 3P: Infiltration Basin Discarded=0.5 cfs	Peak Elev=109.60' Storage=74,483 cf Inflow=44.4 cfs 142,445 cf s 39,017 cf Primary=7.3 cfs 75,356 cf Outflow=7.8 cfs 114,373 cf
Pond 4P: Infiltration Basin Discarded=0.2	Peak Elev=118.16' Storage=3,449 cf Inflow=5.2 cfs 19,946 cf cfs 9,794 cf Primary=4.8 cfs 10,152 cf Outflow=5.0 cfs 19,946 cf
Pond 5P: Infiltration Basin Discarded=0.5 c	Peak Elev=123.12' Storage=11,794 cf Inflow=12.6 cfs 39,008 cf fs 25,112 cf Primary=5.8 cfs 13,896 cf Outflow=6.4 cfs 39,008 cf
Pond 6P: Recharge Trench Discarded=0.0 cfs 3,758 cf Primary=3.0 cfs	Peak Elev=121.33' Storage=491 cf Inflow=5.0 cfs 17,830 cf 13,037 cf Secondary=1.9 cfs 1,035 cf Outflow=5.0 cfs 17,830 cf

Total Runoff Area = 1,789,987 sf Runoff Volume = 611,090 cf Average Runoff Depth = 4.10" 79.88% Pervious = 1,429,771 sf 20.12% Impervious = 360,216 sf

Summary for Subcatchment PS1:

Runoff = 18.4 cfs @ 12.33 hrs, Volume= 91,235 cf, Depth= 3.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"

A	rea (sf)	CN E	Description					
2	02,359	55 V	Voods, Good, HSG B					
1	35,428	61 >	75% Grass cover, Good, HSG B					
	3,265	98 L	Jnconnecte	ed pavemer	nt, HSG B			
	2,722	98 L	Inconnecte	ed roofs, HS	SG B			
3	43,774	58 V	Veighted A	verage				
3	37,787	ç	8.26% Per	vious Area				
	5,987	1	1.74% Impervious Area					
	5,987	1	00.00% Ui	nconnected				
Тс	Length	Slope	Velocity	Capacity	Description			
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)				
21.8	50	0.0200	0.04		Sheet Flow,			
					Woods: Dense underbrush n= 0.800 P2= 3.10"			
0.7	147	0.0480	3.53		Shallow Concentrated Flow,			
					Unpaved Kv= 16.1 fps			
22.5	197	Total						

Summary for Subcatchment PS10:

Runoff = 12.5 cfs @ 12.09 hrs, Volume= 39,884 cf, Depth= 6.07"

Α	rea (sf)	CN	Description					
	43,871	98	Paved road	s w/curbs &	& sewers, HSG B			
	31,599	61	>75% Gras	s cover, Go	ood, HSG B			
	3,340	98	Unconnecte	d pavemer	ent, HSG B			
	78,810	83	Weighted A	verage				
	31,599		40.10% Per	vious Area	a			
	47,211		59.90% Impervious Area					
	3,340		7.07% Unconnected					
_		<u>.</u>		•				
Тс	Length	Slope						
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)				
6.0					Direct Entry,			

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Summary for Subcatchment PS11:

Runoff = 10.8 cfs @ 12.09 hrs, Volume= 33,965 cf, Depth= 5.60"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"

A	rea (sf)	CN	Description					
	13,154	55	Woods, Go	od, HSG B				
	21,827	61	>75% Gras	s cover, Go	ood, HSG B			
	10,719	98	Paved road	s w/curbs &	& sewers, HSG B			
	16,333	98	Roofs, HSG	БB				
	10,734	96	Gravel surfa	ace, HSG E	3			
	72,767	79	79 Weighted Average					
	45,715		62.82% Pervious Area					
	27,052		37.18% Impervious Area					
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft) (ft/sec) (cfs)						
6.0			Direct Entry,					

Summary for Subcatchment PS12:

Runoff = 4.4 cfs @ 12.09 hrs, Volume= 13,732 cf	, Depth= 3.63"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"

Area (sf)	CN	Description						
43,615	61	>75% Gras	s cover, Go	ood, HSG B				
1,729	98	Unconnecte	ed pavemer	nt, HSG B				
45,344	62	Weighted A	verage					
43,615		96.19% Pervious Area						
1,729		3.81% Impervious Area						
1,729		100.00% Unconnected						
Tc Length	Slop	be Velocity	Capacity	Description				
(min) (feet)	(ft/		(cfs)	Decemption				
6.0	•			Direct Entry,				

Summary for Subcatchment PS13:

Runoff = 3.3 cfs @ 12.09 hrs, Volume= 10,205 cf, Depth= 4.78"

Type III 24-hr 100 Year Rainfall=8.10" Printed 11/19/2020 Page 86

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Area (sf)	CN	Description							
17,857	61	>75% Grass cover, Good, HSG B							
5,444	98	Roofs, HSG B							
2,305	98	Unconnected pavement, HSG B							
25,606	72	Weighted Average							
17,857		69.74% Pervious Area							
7,749		30.26% Impervious Area							
2,305		29.75% Unconnected							
Tc Length	Slop								
(min) (feet)	(ft/	ft) (ft/sec) (cfs)							

6.0

Direct Entry,

Summary for Subcatchment PS14:

Runoff = 2.2 cfs @ 12.09 hrs, Volume= 6,909 cf, Depth= 3	3.75"
--	-------

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"

A	rea (sf)	CN /	CN Adj Description						
	19,819	61	>75	% Grass co	ver, Good, HSG B				
	2,305	98	Unc	onnected pa	avement, HSG B				
	22,124	65	65 63 Weighted Average, UI Adjusted						
	19,819		89.58% Pervious Area						
	2,305		10.42% Impervious Area						
	2,305		100.00% Unconnected						
_		~		.	_				
Тс	Length	Slope	Velocity	Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)					
6.0					Direct Entry,				

Direct Entry,

Summary for Subcatchment PS15:

Runoff = 4.0 cfs @ 12.08 hrs, Volume= 14,264 cf, Depth= 7.86"

Α	rea (sf)	CN	Description		
	21,777	98	Roofs, HSG	βB	
	21,777		100.00% In	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
6.0					Direct Entry,

Summary for Subcatchment PS16:

Runoff = 4.0 cfs @ 12.08 hrs, Volume= 14,264 cf, Depth= 7.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"

Area (sf) Cl	N Description							
21,777 98 Roofs, HSG B								
21,777 100.00% Impervious Area								
0	Slope Velocity Capacity Description							
	(ft/ft) (ft/sec) (cfs)							
6.0	Direct Entry,							
Summary for Subcatchment PS17:								
Runoff = 5.0 cfs @ 12.08 hrs, Volume= 17,830 cf, Depth= 7.86"								
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"								
Area (sf) Cl	N Description							
27,221 9	08 Roofs, HSG B							
27,221	100.00% Impervious Area							
	Slope Velocity Capacity Description (ft/ft) (ft/sec) (cfs)							
6.0	Direct Entry,							

Summary for Subcatchment PS2:

Runoff = 8.1 cfs @ 12.19 hrs, Volume= 32,743 cf, Depth= 3.30"

Area (sf)	CN	Adj	Description
61,041	55		Woods, Good, HSG B
51,977	61		>75% Grass cover, Good, HSG B
3,457	98		Unconnected pavement, HSG B
2,722	98		Unconnected roofs, HSG B
119,197	60	59	Weighted Average, UI Adjusted
113,018			94.82% Pervious Area
6,179			5.18% Impervious Area
6,179			100.00% Unconnected

Prepare	Willow Road Proposed ConditionsType III 24-hr 100 Year Rainfall=8.10Prepared by The Morin-Cameron Group, Inc.Printed 11/19/2020								
HydroCA	D® 10.10-	<u>3a_s/n 00</u>	401 © 202	0 HydroCAD	O Software Solutions LLC Page 88				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
11.5	50	0.1000	0.07		Sheet Flow,				
2.2	470	0.0500	3.60		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
13.7	520	Total							
Summary for Subcatchment PS2A:									
Runoff	=	3.5 c	fs @ 12.1	6 hrs, Volu	ume= 13,385 cf, Depth= 3.07"				
			nod, UH=S ainfall=8.1(ted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs				
А	rea (sf)	CN A	Adj Desc	ription					
	35,762	55	Woo	ds, Good, H	ISG B				
	15,344	61			ver, Good, HSG B				
	1,152	98			avement, HSG B				
	52,258	58			age, UI Adjusted				
	51,106			0% Perviou					
	1,152 1,152			% Impervio 00% Uncon					
	1,152		100.0		lilected				
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
10.7	50	0.1200	0.08		Sheet Flow,				
0.5	130	0.0850	4.69		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
11.2	180	Total							
			Sun	nmary foi	r Subcatchment PS3:				

Summary for Subcatchment PS3:

Runoff = 5.9 cfs @ 12.23 hrs, Volume= 25,761 cf, Depth= 3.18"

Area (sf)	CN	Adj	Description
50,666	55		Woods, Good, HSG B
42,944	61		>75% Grass cover, Good, HSG B
3,457	98		Unconnected pavement, HSG B
97,067	59	58	Weighted Average, UI Adjusted
93,610			96.44% Pervious Area
3,457			3.56% Impervious Area
3,457			100.00% Unconnected

Prepare	d by The	Morin-C		Group, Inc	<i>Type III 24-hr 100 Year Rainfall=8.10"</i> Printed 11/19/2020 Software Solutions LLC Page 89				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
11.5	50	0.1000	0.07		Sheet Flow,				
4.8	735	0.0250	2.55		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
16.3	785	Total							
	Summary for Subcatchment PS3A:								
Runoff	=	3.5 c	fs @ 12.3	2 hrs, Vol	ume= 17,405 cf, Depth= 3.07"				
Type III 2	24-hr 100) Year Ra	ainfall=8.10)"	ted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs				
A	<u>rea (sf)</u> 53,432	<u>CN</u>		ription ds, Good, I					
	12,217	61			ver, Good, HSG B				
	2,305	98			avement, HSG B				
	67,954	58	57 Weig	hted Avera	age, UI Adjusted				
	65,649			1% Perviou					
	2,305			% Impervio					
	2,305		100.0	00% Uncor	nnected				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
21.8	50	0.0200	0.04	(010)	Sheet Flow,				
21.0	00	0.0200	0.04		Woods: Dense underbrush n= 0.800 P2= 3.10"				
0.2	80	0.1250	5.69		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
22.0	130	Total							
			_	_					

Summary for Subcatchment PS4:

Runoff = 15.2 cfs @ 12.11 hrs, Volume= 50,462 cf, Depth= 3.52"

Area (sf)	CN	Adj	Description			
48,637	55		Woods, Good, HSG B			
107,523	61		>75% Grass cover, Good, HSG B			
10,372	98		Unconnected pavement, HSG B			
5,444	98		Unconnected roofs, HSG B			
171,976	63	61	Weighted Average, UI Adjusted			
156,160			90.80% Pervious Area			
15,816			9.20% Impervious Area			
15,816			100.00% Unconnected			

Type III 24-hr 100 Year Rainfall=8.10" Printed 11/19/2020 tions LLC Page 90

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	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	7.5	50	0.0100	0.11		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.10"
	0.1	50	0.2400	7.89		Shallow Concentrated Flow,
_						Unpaved Kv= 16.1 fps
	7.6	100	Total			

Summary for Subcatchment PS5:

Runoff = 4.2 cfs @ 12.27 hrs, Volume= 19,610 cf, Depth= 3.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.10"

A	rea (sf)	CN E	Description					
	48,067	55 V	5 Woods, Good, HSG B					
	23,521	61 >	75% Gras	s cover, Go	bod, HSG B			
	2,304	98 L	Inconnecte	ed pavemer	nt, HSG B			
	73,892	58 V	Veighted A	verage				
	71,588	g	6.88% Per	vious Area				
	2,304	3	.12% Impe	ervious Are	а			
	2,304	1	00.00% U	nconnected	1			
Тс	Length	Slope	Velocity	Capacity	Description			
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)				
18.6	50	0.0300	0.04		Sheet Flow,			
					Woods: Dense underbrush n= 0.800 P2= 3.10"			
0.8	180	0.0500	3.60		Shallow Concentrated Flow,			
					Unpaved Kv= 16.1 fps			
19.4	230	Total						

Summary for Subcatchment PS5A:

Runoff = 5.0 cfs @ 12.28 hrs, Volume= 23,456 cf, Depth= 2.96"

Area (sf)	CN	Adj	Description
77,272	55		Woods, Good, HSG B
16,576	61		>75% Grass cover, Good, HSG B
1,152	98		Unconnected pavement, HSG B
95,000	57	56	Weighted Average, UI Adjusted
93,848			98.79% Pervious Area
1,152			1.21% Impervious Area
1,152			100.00% Unconnected

Prepare	d by The	e Morin-C		Group, Inc	Type III 24-hr 100 Year Rainfall=8.10"c.Printed 11/19/2020c.Printed 11/19/2020c.Page 91
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
18.6	50	0.0300	0.04	· · · · ·	Sheet Flow,
0.3	100	0.1000	5.09		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
18.9	150	Total			
			Sun	nmary fo	r Subcatchment PS6:
Runoff	=	15.2 c	fs @ 12.1	3 hrs, Vol	ume= 52,757 cf, Depth= 3.75"
			nod, UH=S ainfall=8.1(ted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs
А	rea (sf)	CN A	Adj Desc	ription	
	67,828	55	Woo	ds, Good, I	HSG B
	74,644	61			ver, Good, HSG B
	11,625	98			avement, HSG B
	13,498	98		s, HSG B	
	1,343	98			curbs & sewers, HSG B
	68,938	64			age, UI Adjusted
I	42,472 26,466			3% Perviou 7% Impervi	
	11,625			2% Unconr	
	11,020		-0.0		
Тс	Length	Slope	Velocity	Capacity	Description
(min) (feet) (ft/ft) (ft/sec) (cfs)			ı 		
8.7	50	0.0500	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.10"

9.2 220 Total

170 0.1120

0.5

Summary for Subcatchment PS7:

Shallow Concentrated Flow, Unpaved Kv= 16.1 fps

Runoff = 12.6 cfs @ 12.09 hrs, Volume= 39,008 cf, Depth= 4.90"

5.39

Area (sf)	CN	Description
64,959	61	>75% Grass cover, Good, HSG B
10,888	98	Roofs, HSG B
7,062	98	Unconnected pavement, HSG B
12,647	98	Paved roads w/curbs & sewers, HSG B
95,556	73	Weighted Average
64,959		67.98% Pervious Area
30,597		32.02% Impervious Area
7,062		23.08% Unconnected

Prepared by Th	Proposed ConditionsType III 24-hr100 Year Rainfall=8.10"e Morin-Cameron Group, Inc.Printed 11/19/2020-3a s/n 00401 © 2020 HydroCAD Software Solutions LLCPage 92						
Tc Length (min) (feet)	Slope Velocity Capacity Description (ft/ft) (ft/sec) (cfs)						
6.0	Direct Entry,						
	Summary for Subcatchment PS8:						
Runoff =	6.6 cfs @ 12.08 hrs, Volume= 21,318 cf, Depth= 6.55"						
	R-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs 0 Year Rainfall=8.10"						
Area (sf)	CN Description						
25,064	98 Paved roads w/curbs & sewers, HSG B						
2,787 11,222	 98 Unconnected pavement, HSG B 61 >75% Grass cover, Good, HSG B 						
39,073	87 Weighted Average						
11,222	28.72% Pervious Area						
27,851	71.28% Impervious Area						
2,787	10.01% Unconnected						
Tc Length	Slope Velocity Capacity Description						
(min) (feet)	(ft/ft) (ft/sec) (cfs)						
6.0							
Summary for Subcatchment PS9:							
Runoff =	23.1 cfs @ 12.09 hrs, Volume= 72,898 cf, Depth= 5.84"						

Area (sf)	CN	Description				
22,164	98	Paved roads w/curbs & sewers, HSG B				
69,747	61	>75% Grass cover, Good, HSG B				
3,523	98	Unconnected pavement, HSG B				
54,442	98	Roofs, HSG B				
149,876	81	Weighted Average				
69,747		46.54% Pervious Area				
80,129		53.46% Impervious Area				
3,523		4.40% Unconnected				
Tc Length (min) (feet)	Slop	pe Velocity Capacity Description /ft) (ft/sec) (cfs)				
/	(11/					
6.0		Direct Entry,				

Summary for Reach DP1:

Inflow Area =	343,774 sf,	1.74% Impervious,	Inflow Depth = 3.18"	for 100 Year event
Inflow =	18.4 cfs @	12.33 hrs, Volume=	91,235 cf	
Outflow =	18.4 cfs @	12.33 hrs, Volume=	91,235 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2:

Inflow Area	a =	342,992 sf,	25.01% Impervious,	Inflow Depth >	3.80"	for 100 Year event
Inflow	=	19.1 cfs @	12.16 hrs, Volume=	108,682	of	
Outflow	=	19.1 cfs @	12.16 hrs, Volume=	108,682	cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP2A:

Inflow Area =	99,641 sf,	30.79% Impervious,	Inflow Depth = 2.70"	for 100 Year event
Inflow =	9.4 cfs @	12.14 hrs, Volume=	22,447 cf	
Outflow =	9.4 cfs @	12.14 hrs, Volume=	22,447 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3:

Inflow Area	a =	214,366 sf,	16.46% Impervious,	Inflow Depth =	3.04" 1	for 100 Year event
Inflow	=	12.9 cfs @	12.15 hrs, Volume=	54,353 c	f	
Outflow	=	12.9 cfs @	12.15 hrs, Volume=	54,353 c	f, Atten	= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP3A:

Inflow Area	a =	117,299 sf,	27.14% Impervious,	Inflow Depth = 2.93"	for 100 Year event
Inflow	=	8.4 cfs @	12.11 hrs, Volume=	28,592 cf	
Outflow	=	8.4 cfs @	12.11 hrs, Volume=	28,592 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP4:

Inflow Area =	455,469 sf,	37.90% Impervious,	Inflow Depth = 3.31"	for 100 Year event
Inflow =	16.0 cfs @	12.12 hrs, Volume=	125,817 cf	
Outflow =	16.0 cfs @	12.12 hrs, Volume=	125,817 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5:

Inflow Area =	433,386 sf,	13.96% Impervious,	Inflow Depth = 3.04"	for 100 Year event
Inflow =	26.9 cfs @	12.18 hrs, Volume=	109,719 cf	
Outflow =	26.9 cfs @	12.18 hrs, Volume=	109,719 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Reach DP5A:

Inflow Area	a =	190,556 sf,	16.66% Impervious,	Inflow Depth = 2.35"	for 100 Year event
Inflow	=	10.8 cfs @	12.26 hrs, Volume=	37,351 cf	
Outflow	=	10.8 cfs @	12.26 hrs, Volume=	37,351 cf, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

Summary for Pond 1P: Detention Basin

Inflow Area =	124,154 sf, 39.42% Impervic	ous, Inflow Depth = 5.18" for 100 Year event
Inflow =	16.9 cfs @ 12.09 hrs, Volun	ne= 53,616 cf
Outflow =	5.3 cfs @ 12.41 hrs, Volun	ne= 53,492 cf, Atten= 69%, Lag= 19.3 min
Primary =	5.3 cfs @ 12.41 hrs, Volun	ne= 53,492 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 109.29' @ 12.41 hrs Surf.Area= 6,966 sf Storage= 21,824 cf

Plug-Flow detention time= 157.8 min calculated for 53,477 cf (100% of inflow) Center-of-Mass det. time= 156.5 min (963.4 - 807.0)

Volume	Invert	Avail.Sto	rage Storage	Description	
#1	105.00'	26,98	B7 cf Custom	Stage Data (Prism	atic)Listed below (Recalc)
Elevatio (fee		ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
105.0 106.0)0)0	2,562 4,302	0 3,432	0 3,432	
108.0 110.0		5,832 7,589	10,134 13,421	13,566 26,987	
Device	Routing	Invert	Outlet Device:	S	
#1	Primary	98.00'	Inlet / Outlet I	Culvert L= 40.0' nvert= 98.00' / 96.00 w Area= 0.79 sf	Ke= 0.500)' S= 0.0500 '/' Cc= 0.900
#2 #3 #4	Device 1 Device 1 Device 1	105.00' 106.00' 107.60'	3.0" Vert. Ori 4.0" Vert. Ori 10.0" W x 3.0	fice/Grate C= 0.60	00 Limited to weir flow at low heads 00 Limited to weir flow at low heads cate C= 0.600
#5	Device 1	108.90'	Head (feet) 0	5' breadth Broad-C .20 0.40 0.60 0.80 i) 2.80 2.92 3.08 3	

Primary OutFlow Max=5.3 cfs @ 12.41 hrs HW=109.29' TW=0.00' (Dynamic Tailwater)

-2=Orifice/Grate (Orifice Controls 0.5 cfs @ 9.83 fps)

-3=Orifice/Grate (Orifice Controls 0.7 cfs @ 8.51 fps)

-4=Orifice/Grate (Orifice Controls 1.3 cfs @ 6.02 fps)

-5=Broad-Crested Rectangular Weir (Weir Controls 2.8 cfs @ 1.82 fps)

Summary for Pond 2P: Infiltration Basin

Inflow Area =	47,383 sf, 62.31% Impervious, Inflow Depth = 6.20" for 100 Year event
Inflow =	7.3 cfs @ 12.09 hrs, Volume= 24,469 cf
Outflow =	6.2 cfs @ 12.13 hrs, Volume= 23,992 cf, Atten= 15%, Lag= 3.0 min
Discarded =	0.2 cfs @ 12.13 hrs, Volume= 14,929 cf
Primary =	6.0 cfs @ 12.13 hrs, Volume= 9,063 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 109.74' @ 12.13 hrs Surf.Area= 3,765 sf Storage= 7,780 cf

Plug-Flow detention time= 267.0 min calculated for 23,985 cf (98% of inflow) Center-of-Mass det. time= 254.9 min (1,028.9 - 774.0)

Volume	Inver	t Avail.Sto	rage Storage [Description		
#1	106.00	' 8,7	99 cf Custom	Stage Data (Coni	c) Listed below (F	Recalc)
Elevatio (fee 106.0 108.0 110.0	20 20 20	urf.Area (sq-ft) 781 2,086 4,059	Inc.Store (cubic-feet) 0 2,762 6,037	Cum.Store (cubic-feet) 0 2,762 8,799	Wet.Area (sq-ft) 781 2,112 4,123	
Device	Routing	Invert	Outlet Devices	i		
#1	Primary	109.50'	Head (feet) 0.2 2.50 3.00 3.5	0	0 1.00 1.20 1.4	0 1.60 1.80 2.00
#2	Discarded	106.00'	2.85 3.07 3.2) 2.54 2.61 2.61 0 3.32 filtration over Su		

Discarded OutFlow Max=0.2 cfs @ 12.13 hrs HW=109.74' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.2 cfs)

Primary OutFlow Max=6.0 cfs @ 12.13 hrs HW=109.74' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Weir Controls 6.0 cfs @ 1.25 fps)

Summary for Pond 3P: Infiltration Basin

Willow Road Proposed ConditionsType III 24-hr100 Year Rainfall=8.10"Prepared by The Morin-Cameron Group, Inc.Printed11/19/2020HydroCAD® 10.10-3a s/n 00401 © 2020 HydroCAD Software Solutions LLCPage 96						
Inflow A Inflow Outflow Discarde Primary Routing	= = ed = =	44.4 cfs @ 1 7.8 cfs @ 1 0.5 cfs @ 1 7.3 cfs @ 1	2.09 hrs, Volum 2.55 hrs, Volum 2.55 hrs, Volum 2.55 hrs, Volum	ie= 142,44 ie= 114,3 ie= 39,0	73 cf, Atten= 82%, Lag= 27.7 min 17 cf 56 cf	
Peak Ele	ev= 109.60'	@ 12.55 hrs	Surf.Area= 22,04	43 sf Storage=	74,483 cf	
			nin calculated for nin (1,073.1 - 79	⁻ 114,373 cf (80%	6 of inflow)	
Volume			rage Storage D			-
#1	104.00	83,5	98 cf Custom	Stage Data (Cor	hic) Listed below (Recalc)	
Elevatio (fee		urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
104.0		8,168	0	0	8,168	
105.0		9,203	8,680	8,680	9,254	
106.0 108.0		10,294 15,794	9,743 25,893	18,424 44,316	10,400 15,959	
108.0		23,758	39,282	83,598	23,984	
110.0		20,700	00,202	00,000	20,004	
Device	Routing		Outlet Devices			-
#1	Primary	106.50'		Culvert L= 34.0		
					06.00' S= 0.0147 '/' Cc= 0.900 ed, Flow Area= 0.79 sf	
#2	Device 1	107.00'			600 Limited to weir flow at low heads	
#2	Device 1	108.00'			600 Limited to weir flow at low heads	
#4	Device 1	109.00'		rifice/Grate C=		
				flow at low head		
#5	Primary	109.50'	Head (feet) 0.2 2.50 3.00 3.50 Coef. (English)	20 0.40 0.60 0. 0 4.00 4.50 5.0	2.68 2.67 2.67 2.65 2.66 2.66	
#6	Discarded	104.00'	1.020 in/hr Ext	filtration over S	urface area Phase-In= 0.01'	
Discard	ed OutFlow	Max=0.5 cfs	@ 12 55 hrs HV	V=109.60' (Free	e Discharge)	

Discarded OutFlow Max=0.5 cfs @ 12.55 hrs HW=109.60' (Free Discharge) **G=Exfiltration** (Exfiltration Controls 0.5 cfs)

Primary OutFlow Max=7.3 cfs @ 12.55 hrs HW=109.60' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 5.7 cfs @ 7.28 fps) 2=Orifice/Grate (Passes < 0.4 cfs potential flow)

- **3=Orifice/Grate** (Passes < 1.1 cfs potential flow) **4=Orifice/Grate** (Passes < 9.6 cfs potential flow)

-5=Broad-Crested Rectangular Weir (Weir Controls 1.5 cfs @ 0.76 fps)

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Summary for Pond 4P: Infiltration Basin

Inflow Area =	49,345 sf,	59.84% Impervious,	Inflow Depth = 4.85" for	100 Year event
Inflow =	5.2 cfs @	12.09 hrs, Volume=	19,946 cf	
Outflow =	5.0 cfs @	12.11 hrs, Volume=	19,946 cf, Atten= 3	3%, Lag= 1.5 min
Discarded =	0.2 cfs @	12.11 hrs, Volume=	9,794 cf	
Primary =	4.8 cfs @	12.11 hrs, Volume=	10,152 cf	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 118.16' @ 12.11 hrs Surf.Area= 4,241 sf Storage= 3,449 cf

Plug-Flow detention time= 70.3 min calculated for 19,940 cf (100% of inflow) Center-of-Mass det. time= 70.3 min (851.3 - 781.0)

Volume	Invert	t Avail.Sto	orage Storage	age Storage Description			
#1	117.00	' 4,9	51 cf Custom	Stage Data (Coni	ic) Listed below (Red	alc)	
Elevatio	on S	urf.Area	Inc.Store	Cum.Store	Wet.Area		
(fee		(sq-ft)	(cubic-feet)	(cubic-feet)	(sq-ft)		
117.0	00	1,691	0	0	1,691		
118.0	00	4,012	2,769	2,769	4,019		
118.5	50	4,726	2,182	4,951	4,743		
Device	Routing	Invert	Outlet Device	S			
#1	Primary	117.90'			d-Crested Rectang 30 1.00 1.20 1.40		
			2.50 3.00 Coef. (English 3.30 3.31 3.3		2.85 2.98 3.08 3.	20 3.28 3.31	
#2	Primary	118.10'	25.0' long x [•] Head (feet) 0	1.0' breadth Broad	d-Crested Rectang 30 1.00 1.20 1.40		
			2.50 3.00 Coef. (English 3.30 3.31 3.3		2.85 2.98 3.08 3.	20 3.28 3.31	
#3	Discarded	117.00'			rface area Phase-	ln= 0.01'	
		M 00 (

Discarded OutFlow Max=0.2 cfs @ 12.11 hrs HW=118.16' (Free Discharge) **3=Exfiltration** (Exfiltration Controls 0.2 cfs)

Primary OutFlow Max=4.8 cfs @ 12.11 hrs HW=118.16' TW=0.00' (Dynamic Tailwater) -1=Broad-Crested Rectangular Weir (Weir Controls 3.7 cfs @ 1.39 fps) -2=Broad-Crested Rectangular Weir (Weir Controls 1.1 cfs @ 0.68 fps)

Summary for Pond 5P: Infiltration Basin

Inflow Area =	95,556 sf,	32.02% Impervious,	Inflow Depth = 4.90" for 100 Year event
Inflow =	12.6 cfs @	12.09 hrs, Volume=	39,008 cf
Outflow =	6.4 cfs @	12.24 hrs, Volume=	39,008 cf, Atten= 49%, Lag= 9.1 min
Discarded =	0.5 cfs @	12.24 hrs, Volume=	25,112 cf
Primary =	5.8 cfs @	12.24 hrs, Volume=	13,896 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs

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Peak Elev= 123.12' @ 12.24 hrs Surf.Area= 9,483 sf Storage= 11,794 cf

Plug-Flow detention time= 132.1 min calculated for 38,997 cf (100% of inflow) Center-of-Mass det. time= 132.1 min (950.0 - 817.9)

Volume	Inve	rt Avail.Sto	rage Storage	e Description	
#1	121.5	0' 20,80	63 cf Custor	n Stage Data (P	rismatic)Listed below (Recalc)
Elevatio		Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
121.5	50	2,680	0	0	
121.7	75	4,316	875	875	
122.0	00	7,408	1,466	2,340	
124.0	00	11,115	18,523	20,863	
Device	Routing	Invert	Outlet Device	es	
#1	Primary	122.75'	10.0' long x	2.0' breadth Br	oad-Crested Rectangular Weir
	-		Head (feet)	0.20 0.40 0.60	0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3	.50	
			Coef. (Englis	h) 2.54 2.61 2.	61 2.60 2.66 2.70 2.77 2.89 2.88
			2.85 3.07 3	.20 3.32	
#2	Discardeo	121.50'	2.410 in/hr E	Exfiltration over	Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.5 cfs @ 12.24 hrs HW=123.12' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.5 cfs)

Summary for Pond 6P: Recharge Trench

Inflow Area =	27,221 sf,100.00% Impervious,	Inflow Depth = 7.86" for 100 Year event
Inflow =	5.0 cfs @ 12.08 hrs, Volume=	17,830 cf
Outflow =	5.0 cfs @ 12.08 hrs, Volume=	17,830 cf, Atten= 0%, Lag= 0.0 min
Discarded =	0.0 cfs @ 3.94 hrs, Volume=	3,758 cf
Primary =	3.0 cfs @ 12.08 hrs, Volume=	13,037 cf
Secondary =	1.9 cfs @ 12.08 hrs, Volume=	1,035 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 121.33' @ 12.08 hrs Surf.Area= 720 sf Storage= 491 cf

Plug-Flow detention time= 32.5 min calculated for 17,830 cf (100% of inflow) Center-of-Mass det. time= 32.5 min (773.6 - 741.1)

Volume	Invert	Avail.Storage	Storage Description
#1	115.50'	392 cf	Custom Stage Data (Prismatic)Listed below (Recalc)
			1,080 cf Overall - 101 cf Embedded = 979 cf x 40.0% Voids
#2	116.17'	94 cf	6.0" Round Pipe Storage Inside #1
			L= 480.0'
			101 cf Overall - 0.1" Wall Thickness = 94 cf
#3	117.00'	12 cf	0.50'D x 10.00'H Vertical Cone/Cylinder x 6 -Impervious
		498 cf	Total Available Storage

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
115.50	720	0 1,080	0
117.00	720		1,080

Device	Routing	Invert	Outlet Devices
#1	Discarded	115.50'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'
#2	Primary	118.00'	4.0" Horiz. Orifice/Grate X 4.00 C= 0.600
			Limited to weir flow at low heads
#3	Secondary	120.00'	4.0" Horiz. Orifice/Grate X 4.00 C= 0.600
			Limited to weir flow at low heads

Discarded OutFlow Max=0.0 cfs @ 3.94 hrs HW=115.62' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=3.0 cfs @ 12.08 hrs HW=121.32' TW=118.16' (Dynamic Tailwater) **2=Orifice/Grate** (Orifice Controls 3.0 cfs @ 8.56 fps)

Secondary OutFlow Max=1.9 cfs @ 12.08 hrs HW=121.32' TW=0.00' (Dynamic Tailwater) -3=Orifice/Grate (Orifice Controls 1.9 cfs @ 5.53 fps)

MANAGEMENT CALCULATIONS

STORMWATER

APPENDIX D:

Stormwater Management Calculations

STANDARD 3: Recharge To Groundwater: Static Method

- Calculate Impervious Area (From HydroCAD Model) Proposed Impervious Area (HSG B Soil) = 370,950 SF
- Determine Rainfall Depth to be Recharged (MassDEP Stormwater Management Handbook: Table 2.3.2) Hydrologic Soil Group Recharge Rainfall Depth В

- Calculate Recharge Volume
 - *'Rv'* = [0.35" x 370,950 SF] / 12 SF-In = 10,820 CF

<u>'Rv' = 10,820 CF</u>

 Capture Area Adjustment Schedule of Areas Tributary to Recharge Systems

HCAD	Tributary
System ID	Impervious Area
PS7	30,597 sf
PS8	27,851 sf
PS9	80,129 sf
PS11	37,786 sf
PS13	7,749 sf
PS14	2,305 sf
PS15	21,777 sf
PS16	21,777 sf
PS17	27,221 sf
Total:	257,192 sf

Total Impervious Area = 370,950 SF

Capture Area Adjustment = 370,950 sf / 257,192 sf = 1.44 Required Recharge Volume '*Rv*' = 1.44 x Rv = 1.44 x 10,820 CF = 15,581 CF • Calculate Provided Recharge

HCAD	Bottom	Lowest System Outlet	Total Recharge
System ID	of System	or Top of Galley	Volume Provided
2P	106.00′	109.50′	6,910 CF
3P	104.00′	107.00′	29,995 CF
4P	117.00′	117.50′	1,094 CF
5P	121.50′	122.75′	8,417 CF
6P	115.50′	118.00′	486 CF
		Total Volume:	47,660 CF

Schedule of Proposed Recharge System Volumes

Recharge volume provided measured to lowest system outlet.

Required Recharge Volume Summary

Total Volume Provided Below Outlets = 47,660 CF Total Volume Required = 15,581 CF

Verify Drawdown, Maximum 72-Hours: Static Method

HCAD System ID	Recharge Volume (CF)	Bottom Surface Area (SF)	Rawls Rate (Inches/Hour)	Drawdown Time Rv / (K x A) (Hours)	Description
2P	6,910	781	2.41	44.1	Infiltration Basin
3P	29,995	8,168	1.02	43.2	Infiltration Basin
4P	1,094	1,691	2.41	3.2	Infiltration Basin
5P	8,417	2,680	2.41	15.6	Infiltration Basin
6P	486	720	2.41	3.4	Stone Trench

Design Complies with Recharge Volume Standard

STANDARD 4: Water Quality Volume

• <u>3P – Infiltration Basin</u>

- Tributary Impervious Area = 68,681 SF
- Calculate required water quality volume (1" depth)
 WQV = [1" x 68,681 SF] / 12 SF-In = 5,723 CF
- Lowest outlet elevation = 107.00'
 WQV provided below lowest outlet = 29,995 CF (OK)

• <u>5P – Infiltration Basin</u>

- Tributary Impervious Area = 12,647 SF
- Calculate required water quality volume (1" depth)
 - WQV = [1" x 12,647 SF] / 12 SF-In = **1,054 CF**
- Lowest outlet elevation = 122.75'
 WQV provided below lowest outlet = 8,417 CF (OK)

• <u>3P – Infiltration Basin Forebay</u>

- Tributary Impervious Area = 68,681 SF
- Calculate required treatment volume (0.1" depth)
 - WQV = [0.1" x 68,681 SF] / 12 SF-In = **572 CF**
- Lowest outlet elevation = 107.00'
 WQV provided below forebay outlet = 1,297 CF (OK)

• <u>5P – Infiltration Basin Forebay</u>

- Tributary Impervious Area = 12,647 SF
- Calculate required treatment volume (0.1" depth)
 WQV = [0.1" x 12,647 SF] / 12 SF-In = **105 CF**
- Lowest outlet elevation = 121.50'
 WQV provided below forebay outlet = 376 CF (OK)

Pipe Sizing Calculation Spreadsheet:

THE MORIN-CAMERON GROUP, INC. 25 Kenoza Avenue

Haverhill, MA

P: (978) 373-0310

F: (978) 774-3488

W: www.morincameron.com

Name: The Willows at Boxford Location: Willow Road Boxford, MA County: Essex County Owner: Toll Brothers, Inc.

Proj. No.: 3717 Date: 11/19/2020 **Revised:** Computed by: Annie Raftery, EIT Checked by: Scott P, Cameron, P.E.

	LOCATION						FLOW TIME (MIN)			DESIGN					CAPACITY		PIPE PROFILE				
DESCRIPTION	FROM	то	AREA (AC.)	С	СхА	SUM C x A	PIPE	CONC. TIME	į*	Q cfs	V fps	n	PIPE SIZE	SLOPE	Q full ft^3/s	V full ft/s	LENGTH ft	FALL ft	RIM	INV UPPER	INV LOWER
CB-1	CB-1	DMH-1	0.21	0.85	0.17	0.17	0.09	6.0	5.7	1.0	3.4	0.012	12	0.010	3.9	4.9	18	0.18	124.90	121.80	121.62
CB-2	CB-2	DMH-2	0.15	0.90	0.13	0.13	0.02	6.0	5.7	0.8	3.1	0.012	12	0.010	3.9	4.9	3	0.03	124.90	121.80	121.77
DMH-1	DMH-1	FES-1	0.35	0.87	0.31	0.31	0.36	6.1	5.7	1.8	3.2	0.012	12	0.005	2.7	3.5	68	0.34	124.82	121.67	121.33
CB-3	CB-3	DMH-2	0.30	0.75	0.22	0.22	0.11	6.0	5.7	1.3	3.7	0.012	12	0.010	3.8	4.8	24	0.23	121.33	118.23	118.00
CB-4	СВ-4	DMH-2	0.24	0.77	0.18	0.18	0.09	6.0	5.7	1.0	4.5	0.012	12	0.021	5.6	7.1	23	0.48	121.33	118.23	117.75
DMH-2	DMH-2	DMH-3	0.53	0.76	0.40	0.40	0.20	6.1	5.7	2.3	4.9	0.012	12	0.014	4.5	5.7	58	0.79	121.60	117.65	116.86
DMH-3	DMH-3	DMH-4	0.53	0.76	0.40	0.40	0.71	6.3	5.7	2.3	5.1	0.012	12	0.016	4.8	6.2	219	3.45	120.23	116.76	113.31
CB-5	CB-5	DMH-4	0.23	0.78	0.18	0.18	0.05	6.0	5.7	1.0	3.5	0.012	12	0.010	3.9	4.9	11	0.11	116.55	113.45	113.34
CB-6	CB-6	DMH-4	0.15	0.70	0.10	0.10	0.07	6.0	5.7	0.6	3.4	0.012	12	0.017	5.1	6.4	14	0.24	116.55	113.45	113.21
DMH-4	DMH-4	DMH-8	0.90	0.76	0.68	0.68	0.29	7.0	5.5	3.8	6.3	0.012	12	0.019	5.3	6.7	108	2.01	116.83	113.11	111.10
CB-7	CB-7	DMH-5	0.04	0.90	0.04	0.04	0.50	6.0	5.7	0.2	1.7	0.012	12	0.006	3.1	4.0	51	0.33	118.48	115.38	115.05
CB-8	CB-8	DMH-5	0.33	0.46	0.15	0.15	0.37	6.0	5.7	0.9	2.3	0.012	12	0.004	2.4	3.0	52	0.20	118.48	115.38	115.18
DMH-5	DMH-5	DMH-6	0.37	0.51	0.19	0.19	0.76	6.5	5.6	1.1	3.5	0.012	12	0.010	3.9	4.9	160	1.60	119.66	115.05	113.45
DMH-6	DMH-6	DMH-7	0.37	0.51	0.19	0.19	0.48	7.3	5.5	1.0	3.5	0.012	12	0.010	3.9	4.9	102	1.03	118.99	113.35	112.32
CB-9	СВ-9	DMH-7	0.31	0.57	0.18	0.18	0.08	6.0	5.7	1.0	3.6	0.012	12	0.011	4.1	5.2	18	0.20	116.52	113.42	113.22
CB-10	CB-10	DMH-7	0.05	0.90	0.05	0.05	0.09	6.0	5.7	0.3	2.2	0.012	12	0.011	4.0	5.1	12	0.13	116.52	113.42	113.29
DMH-7	DMH-7	DMH-8	0.74	0.56	0.41	0.41	0.19	7.7	5.3	2.2	6.4	0.012	12	0.028	6.5	8.3	71	2.02	116.23	113.12	111.10
DMH-8	DMH-8	FES-2	1.64	0.67	1.09	1.09	0.19	7.9	5.3	5.8	8.9	0.012	12	0.034	7.1	9.0	104	3.50	115.07	111.00	107.50
CB-11	CB-11	DMH-9	0.35	0.79	0.28	0.28	0.06	6.0	5.7	1.6	4.1	0.012	12	0.011	4.0	5.1	15	0.16	112.69	109.59	109.43
CB-12	CB-12	DMH-9	0.56	0.65	0.36	0.36	0.09	6.0	5.7	2.1	4.3	0.012	12	0.010	3.9	5.0	22	0.23	112.69	109.59	109.36
DMH-9	DMH-9	FES-3	0.91	0.70	0.64	0.64	0.08	6.1	5.7	3.7	8.5	0.012	12	0.044	8.1	10.3	40	1.76	112.80	109.26	107.50
CB-16	CB-16	DMH-11	0.32	0.69	0.22	0.22	0.05	6.0	5.7	1.3	5.8	0.012	12	0.038	7.5	9.6	16	0.61	120.11	117.01	116.40
CB-15	CB-15	DMH-11	0.37	0.69	0.26	0.26	0.04	6.0	5.7	1.5	6.5	0.012	12	0.044	8.1	10.3	14	0.61	120.11	117.01	116.40
DMH-11	DMH-11	DMH-10	0.69	0.69	0.47	0.47	0.29	6.0	5.7	2.7	8.2	0.012	12	0.048	8.4	10.8	142	6.80	119.56	116.30	109.50
DMH-10	DMH-10	DMH-12	0.69	0.69	0.47	0.47	0.35	6.3	5.7	2.7	5.4	0.012	12	0.016	4.9	6.3	114	1.87	112.67	109.40	107.53

Design Parameters:

0.2

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IDF Curve Year Storm Boston, MA -

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THE MORIN-CAMERON GROUP, INC.

25 Kenoza Avenue

Haverhill, MA

P: (978) 373-0310

F: (978) 774-3488

W: www.morincameron.com

Pipe Sizing Calculation Spreadsheet:

Name: The Willows at Boxford Location: Willow Road Boxford, MA County: Essex County Owner: Toll Brothers, Inc. Proj. No.: 3717 Date: 11/19/2020 Revised: Computed by: Annie Raftery, EIT Checked by: Scott P, Cameron, P.E.

	LOCA	ΓΙΟΝ					FLOW	FLOW TIME (MIN)		FLOW TIME (MIN)		FLOW TIME (MIN)				DESIGN			CA	ΡΑϹΙΤΥ			PIPE PROFIL	.E	
DESCRIPTION	FROM TO		AREA (AC.)	с	CXA	SUM C x A	PIPE	CONC. TIME	į*	Q cfs	V fps	n	PIPE SIZE	SLOPE	Q full ft^3/s	V full ft/s	LENGTH ft	FALL ft	RIM	INV UPPER	INV LOWER				
CB-13	CB-13	DMH-12	0.58	0.73	0.42	0.42	0.06	6.0	5.7	2.4	4.5	0.012	12	0.011	4.0	5.1	16	0.17	110.85	107.70	107.53				
CB-14	CB-14	DMH-12	0.55	0.67	0.36	0.36	0.01	6.0	5.7	2.1	6.6	0.012	12	0.034	7.1	9.1	5	0.17	110.85	107.70	107.53				
DMH-12	DMH-12	CDS-1	1.81	0.70	1.26	1.26	0.10	6.7	5.6	7.0	7.7	0.012	18	0.022	17.0	9.6	46	1.03	110.85	106.93	105.90				
CDS-1	CDS-1	FES-4	1.81	0.70	1.26	1.26	0.79	6.8	5.6	7.0	4.8	0.012	18	0.006	8.6	4.9	226	1.30	111.38	105.80	104.50				

Design	Parameters:
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IDF Curve Year Storm Boston, MA 👻

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THE MORIN-CAMERON GROUP, INC. 25 Kenoza Avenue Haverhill, MA 01830 P: (978) 373-0310 F: (978) 774-3488 W: www.morincameron.com

Description of Area	Area	Runoff	AxC
CB-1	(acres)	Coefficient	
Pervious	0.020	0.35	0.01
Impervious	0.185	0.90	0.17
Totals =	0.205		0.17

Weighted Runoff Coefficient = S(AxC) / SA = 0.85

Description of Area	Area	Runoff	AxC
CB-3	(acres)	Coefficient	12
Pervious	0.080	0.35	0.03
Impervious	0.215	0.90	0.19
Totals =	0.295		0.22

Weighted Runoff Coefficient = S(AxC) / SA = 0.75

Description of Area	Area	Runoff	AxC
CB-5	(acres)	Coefficient	
Pervious	0.049	0.35	0.02
Impervious	0.176	0.90	0.16
Totals =	0.225		0.18

Weighted Runoff Coefficient = S(AxC) / SA = 0.78

Description of Area	Area	Runoff	AxC
CB-7	(acres)	Coefficient	
Pervious	0.000	0.35	0.00
Impervious	0.042	0.90	0.04
Totals =	0.042		0.04

Weighted Runoff Coefficient = S(AxC) / SA = 0.90

Description of Area	Area	Runoff	AxC
CB-9	(acres)	Coefficient	
Pervious	0.187	0.35	0.07
Impervious	0.122	0.90	0.11
Totals =	0.309		0.18

Weighted Runoff Coefficient = S(AxC) / SA

Description of Area	Area	Runoff	AxC
CB-11	(acres)	Coefficient	
Pervious	0.068	0.35	0.02
Impervious	0.282	0.90	0.25
Totals =	0.350		0.28

Weighted Runoff Coefficient = S(AxC) / SA 0.79

Description of Area CB-13	Area (acres)	Runoff Coefficient	AxC
Pervious	0.182	0.35	0.06
Impervious	0.393	0.90	0.35
Totals =	0.575		0.42

Weighted Runoff Coefficient = S(AxC) / SA = 0.73

Description of Area CB-15	Area (acres)	Runoff Coefficient	AxC
Pervious	0.139	0.35	0.05
Impervious	0.230	0.90	0.21
Totals =	0.369		0.26

Weighted Runoff Coefficient = S(AxC) / SA = 0.69

Pervious Soil 0.35

Impervious 0.9

Rainfall Intensity (i) 5.7

Description of Area	Area	Runoff	AxC
CB-2	(acres)	Coefficient	
Pervious	0.000	0.35	0.00
Impervious	0.148	0.90	0.13
	1		
Totals =	0.148		0.13

Weighted Runoff Coefficient = S(AxC) / SA = 0.90

Description of Area	Area	Runoff	AxC
CB-4	(acres)	Coefficient	그는 문제 같이
Pervious	0.054	0.35	0.02
Impervious	0.182	0.90	0.16
			4 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
Totals =	0.236		0.18

Weighted Runoff Coefficient = S(AxC) / SA = 0.77

Description of Area	Area	Runoff	AxC
CB-6	(acres)	Coefficient	
Pervious	0.053	0.35	0.02
Impervious	0.092	0.90	0.08
	1.11		a strand states in
Totals =	0.145		0.10

Weighted Runoff Coefficient = S(AxC) / SA = 0.70

Description of Area	Area	Runoff	AxC
CB-8	(acres)	Coefficient	
Pervious	0.266	0.35	0.09
Impervious	0.067	0.90	0.06
	1997 - A.		
Totals =	0.333		0.15

Weighted Runoff Coefficient = S(AxC) / SA = 0.46

Description of Area CB-10	Area (acres)	Runoff Coefficient	AxC
Pervious	0.000	0.35	0.00
Impervious	0.052	0.90	0.05
		T	
Totals =	0.052		0.05

efficient = S(AxC) / SA = 0.90

Description of Area	Area	Runoff	AxC
CB-12	(acres)	Coefficient	
Pervious	0.254	0.35	0.09
Impervious	0.303	0.90	0.27
			and the left of the
Totals =	0.557		0.36

oefficient = S(AxC) / SA = 0.65 Weighted Runof

Description of Area	Area	Runoff	AxC
CB-14	(acres)	Coefficient	
Pervious	0.230	0.35	0.08
Impervious	0.315	0.90	0.28
	100 A.A.A.A.	1	
Totals =	0.545	1	0.36

Weighted Runoff Coefficient = S(AxC) / SA = 0.67

Description of Area CB-16	Area (acres)	Runoff Coefficient	AxC	
Pervious	0.122	0.35	0.04	
Impervious	0.196	0.90	0.18	
Totals =	0.318		0.22	

Weighted Runoff Coefficient = S(AxC) / SA = 0.69

C'- Coefficients

= 0.57		Weighted Runoff Coe
	AxC	Description of Area
t		CB-12
	0.02	Pervious
	0.25	Impervious
	0.28	Totals =
=	0.79	Weighted Runoff Coe

THE MO 66 Elm Sti	RIN-CAMERON GROUP,		Standard 4: Total Suspended Solids Calculation Detention Basin (1P)			
Danvers, MA 01923 Name		Location:	The Willows at Boxford Willow Road Boxford, MA	Revised:	11/19/2020	
Å		County: Applicant:	Essex Toll Brothers, Inc.		Daniel Powers, E.I.T. Scott P. Cameron, P.E.	
ВС		С	D	Е	F	
	TSS Removal BMP Rate		Starting TSS Load (*F)	Amount Removed (C*D)	Remaining Load (D-E)	
heet	Deep Sump and Hooded Catch Basin	0.25	1.00	0.25	0.75	
Removal on Worksheet	Proprietary Treatment Practice	0.80	0.75	0.60	0.15	
a)	Dry Detention Basin	0.00	0.15	0.00	0.15	
TSS Re Calculation		0.00	0.15	0.00	0.15	
Calc		0.00	0.15	0.00	0.15	

Total TSS Removal =

*Equals remaining load from previous BMP (E) which enters the BMP

85%

THE MORIN-CAMERON GROUP, INC.Standard 4: Total Suspended S66 Elm Street,Infiltration Basin (3P) Pretreated					
Danvers, MA 01923 Na p 978.777.8586 Loca Course		Name: Location: County:	The Willows at Boxford Willow Road Boxford, MA	Proj. No.: Date: Revised: Computed by:	3717 11/19/2020 Daniel Powers, E.I.T. Scott P. Cameron, P.E.
	B C TSS Ren		D Starting TSS	E Amount	F Remaining
	BMP	Rate	Load (*F)	Removed (C*D)	Load (D-E)
heet	Deep Sump and Hooded Catch Basin	0.25	1.00	0.25	0.75
TSS Removal Calculation Worksheet	Sediment Forebay	0.25	0.75	0.19	0.56
Rem on M		0.00	0.56	0.00	0.56
TSS sulatio		0.00	0.56	0.00	0.56
Calc	0.00 0.56		0.00	0.56	
	Total TSS Removal =				

*Equals remaining load from previous BMP (E) which enters the BMP

THE MO 66 Elm Str	RIN-CAMERON GROUP,		Standard 4: Total Suspended So Infiltration Basin (3P)	lids Calculation	
Danvers, N			The Willows at Boxford	Proj. No.:	
p 978.77	77.8586	Location:	Willow Road Boxford, MA	Revised:	11/19/2020
		County:	Essex		Daniel Powers, E.I.T.
		Applicant:	Toll Brothers, Inc.	Checked by:	Scott P. Cameron, P.E.
	ВС		D	E	F
		TSS Removal	Starting TSS	Amount	Remaining
	BMP	Rate	Load (*F)	Removed (C*D)	Load (D-E)
heet	Deep Sump and Hooded Catch Basin 0.25 Sediment Forebay 0.25		1.00	0.25	0.75
Removal on Works			0.75	0.19	0.56
s Rem ion W	Infiltration Basin	0.80	0.56	0.45	0.11

TSS R Calculation

Total TSS Removal =

0.11

0.11

0.00

0.00

*Equals remaining load from previous BMP (E) which enters the BMP

0.11

0.11

0.00

0.00

89%

THE MORIN-CAMERON GROUP, INC.Standard 4: Total Suspended S66 Elm Street,Infiltration Basin (5P) Pretreated					
Danvers, MA 01923 Na p 978.777.8586 Locat Cou		Name: Location: County:	The Willows at Boxford Willow Road Boxford, MA	Proj. No.: Date: Revised: Computed by:	3717 11/19/2020 Daniel Powers, E.I.T. Scott P. Cameron, P.E.
	B C TSS Rem		D Starting TSS	E Amount	F Remaining
	BMP	Rate	Load (*F)	Removed (C*D)	Load (D-E)
heet	Deep Sump and Hooded Catch Basin	0.25	1.00	0.25	0.75
TSS Removal Calculation Worksheet	Sediment Forebay	0.25	0.75	0.19	0.56
Rem on M		0.00	0.56	0.00	0.56
TSS sulatio		0.00	0.56	0.00	0.56
Calc	0.00 0.56		0.00	0.56	
	Total TSS Removal =				

*Equals remaining load from previous BMP (E) which enters the BMP

THE MO 66 Elm St	RIN-CAMERON GROUP,		Standard 4: Total Suspended Solids Calculation Infiltration Basin (5P)			
Danvers, MA 01923 p 978.777.8586		Name: Location: County:	Name: The Willows at Boxford Location: Willow Road Boxford, MA County: Essex Applicant: Toll Brothers, Inc.		3717 11/19/2020 Daniel Powers, E.I.T. Scott P. Cameron, P.E.	
В		С	D	E	F	
	BMP	TSS Removal Rate	Starting TSS Load (*F)	Amount Removed (C*D)	Remaining Load (D-E)	
heet	Deep Sump and Hooded Catch Basin	0.25	1.00	0.25	0.75	
moval Worksheet	Sediment Forebay	0.25	0.75	0.19	0.56	
	Infiltration Basin	0.80	0.56	0.45	0.11	
TSS Re Calculation		0.00	0.11	0.00	0.11	
Calc		0.00	0.11	0.00	0.11	

Total TSS Removal =

*Equals remaining load from previous BMP (E) which enters the BMP

89%

APPENDIX E: VERNAL POOL WATER BUDGET SUMMARY

		<u>Exist</u>	ing Con	<u>ditions</u>		
<u>2-Year</u> Vernal Pool 1	Subcatchment	Area	Rainfall	Total Volume	Surface Flow	Infiltration
DP2A	ES2A	84051	0.27	22,694	2,970	19,724
Vernal Pool 2						
DP5A	ES5A	168926	0.27	45,610	5,476	40,134
Vernal Pool 3						
DP3A	ES3A	115072	0.27	31,069	3,099	27,970
<u>10-Year</u> Vernal Pool 1	Subcatchment	Area	Rainfall	Total Volume	Surface Flow	Infiltration
DP2A	ES2A	84051	0.4267	35,865	9,608	26,257
Vernal Pool 2						
DP5A	ES5A	168926	0.4267	72,081	18,341	53,740
Vernal Pool 3						
DP5A	ES3A	115072	0.4267	49,101	11,211	37,890
<u>100-Year</u> Vernal Pool 1	Subcatchment	Area	Rainfall	Total Volume	Surface Flow	Infiltration
DP2A	ES2A	84051	0.675	56,734	23,874	32,860
Vernal Pool 2						
DP5A	ES5A	168926	0.675	114,025	56,404	57,621
Vernal Pool 3						
DP3A	ES3A	115072	0.675	77,674	29,473	48,201

Proposed Conditions							
<u>2-Year</u>	Subcatchment	Area	Rainfall	Total Volume	Surface Flow	Infiltration	
Vernal Pool 1							
DP2A	PS2A	52,258	0.27	14,110	1407	12,703	
	PS13	25,606	0.27	6,914	2037	4,877	
	2P	-	-	7,494	0	7,494	
Vernal Pool 2		05 000	0.07	25 650	2244	22.226	
DP5A	PS5A	95,000	0.27	25,650	2314	23,336	
	PS7	95,556	0.27	25,800	8030	17,770	
	5P	-	-	8,030	0	8,030	
Vernal Pool 3							
DP3A	PS3A	67,954	0.27	18,348	1830	16,518	
	PS14	22,124	0.27	5,973	991	4,982	
	4P	,	_	4,910	222	4,688	
	6P	_	_	2,903	0	2,903	
	UF	-	-	2,903	0	2,903	
10-Year	Subcatchment	Area	Rainfall	Total Volume	Surface Flow	Infiltration	
Vernal Pool 1							
DP2A	PS2A	52,258	0.4267	22,298	5091	17,207	
	PS13	25,606	0.4267	10,926	4888	6,038	
	2P	-	-	13,749	646	13,103	
Vernal Pool 2							
DP5A	PS5A	95,000	0.4267	40,537	8740	31,797	
	PS7	95,556	0.4267	40,774	18912	21,862	
	5P	-	-	18,912	0	18,912	
Vernal Pool 3	500.0						
DP3A	PS3A	67,954	0.4267	28,996	6,620	22,376	
	PS14	22,124	0.4267	9,440	2,923	6,517	
	4P	-	-	10,360	3474	6,886	
	6P	-	-	3,566	176	3,390	
<u> 100-Year</u>	Subcatchment	Area	Rainfall	Total Volume	Surface Flow	Infiltration	
Vernal Pool 1							
DP2A	PS2A	52,258	0.675	35,274	13385	21,889	
	PS13	25,606	0.675	17,284	10205	7,079	
	2P	-	-	24,469	9063	15,406	
Vernal Pool 2	D.C.T. 1		0	<i></i>	22.5	10.000	
DP5A	PS5A	95,000	0.675	64,125	23456	40,669	
	PS7	95,556	0.675	64,500	39008	25,492	
	5P	-	-	39,008	13896	25,112	

Vernal Pool 3 DP3A

PS3A	67,954	0.675	45,869	17405	28,464
PS14	22,124	0.675	14,934	6909	8,025
4P	-	-	19,946	10152	9,794
6P	-	-	4776	1018	3,758

Infiltration Comparison							
		Existing	Proposed	Delta	%		
Vernal Pool 1							
	2-Year	19,724	25,073	5,350	27.1%		
	10-Year	26,257	36,349	10,092	38.4%		
	100-Year	32,860	44,374	11,514	35.0%		
Vernal Pool 2							
	2-Year	40,134	49,136	9,002	22.4%		
	10-Year	53,740	72,570	18,831	35.0%		
	100-Year	57,621	91,273	33,652	58.4%		
Vernal Pool 3							
	2-Year	27,970	29,091	1,121	4.0%		
	10-Year	37,890	39,169	1,279	3.4%		
	100-Year	48,201	50,041	1,840	3.8%		

Total Volume Comparison

		Existing	Proposed	Delta	
Vernal Pool 1					
	2-Year	22,694	26,480	3,787	16.7%
	10-Year	35,865	42,086	6,221	17.3%
	100-Year	56,734	66,822	10,088	17.8%
Vernal Pool 2					
	2-Year	45,610	51,450	5,840	12.8%
	10-Year	72,081	81,310	9,230	12.8%
	100-Year	114,025	128,625	14,600	12.8%
Vernal Pool 3					
	2-Year	31,069	31,143	74	0.2%
	10-Year	49,101	49,263	162	0.3%
	100-Year	77,674	77,598	-76	-0.1%

BEST MANAGEMENT PRACTICES

CONSTRUCTION PHASE

APPENDIX F:

Construction Phase Best Management Practices (BMP's)

Erosion and Sedimentation will be controlled at the site by utilizing Structural Practices, Stabilization Practices, and Dust Control. These practices correspond with plans entitled "Site Plan of Land for the Willows at Boxford" in Boxford, Massachusetts, Willow Road prepared by The Morin-Cameron Group, Inc. dated November 19, 2020 as revised and approved by the Boxford Planning Board, hereinafter referred to as the Site Plans.

Responsible Party Contact Information:	
Stormwater Management System Owner:	Toll Brothers, Inc.
	134 Flanders Road
	Westborough, MA 01581
	P: (508) 366-1440
Boxford Department of Public Works:	7B Spofford Road
	Boxford MA 01921
	P: (978) 685-0950
Boxford Planning Board:	7A Spofford Road
-	Boxford MA 01921
	P: (978) 887 6000
Boxford Zoning Board of Appeals:	7A Spofford Road
	Boxford MA 01921
	P: (978) 887-6401
Boxford Conservation Commission:	7A Spofford Road
	Boxford MA 01921
	P: (978) 887-6000 ext. 181
Site Design Engineer Information:	The Morin-Cameron Group,
	66 Elm Street
	Danvers, MA 01923
	Phone: (978) 777-8586

Inc.

Structural Practices:

- <u>Silt Fence & Silt Sock</u> A siltation fence and sock barrier shall be installed in accordance with the approved plans where high rates of stormwater runoff are anticipated.
 - a) Installation Schedule: Prior to Start of land disturbance
 - a) Maintenance and Inspection: The site supervisor shall inspect the barrier at least once per week or after a major storm (3.15 inches of rainfall within a twenty-four-hour period). event and shall repair any damaged or affected areas of the barrier at the time they are noted. Remove sediment deposits promptly after storm events to provide adequate storage volume for the next rain and to reduce pressure on the barrier. Sediment will be removed from in front of the barrier when it becomes about 4" deep at the barrier. Take care to avoid undermining the barrier during cleanout.
- 2) Inlet Protection Inlet Protection will be utilized around the catch basin grates in the street layout in the closest down gradient structure. The inlet protection will allow the storm drain inlets to be used before final stabilization. This structural practice will allow early use of the drainage system. Siltsack or equivalent will be utilized for the inlet protection. Siltsack is manufactured by ACF Environmental. The telephone number is 800-448-3636. Regular flow siltsack will be utilized, and if it does not allow enough storm water flow, hi-flow siltsack will be utilized.

Silt Sack (or equivalent) Inlet Protection Inspection/Maintenance Requirements *

- a) The silt sack trapping devices and the catch basins should be inspected after every rain storm and repairs made as necessary.
- b) Sediment should be removed from the silt sack after the sediment has reached a maximum depth of one-half the depth of the trap.
- c) Sediment should be disposed of in a suitable area and protected from erosion by either structural or vegetative means. Sediment material removed shall be disposed of in accordance with all applicable local, state, and federal regulations.
- d) The silt sack must be replaced if it is ripped or torn in any way.
- e) Temporary traps should be removed and the area repaired as soon as the contributing drainage area to the inlet has been completely stabilized.

3) Sediment Track-Out: The site supervisor will inspect and ensure that sediment is not tracked into the roadway. If tracking onto the roadway is noted, it shall be removed immediately via by hand or a mechanical street sweeper. (If Required: Stabilized Construction Exit: Crushed stone anti-tracking pads will be installed at the entrance to the site. This will prevent trucks from tracking material onto the road from the construction site. If, at any point during the project, the tracking pad becomes ineffective due to accumulation of soil, the crushed stone shall be replaced. Details for construction of the stabilized entrance can be found in the details sheet that is part of the permit plan set associated with the project. The site supervisor will inspect the tracking pads weekly to ensure that they are properly limiting the tracking of soil onto the road. If tracking onto the roadway is noted, it shall be removed immediately via by hand or a mechanical street sweeper.)

Stabilization Practices:

Stabilization measures shall be implemented as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased, but in no case more than 14 days after the construction activity in that portion of the site has temporarily or permanently ceased, with the following exceptions.

- Where the initiation of stabilization measures by the 14th day after construction activity temporary or permanently cease is precluded by snow cover, stabilization measures shall be initiated as soon as practicable.
- Where construction activity will resume on a portion of the site within 21 days from when activities ceased, (e.g. the total time period that construction activity is temporarily ceased is less than 21 days) then stabilization measures do not have to be initiated on that portion of the site by the 14th day after construction activity temporarily ceased.
- <u>Temporary Seeding</u> Temporary seeding will allow a short-term vegetative cover on disturbed site areas that may be in danger of erosion. Temporary seeding will be done at stock piles and disturbed portions of the site where construction activity will temporarily cease for at least 21 days. The temporary seeding will stabilize cleared and unvegetated areas that will not be brought into final grade for several weeks or months.

Temporary Seeding Planting Procedures *

 a) Planting should preferably be done between April 1st and June 30th, and September 1st through September 31st. If planting is done in the months of July and August, irrigation may be required. If planting is done between October 1st and March 31st, mulching should be applied immediately after planting. b) Before seeding, install structural practice controls. Utilize Amoco supergro or equivalent.

Species	Seeding Rate	Seeding Rate	Recommended Seeding	Seed Cover
	(lbs./1,000 sq.)	(lbs./acre)	Dates	required
Annual	1	40	April 1 st to June 1 st	¼ inch
Ryegrass			August 15 th to Sept. 15 th	
Foxtail	0.7	30	May 1 st to June 30 th	1⁄2 to 3⁄4 inch
Millet				
Oats	2	80	April 1 st to July 1 st	1 to 1-½
			August 15 th to Sept. 15 th	inch
Winter	3	120	August 15 th to Oct. 15 th	1 to 1-½
Rye				inch

c) Select the appropriate seed species for temporary cover from the following table.

Apply the seed uniformly by hydroseeding, broadcasting, or by hand.

d) Use effective mulch, such as clean grain straw; tacked and/or tied with netting to protect seedbed and encourage plant growth.

Temporary Seeding Inspection/Maintenance *

- a) Inspect within 6 weeks of planting to see if stands are adequate. Check for damage within 24 hours of the end to a heavy rainfall, defined as a 2-year storm event (i.e., 3.15 inches of rainfall within a twenty-four-hour period). Stands should be uniform and dense. Reseed and mulch damaged and sparse areas immediately. Tack or tie down mulch as necessary.
- b) Seeds should be supplied with adequate moisture. Furnish water as needed, especially in abnormally hot or dry weather. Water application rates should be controlled to prevent runoff.
- <u>Geotextiles</u> Geotextiles such as jute netting will be used in combination with other practices such as mulching to stabilize slopes. The following geotextile materials or equivalent are to be utilized for structural and nonstructural controls as shown in the following table.

Practice	Manufacturer	Product	Remarks
Sediment Fence	Amoco	Woven polypropylene	0.425 mm opening
		1198 or equivalent	
Construction	Amoco	Woven polypropylene	0.300 mm opening
Entrance		2002 or equivalent	

Outlet Protection	Amoco	Nonwoven polypropylene 4551 or equivalent	0.150 mm opening
Erosion Control (slope stability)	Amoco	Supergro or equivalent	Erosion control revegetation mix, open polypropylene fiber on degradable polypropylene net scrim

Amoco may be reached at (800) 445-7732

Geotextile Installation

a) Netting and matting require firm, continuous contact between the materials and the soil. If there is no contact, the material will not hold the soil and erosion will occur underneath the material.

Geotextile Inspection/Maintenance *

- a) In the field, regular inspections should be made to check for cracks, tears, or breaches in the fabric. The appropriate repairs should be made.
- 3) <u>Mulching and Netting</u> Mulching will provide immediate protection to exposed soils during the period of short construction delays, or over winter months through the application of plant residues, or other suitable materials, to exposed soil areas. In areas, which have been seeded either for temporary or permanent cover, mulching should immediately follow seeding. On steep slopes, mulch must be supplemented with netting. The preferred mulching material is straw.

Mulch (Hay or Straw) Materials and Installation

a) Straw has been found to be one of the most effective organic mulch materials. The specifications for straw are described below, but other material may be appropriate. The straw should be air-dried; free of undesirable seeds & coarse materials. The application rate per 1,000 sq. is 90-100 lbs. (2-3 bales) and the application rate per acre is 2 tons (100-120 bales). The application should cover about 90% of the surface. The use of straw mulch is appropriate where mulch is maintained for more than three months. Straw mulch is subject to wind blowing unless anchored, is the most commonly used mulching material, and has the best microenvironment for germinating seeds.

Mulch Maintenance *

- a) Inspect after rainstorms to check for movement of mulch or erosion. If washout, breakage, or erosion occurs, repair surface, reseed, remulch, and install new netting.
- b) Straw or grass mulches that blow or wash away should be repaired promptly.
- c) If plastic netting is used to anchor mulch, care should be taken during initial mowing to keep the mower height high. Otherwise, the netting can wrap up on the mower blade shafts. After a period of time, the netting degrades and becomes less of a problem.
- d) Continue inspections until vegetation is well established.
- 4) **Land Grading** Grading on fill slopes, cut slopes, and stockpile areas will be done with full siltation controls in place.

Land Grading Design/Installation Requirements

- a) Areas to be graded should be cleared and grubbed of all timber, logs, brush, rubbish, and vegetated matter that will interfere with the grading operation. Topsoil should be stripped and stockpiled for use on critical disturbed areas for establishment of vegetation. Cut slopes to be topsoiled should be thoroughly scarified to a minimum depth of 3-inches prior to placement of topsoil.
- b) Fill materials should be generally free of brush, rubbish, rocks, and stumps.
 Frozen materials or soft and easily compressible materials should not be used in fills intended to support buildings, parking lots, roads, conduits, or other structures.
- c) Earth fill intended to support structural measures should be compacted to a minimum of 90 percent of Standard Proctor Test density with proper moisture control, or as otherwise specified by the engineer responsible for the design. Compaction of other fills should be to the density required to control sloughing, erosion or excessive moisture content. Maximum thickness of fill layers prior to compaction should not exceed 9 inches.
- d) The uppermost one foot of fill slopes should be compacted to at least 85 percent of the maximum unit weight (based on the modified AASHTO compaction test). This is usually accomplished by running heavy equipment over the fill.
- e) Fill should consist of material from borrow areas and excess cut will be stockpiled on site. All disturbed areas should be free draining, left with a neat and finished appearance, and should be protected from erosion.

Land Grading Stabilization Inspection/Maintenance *

- a) All slopes should be checked periodically to see that vegetation is in good condition. Any rills or damage from erosion and animal burrowing should be repaired immediately to avoid further damage.
- b) If seeps develop on the slopes, the area should be evaluated to determine if the seep will cause an unstable condition. Subsurface drains or a gravel mulch may be required to solve seep problems.
- c) Areas requiring revegetation should be repaired immediately. Control undesirable vegetation such as weeds and woody growth to avoid bank stability problems in the future.
- 5) <u>Topsoiling *</u> Topsoiling will help establish vegetation on all disturbed areas throughout the site during the seeding process. The soil texture of the topsoil to be used will be a sandy loam to a silt loam texture with 15% to 20% organic content.

Topsoiling Placement

- a) Topsoil should not be placed while in a frozen or muddy condition, when the subgrade is excessively wet, or when conditions exist that may otherwise be detrimental to proper grading or proposed seeding.
- b) Do not place topsoil on slopes steeper than 2.5:1, as it will tend to erode.
- c) If topsoil and subsoil are not properly bonded, water will not infiltrate the soil profile evenly and it will be difficult to establish vegetation. The best method is to actually work the topsoil into the layer below for a depth of at least 6 inches.
- 6) **Permanent Seeding** Permanent Seeding should be done immediately after the final design grades are achieved. Native species of plants should be used to establish perennial vegetative cover on disturbed areas. The revegetation should be done early enough in the fall so that a good cover is established before cold weather comes and growth stops until the spring. A good cover is defined as vegetation covering 75 percent or more of the ground surface.

Permanent Seeding Seedbed Preparation

a) In infertile or coarse-textured subsoil, it is best to stockpile topsoil and re-spread it over the finished slope at a minimum 2 to 6-inch depth and roll it to provide a firm seedbed. The topsoil must have a sandy loam to silt loam texture with 15% to 20% organic content. If construction fill operations have left soil exposed with a loose, rough, or irregular surface, smooth with blade and roll.

- b) Loosen the soil to a depth of 3-5 inches with suitable agricultural or construction equipment.
- c) Areas not to receive topsoil shall be treated to firm the seedbed after incorporation of the lime and fertilizer so that it is depressed no more than ¹/₂ - 1 inch when stepped on with a shoe. Areas to receive topsoil shall not be firmed until after topsoiling and lime and fertilizer is applied and incorporated, at which time it shall be treated to firm the seedbed as described above.

Permanent Seeding Grass Selection/Application

- a) Select an appropriate cool or warm season grass based on site conditions and seeding date. Apply the seed uniformly by hydro-seeding, broadcasting, or by hand. Uniform seed distribution is essential. On steep slopes, hydroseeding may be the most effective seeding method. Surface roughening is particularly important when preparing slopes for hydroseeding.
- b) Lime and fertilize. Organic fertilizer shall be utilized in areas within the 100-foot buffer zone to a wetland resource area.
- c) Mulch the seedings with straw applied at the rate of ½ tons per acre. Anchor the mulch with erosion control netting or fabric on sloping areas. Amoco supergro or equivalent should be utilized.

Permanent Seeding Inspection/Maintenance *

- a) Frequently inspect seeded areas for failure and make necessary repairs and reseed immediately. Conduct or follow-up survey after one year and replace failed plants where necessary.
- b) If vegetative cover is inadequate to prevent rill erosion, overseed and fertilize in accordance with soil test results.
- c) If a stand has less than 40% cover, reevaluate choice of plant materials and quantities of lime and fertilizer. Re-establish the stand following seedbed preparation and seeding recommendations, omitting lime and fertilizer in the absence of soil test results. If the season prevents resowing, mulch or jute netting is an effective temporary cover.
- d) Seeded areas should be fertilized during the second growing season. Lime and fertilize thereafter at periodic intervals, as needed. Organic fertilizer shall be utilized in areas within the 100-foot buffer zone to a wetland resource area.

Dust Control:

Dust control will be utilized throughout the entire construction process of the site. For example, keeping disturbed surfaces moist during windy periods will be an effective control measure, especially for construction access roads. The use of dust control will prevent the movement of soil to offsite areas. However, care must be taken to not create runoff from excessive use of water to control dust. The following are methods of Dust Control that may be used on-site:

- Vegetative Cover The most practical method for disturbed areas not subject to traffic.
- Calcium Chloride Calcium chloride may be applied by mechanical spreader as loose, dry granules or flakes at a rate that keeps the surface moist but not so high as to cause water pollution or plant damage.
- Sprinkling The site may be sprinkled until the surface is wet. Sprinkling will be effective for dust control on haul roads and other traffic routes.
- Stone Stone will be used to stabilize construction roads and will provide dust control.

The general contractor shall employ an on-site water vehicle for the control of dust as necessary.

Non-Stormwater Discharges:

The construction de-watering and all non-stormwater discharges will be directed into a sediment dirt bag (or equivalent inlet protection) or a sediment basin. Sediment material removed shall be disposed of in accordance with all applicable local, state, and federal regulations.

The developer and site general contractor will comply with the E.P.A.'s Final General Permit for Construction De-watering Discharges, (N.P.D.E.S., Section 402 and 40 C.F.R. 122.26(b) (14) (x).

Inspection/Maintenance:

Operator personnel must inspect the construction site at least once every 14 calendar days and within 24 hours of a storm event of ½-inch or greater. The applicant shall be responsible to secure the services of a design professional or similar professional (inspector) on an on-going basis throughout all phases of the project. Refer to the Inspection/Maintenance Requirements presented earlier in the "Structural and Stabilization Practices." The inspector should review the erosion and sediment controls with respect to the following:

• Whether or not the measure was installed/performed correctly.

- Whether or not there has been damage to the measure since it was installed or performed.
- What should be done to correct any problems with the measure.

The inspector should document the findings and should request the required maintenance or repair for the pollution prevention measures when the inspector finds that it is necessary for the measure to be effective. The inspector should notify the appropriate person to make the required changes.

It is essential that the inspector document the inspection of the pollution prevention measures. These records will be used to request maintenance and repair and to prove that the inspection and maintenance were performed. The forms list each of the measures to be inspected on the site, the inspector's name, the date of the inspection, the condition of the measure/area inspected, maintenance or repair performed and any changes which should be made to the Operation and Maintenance Plan to control or eliminate unforeseen pollution of storm water.

APPENDIX G:

LONG TERM BEST MANAGEMENT

PRACTICES O&M PLAN

Long Term Stormwater Best Management Practices Operation and Maintenance Plan

for

<u>Willow Road</u> Boxford, Massachusetts

November 19, 2020

The following operation and maintenance plan has been provided to satisfy the requirements of Standard 9 of the Mass DEP Stormwater Management Handbook associated with development of the site and associated infrastructure. The success of the Stormwater Management Plan depends on the proper implementation, operation and maintenance of several management components. The following procedures shall be implemented to ensure success of the Stormwater Management Plan:

- 1. The contractor shall comply with the details of construction of the site as shown on the approved plans.
- 2. The stormwater management system shall be inspected and maintained as indicated below.
- 3. Effective erosion control measurers during and after construction shall be maintained until a stable turf is established on all altered areas.
- 4. A Stormwater Management Maintenance Log is included at the end of this Appendix.

Basic Information

Stormwater Management System Owner:	Toll Brothers, Inc. 134 Flanders Road Westborough, MA 01581 P: (508) 366-1440
Boxford Stormwater Advisory Committee:	7A Spofford Road Boxford, MA 01921 P: (978) 887-6000 ext. 181
Boxford Planning Board:	7A Spofford Road Boxford, MA 01921 P: (978) 887-6000 ext. 181
Boxford Conservation Commission:	7A Spofford Road Boxford, MA 01921 P: (978) 887-6000 ext. 181

Erosion and Sedimentation Controls during Construction:

The site and drainage construction contractor shall be responsible for managing stormwater during construction. Routine monitoring of disturbed soils shall be performed to ensure adequate runoff and pollution control during construction.

A sediment and erosion control barrier will be placed as shown on the Grading & Drainage Plan prior to the commencement of any clearing, grubbing, and earth removal or construction activity. The integrity of the erosion control barrier will be maintained by periodic inspection and replacement as necessary. The erosion control barrier will remain in place until the first course of pavement has been placed and all side slopes have been loamed and seeded and vegetation has been established.

Operations and maintenance plans for the Stormwater Management construction phase and long term operation of the system have been attached to this report.

General Conditions

1. The site contractor shall be responsible for scheduling regular inspections and maintenance of the stormwater BMP's until the project has been completed. The BMP maintenance shall be conducted as detailed in the following long-term pollution prevention plan and on the approved design plans:

"Site Plan of Land for the Willows at Boxford, Located at Boxford, Massachusetts" by The Morin Cameron Group, Inc. dated November 19, 2020.

- 2. All Stormwater BMP's shall be operated and maintained in accordance with the design plans and the following Long-Term Pollution Prevention Plan.
- 3. The owner shall:
 - a. Maintain an Operation and Maintenance Log for the last three years. The Log shall include all BMP inspections, repairs, replacement activities and disposal activities (disposal material and disposal location shall be included in the Log);
 - b. Make the log available to the Boxford Planning Board and Conservation Commission upon request;
 - c. Allow members and agents of the Boxford Planning Board and Conservation Commission to enter the premises and ensure that the Owner has complied with the Operation and Maintenance Plan requirements for each BMP.
- 4. A recommended inspection and maintenance schedule is outlined below based on statewide averages. This inspection and maintenance schedule shall be adhered to at a minimum for the first year of service of all BMP's referenced in this document. At the commencement of the first year of service, a more accurate inspection/maintenance schedule shall be determined based on the level of service for this site.

Long-Term Pollution Prevention Plan (LTPPP)

Vegetated Areas:

Immediately after construction, monitoring of the erosion control systems shall occur until establishment of natural vegetation. Afterwards, vegetated areas shall be maintained as such. Vegetation shall be replaced as necessary to ensure proper stabilization of the site.

Cost: Included with annual landscaping budget. Consult with local landscape contractors.

Paved Areas:

Sweepers shall sweep paved areas periodically during dry weather to remove excess sediments and to reduce the amount of sediments that the drainage system shall have to remove from the runoff. The sweeping shall be conducted primarily between March 15th and November 15th. Special attention should be made to sweeping paved surfaces in March and April before spring rains wash residual sand into the drainage system.

Cost: Consult with local landscaping companies for associated costs if necessary.

Salt used for de-icing on the roadway during winter months shall be limited as much as possible as this will reduce the need for removal and treatment. Sand containing the minimum amount of calcium chloride (or approved equivalent) needed for handling may be applied as part of the routine winter maintenance activities.

Deep Sump Hooded Catch Basins:

The Catch basin grates shall be checked quarterly and following heavy rainfalls to verify that the inlet openings are not clogged by debris. Debris shall be removed from the grates and disposed of properly. Deep sump catch basins shall be inspected twice per year and cleaned as needed when accumulated sediments exceeds 2' from the bottom of the sump (approximately 1/2 of the sump capacity). Catch basins with hoods shall be inspected annually to check oil build-up and outlet obstructions. Material shall be removed from catch basins and disposed of in accordance with all applicable regulations

Cost: Estimated \$50 - \$100 per cleaning per catch basin as needed. The Owner shall consult local vacuum cleaning contractors for detailed cost estimates.

Public Safety Concerns: Catch basins shall not be left open and unattended at any time during inspection, cleaning or otherwise. Broken or missing grates or frames shall be replaced immediately. At no time shall any person enter the basin structure unless measures have been taken to ensure safe access in accordance with OSHA enclosed space regulations.

CDS Water Quality Units:

The CDS and Vortsentry water quality pretreatment units shall be inspected twice per year in April and October. The unit shall be cleaned per manufacturer instructions included herein.

Subsurface Stone Trench System:

The subsurface stone trench and pipe recharge systems shall be checked for debris accumulation twice per year. Each system is equipped with inspection ports. Additional inspections should be scheduled during the first few months to make sure that the facility is functioning as intended. Silt, sand and sediment, if significant accumulation occurs, shall be removed annually. Material removed from the stone trench and pipe shall be disposed of in accordance with all applicable local, state, and federal regulations. In the case that water remains in the infiltration facilities for greater than three (3) days after a storm event, an inspection is warranted and necessary maintenance or repairs should be addressed as necessary.

Cost: \$500-\$2,500 per cleaning depending on the volume of material/liquids that need to be removed.

Public Safety Concerns: The inspection port covers shall not be left open and unattended at any time during inspection, cleaning or otherwise. Broken covers shall be replaced immediately.

Infiltration/Detention Basins:

The infiltration basin shall be inspected after every major storm event for the first 3 months after construction; a major storm event is 3.9 inches of rainfall in a 24 hour period (2 year storm). Thereafter, the basin shall be inspected twice per year, typically in the spring and fall. If erosion or loss of vegetation is observed in the basin, it shall be repaired immediately and new vegetation shall be established. Trash, leaves, branches, etc. shall be removed from facility.

The outlet structures and overflow spillways shall be inspected annually for obstructions and structural integrity. The inspections shall be conducted by qualified personnel.

Cost: Consult with local landscaping companies for associated costs if necessary.

Sediment Forebay:

The forebay shall be inspected after every major storm event for the first 3 months after construction; a major storm event is 3.9 inches of rainfall in a 24 hour period (2 year storm). Thereafter, the basin shall be inspected twice per year. All forebays shall be inspected on an annual basis, typically in the spring months, and sediment shall be removed when depth exceeds 6 inches.

Cost: Consult with local landscaping or pumping companies for associated costs if necessary.

Debris & Litter:

All debris and litter shall be removed from the roadway and parking lots as necessary to prevent migration into the drainage system.

Pesticides, Herbicides, and Fertilizers:

Pesticides and herbicides shall be used sparingly. Fertilizers shall be restricted to the use of organic fertilizers only. All fertilizers, herbicides, pesticides, sand and salt for deicing and the like shall be stored in dry area that is protected from weather.

Long Term Stormwater Best Management Practices Operation & Maintenance Plan Willow Road, Boxford, Massachusetts 01921 November 19, 2020 – Page 4 of 5 Cost: Included in the routine landscaping maintenance schedule. The Owner shall consult local landscaping contractors for details.

Public Safety Concerns: Chemicals shall be stored in a secure area to prevent children from obtaining access to them. Any major spills shall be reported to municipal officials.

Prevention of Illicit Discharges:

Illicit discharges to the stormwater management system are not allowed. Illicit discharges are discharges that are not comprised entirely of stormwater. Pursuant to Mass DEP Stormwater Standards the following activities or facilities are not considered illicit discharges: firefighting, water line flushing, landscape irrigation, uncontaminated groundwater, potable water sources, foundation drains, air conditioning condensation, footing drains, individual resident car washing, flows from riparian habitats and wetlands, dechlorinated water from swimming pools, water used for street washing and water used to clean residential building without detergents.

To prevent illicit discharges to the stormwater management system the following policies should be implemented:

- 1. Provisions For Storing Materials And Waste Products Inside Or Under Cover
- 2. Vehicle Maintenance And Washing Controls
- 3. Requirements for Routine Inspections of the Stormwater Management System (i.e.: subsurface infiltration system and outlet control structure.)
- 4. Spill Prevention and Response Plans.

Snow Storage:

Property owner shall inform their snow removal contractor of the designated areas for snow storage shown on the Site Layout Plans in the Site Plan of Land.

Project Location: Willow Road, Boxford, MA

Stormwater Management Maintenance Log

Long Term Practices

Best Management Practice	Inspection Frequency	Date Inspected	Inspector	Minimum Maintenance and Key Items to Check	Cleaning/Repair Needed: (List Items)	Date of Cleaning/ Repair	Performed by
Infiltration/ Detention Basins	Inspect after every major storm event for first 3 months after construction Thereafter, twice per year (April / October)			 Check for standing water in basins 72 hours after a storm to verify if structure is draining Is there erosion or loss of vegetation Remove leaves, trash, debris, etc. from facilities Rehabilitate structure if it fails due to clogging 			
Sediment Forebays	Inspect after every major storm event for first 3 months after construction Thereafter, annually (during Spring months)			 Check for standing water in forebay 72 hours after a storm to verify if draining Remove accumulated sediment when depth exceeds 6" Remove leaves, trash, debris, etc. from facility 			
Deep Sump Hooded Catch Basins	Inspect inlet grate quarterly Inspect structure twice per year (April / October)			 Check inlet grate for obstructions Check that sediment depth in sump is less than 2' Check hood for signs of oil build-up or blockages 			
Water Quality Unit	Inspect after every major storm event for first 3 months after construction Inspect twice per year (April / October)			 Refer to CDS Inspection and Maintenance Guide by Contech 			

Subsurface Stone Trenches	Inspect after every major storm event for first 3 months after construction Thereafter, twice per year (April / October)	 Check for standing water in Stone Trench 72 hours after a storm to verify if structure is draining Rehabilitate structure if it fails due to clogging 	
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(1) Refer to the Massachusetts Stormwater Handbook issued January 2, 2008

Notes (Include deviations from: Site Plan Approval and Order of Conditions and Approved Plans):

- 1. Limited or no use of sodium chloride slats, fertilizers or pesticides recommended. Slow release fertilizer recommended if necessary.
- 2. Major Storm Event: 3.9" of rainfall in a 24 hour period (2 year storm)

Stormwater Control Manager _____



CDS® Inspection and Maintenance Guide





Maintenance

The CDS system should be inspected at regular intervals and maintained when necessary to ensure optimum performance. The rate at which the system collects pollutants will depend more heavily on site activities than the size of the unit. For example, unstable soils or heavy winter sanding will cause the grit chamber to fill more quickly but regular sweeping of paved surfaces will slow accumulation.

Inspection

Inspection is the key to effective maintenance and is easily performed. Pollutant transport and deposition may vary from year to year and regular inspections will help ensure that the system is cleaned out at the appropriate time. At a minimum, inspections should be performed twice per year (e.g. spring and fall) however more frequent inspections may be necessary in climates where winter sanding operations may lead to rapid accumulations, or in equipment washdown areas. Installations should also be inspected more frequently where excessive amounts of trash are expected.

The visual inspection should ascertain that the system components are in working order and that there are no blockages or obstructions in the inlet and separation screen. The inspection should also quantify the accumulation of hydrocarbons, trash, and sediment in the system. Measuring pollutant accumulation can be done with a calibrated dipstick, tape measure or other measuring instrument. If absorbent material is used for enhanced removal of hydrocarbons, the level of discoloration of the sorbent material should also be identified during inspection. It is useful and often required as part of an operating permit to keep a record of each inspection. A simple form for doing so is provided.

Access to the CDS unit is typically achieved through two manhole access covers. One opening allows for inspection and cleanout of the separation chamber (cylinder and screen) and isolated sump. The other allows for inspection and cleanout of sediment captured and retained outside the screen. For deep units, a single manhole access point would allows both sump cleanout and access outside the screen.

The CDS system should be cleaned when the level of sediment has reached 75% of capacity in the isolated sump or when an appreciable level of hydrocarbons and trash has accumulated. If absorbent material is used, it should be replaced when significant discoloration has occurred. Performance will not be impacted until 100% of the sump capacity is exceeded however it is recommended that the system be cleaned prior to that for easier removal of sediment. The level of sediment is easily determined by measuring from finished grade down to the top of the sediment pile. To avoid underestimating the level of sediment in the chamber, the measuring device must be lowered to the top of the sediment pile carefully. Particles at the top of the pile typically offer less resistance to the end of the rod than consolidated particles toward the bottom of the pile. Once this measurement is recorded, it should be compared to the as-built drawing for the unit to determine weather the height of the sediment pile off the bottom of the sump floor exceeds 75% of the total height of isolated sump.

Cleaning

Cleaning of a CDS systems should be done during dry weather conditions when no flow is entering the system. The use of a vacuum truck is generally the most effective and convenient method of removing pollutants from the system. Simply remove the manhole covers and insert the vacuum hose into the sump. The system should be completely drained down and the sump fully evacuated of sediment. The area outside the screen should also be cleaned out if pollutant build-up exists in this area.

In installations where the risk of petroleum spills is small, liquid contaminants may not accumulate as quickly as sediment. However, the system should be cleaned out immediately in the event of an oil or gasoline spill should be cleaned out immediately. Motor oil and other hydrocarbons that accumulate on a more routine basis should be removed when an appreciable layer has been captured. To remove these pollutants, it may be preferable to use absorbent pads since they are usually less expensive to dispose than the oil/water emulsion that may be created by vacuuming the oily layer. Trash and debris can be netted out to separate it from the other pollutants. The screen should be power washed to ensure it is free of trash and debris.

Manhole covers should be securely seated following cleaning activities to prevent leakage of runoff into the system from above and also to ensure that proper safety precautions have been followed. Confined space entry procedures need to be followed if physical access is required. Disposal of all material removed from the CDS system should be done in accordance with local regulations. In many jurisdictions, disposal of the sediments may be handled in the same manner as the disposal of sediments removed from catch basins or deep sump manholes.



CDS Model	Dian	neter	Distance from Water Surface to Top of Sediment Pile		Sediment Storage Capacity	
	ft	m	ft	m	У³	m³
CDS1515	3	0.9	3.0	0.9	0.5	0.4
CDS2015	4	1.2	3.0	0.9	0.9	0.7
CDS2015	5	1.3	3.0	0.9	1.3	1.0
CDS2020	5	1.3	3.5	1.1	1.3	1.0
CDS2025	5	1.3	4.0	1.2	1.3	1.0
CDS3020	6	1.8	4.0	1.2	2.1	1.6
CDS3025	6	1.8	4.0	1.2	2.1	1.6
CDS3030	6	1.8	4.6	1.4	2.1	1.6
CDS3035	6	1.8	5.0	1.5	2.1	1.6
CDS4030	8	2.4	4.6	1.4	5.6	4.3
CDS4040	8	2.4	5.7	1.7	5.6	4.3
CDS4045	8	2.4	6.2	1.9	5.6	4.3
CDS5640	10	3.0	6.3	1.9	8.7	6.7
CDS5653	10	3.0	7.7	2.3	8.7	6.7
CDS5668	10	3.0	9.3	2.8	8.7	6.7
CDS5678	10	3.0	10.3	3.1	8.7	6.7

Table 1: CDS Maintenance Indicators and Sediment Storage Capacities



Support

- Drawings and specifications are available at www.contechstormwater.com.
- Site-specific design support is available from our engineers.
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CDS Inspection & Maintenance Log

CDS Model: Location:					
Date	Water depth to sediment ¹	Floatable Layer Thickness ²	Describe Maintenance Performed	Maintenance Personnel	Comments

1. The water depth to sediment is determined by taking two measurements with a stadia rod: one measurement from the manhole opening to the top of the sediment pile and the other from the manhole opening to the water surface. If the difference between these measurements is less than the values listed in table 1 the system should be cleaned out. Note: to avoid underestimating the volume of sediment in the chamber, the measuring device must be carefully lowered to the top of the sediment pile.

2. For optimum performance, the system should be cleaned out when the floating hydrocarbon layer accumulates to an appreciable thickness. In the event of an oil spill, the system should be cleaned immediately.

ILLICIT DISCHARGE STATEMENT

APPENDIX H:

Illicit Discharge Compliance Statement

I, <u>Scott P. Cameron, P.E.</u>, hereby notify the Boxford Planning Board & Conservation Commission that I have not witnessed, nor am aware of any existing illicit discharges at the site known as Willow Road in Boxford, Massachusetts. I also hereby certify that the development of said property as illustrated on the final plans entitled "Site Plan of Land for the Willows At Boxford," prepared by The Morin-Cameron Group, Inc. dated November 19, 2020 and as revised and approved by the Boxford Planning Board & Conservation Commission and maintenance thereof in accordance with the "Construction Phase Best Management Practices Plan" and "Long-Term Pollution Prevention Plan" prepared by The Morin-Cameron Group, Inc dated November 19, 2020 and as revised and approved by the Boxford Planning Board & Conservation Commission will not create any new illicit discharges. There is no warranty implied regarding future illicit discharges that may occur as a result of improper construction or maintenance of the stormwater management system or unforeseen accidents.

Name:	Scott P. Cameron, P.5.
Company:	The Morin-Cameron Group, Inc.
Title:	Owner's Representative
Signature:	
Date:	11-19-2020